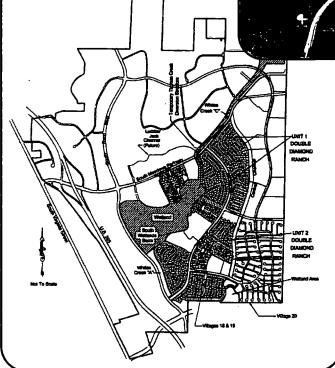
Addendum Hydrologic and Hydraulic Analyses Double Diamond Ranch

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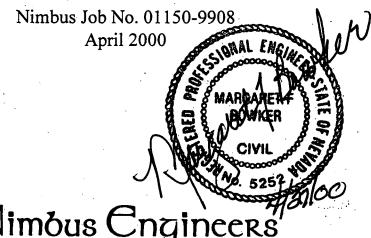
April, 2000 Job No. 9908



ADDENDUM HYDROLOGIC AND HYDRAULIC ANALYSES WILBUR MAY BLVD. AND DOUBLE DIAMOND PARKWAY DOUBLE DIAMOND RANCH

City of Reno, Nevada

PREPARED FOR:
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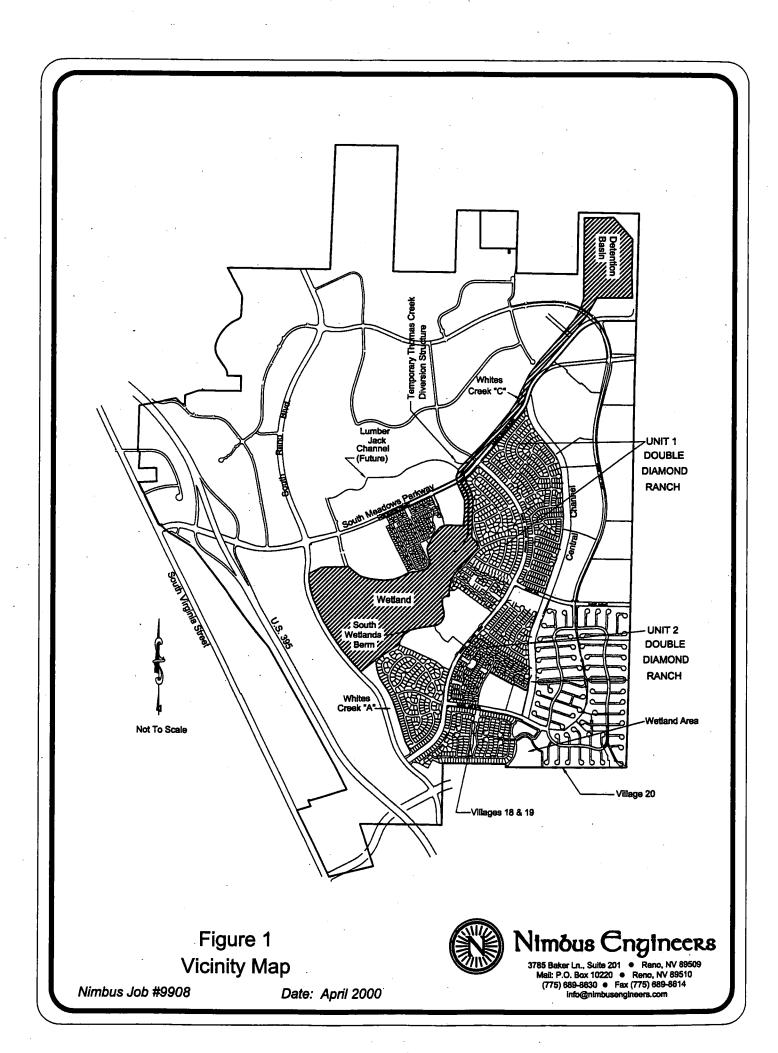
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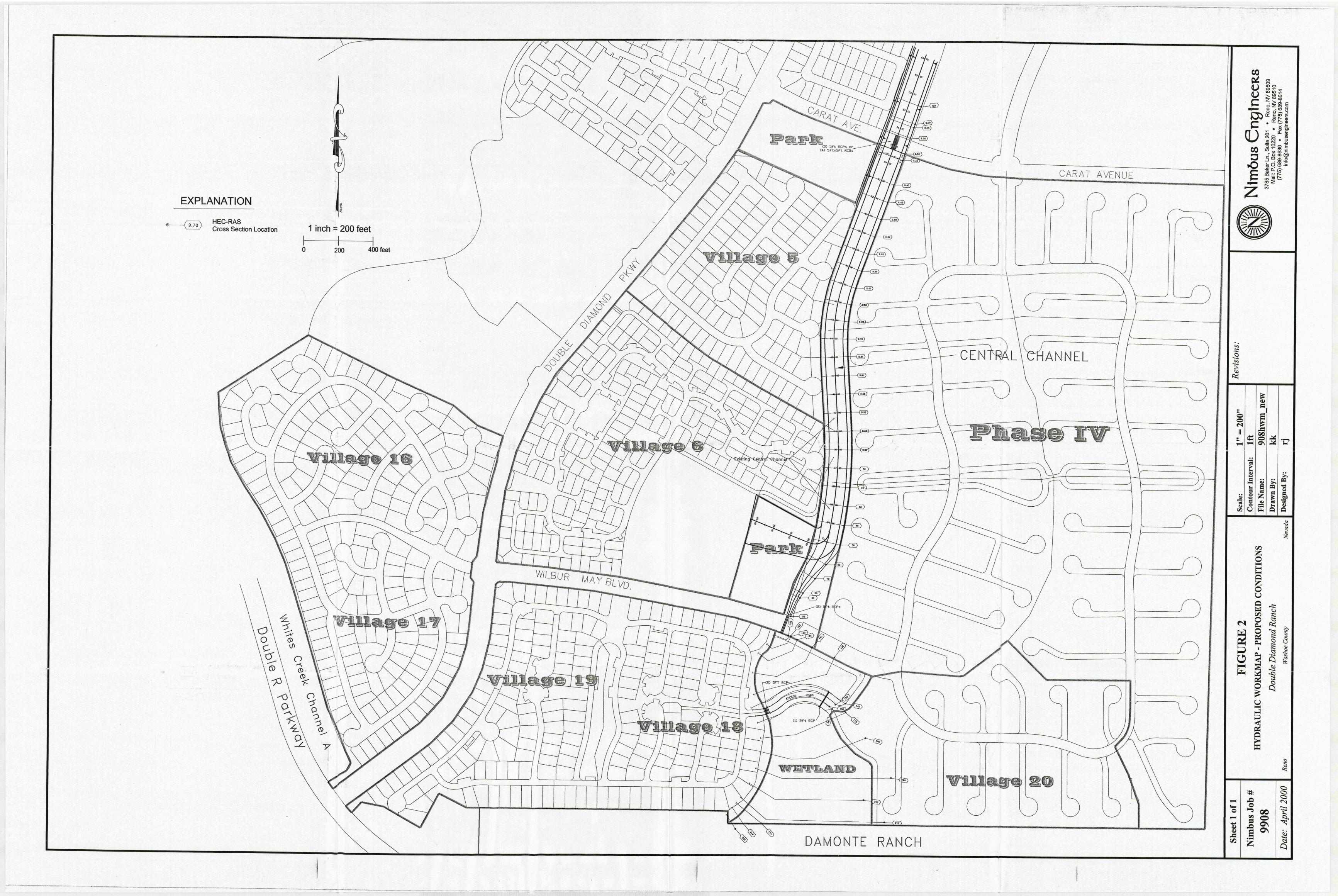
1.0 INTRODUCTION

This report is an addendum to a report prepared by Nimbus Engineers titled *Hydrologic and Hydraulic Analysis, Wilbur May Blvd. and Double Diamond Pkwy., Double Diamond Ranch* (September 1998), hereinafter referred to as the original report. Specifics of the addendum are outlined below. A list of references are contained in the original report.

The Double Diamond Ranch is located in Reno, Nevada in the south Truckee Meadows. A vicinity map of the Double Diamond Ranch is shown in Figure 1. The area of the Double Diamond Ranch that is the subject of this addendum is shown on the hydraulic work map in Figure 2. The project area is described as: (1) a wetland bounded on the west by Double Diamond Villages 18 and 19, on the north by Wilbur May Boulevard, on the east by the Double Diamond Recreation Center and Village 20, and on the south by the Damonte Ranch subdivision; and (2) the Central Channel extending north from the culverts beneath Wilbur May Boulevard to a point approximately 200 feet downstream of the culverts beneath Carat Avenue (Figure 2). This addendum modifies the original hydrologic analysis (HEC-1) and hydraulic analysis (HEC-RAS).

The HEC-1 model was modified from the original analysis to reflect development in the Damonte Ranch because this development will affect peak flows through the Double Diamond Ranch (see Section 2.0). The contributing watershed for the present analysis lies upstream of Carat Avenue where it crosses the existing Central Channel and extends south to the constructed Whites Creek Branch 3 channel located along the south property boundary of the Damonte Ranch. This watershed was designated as W18RB in the Application for Conditional Letter of Map Revision (CLOMR) for Double Diamond Ranch (Nimbus, 1995). The subroutine of the CLOMR HEC-1 model that estimates runoff from W18RB, a subwatershed within the larger Whites Creek watershed, was used in the HEC-1 analysis that is part of the present report. The Branch 3 channel will convey flow from storms of magnitudes less than or equal to the 100-year event to Steamboat Creek. The channel will prevent flow from the Whites Creek watershed that is tributary to Branch 3 from discharging through the Damonte Ranch and the Double Diamond Ranch.





The original HEC-RAS model was developed using a single channel to convey runoff, resulting from the 100-year storm event, from the Damonte Ranch in a northern direction, past Villages 18 and 19, through culverts beneath Wilbur May Boulevard, to the beginning of the existing Central Channel. In this addendum, the revised HEC-RAS model simulates flow through a wetland located east of Villages 18 and 19, beneath Wilbur May Boulevard and through the Central Channel to a point downstream of the culverts beneath Carat Avenue (see Section 3.0).

2.0 HYDROLOGIC ANALYSIS

The HEC-1 analysis in this addendum contains a revised estimate of the Soil Conservation Service (SCS) runoff curve number for the Damonte Ranch. The revised curve number reflects the impervious area within the proposed subdivision when development is completed. The Damonte Ranch is part of subwatershed W18RB within the larger Whites Creek watershed. In the original HEC-1 model, a curve number of 80 was used for W18RB. In the revised HEC-1 model, a curve number of 85 was used to reflect the higher runoff potential of the Damonte Ranch when development is completed.

The revised model contained three phases of development at Double Diamond: (1) Phase II which was modeled to include all of Villages 5 and 6 and portions of Villages 13, 14, and 15; (2) Phase III which include Villages 16, 17, 18, and 19; and (3) Phase IV which included Villages 7, 8, 9, 20, 21, 22, and 23. These development phases were included in the model in order to simulate runoff for final developed conditions and to allow adequate culvert capacity at Carat Avenue. Phase II development was based upon the Preliminary Storm Drainage Study, Phase II, Double Diamond Ranch, Villages 5, 6, 13, 14, & 15 by MacKay & Somps (1997) which also included storm-water discharge from Villages 16 and 17 via the parallel storm drains beneath Double Diamond Parkway labeled D10. Villages 7, 8, 9, 21, 22, and 23 (Phase IV) were modeled as one watershed discharging to the Central Channel because a detailed drainage plan was not available showing discharge points from each village to the Central Channel. Village 20 was modeled separately from the other Phase IV Villages and the flow was assumed to discharge to the wetland.

The original report contains a more detailed discussion of the hydrologic variables used in the HEC-1 model. HEC-1 modeling results for the 100-year, 24-hour storm event are summarized in Table 1. Complete HEC-1 modeling results are contained in Appendix A.

Table 1. Peak Flows Computed by HEC-1 at Selected Points and Corresponding Peak Flow Inputs to HEC-RAS, Double Diamond Ranch, Reno Nevada.

Location	HEC-1 Computation	HEC-RAS Cross Section	Peak Flow (cubic feet per second)		
	Point	Number	HEC-11	HEC-RAS ²	
Discharge Point from Wetland through Culverts at Wilbur May Boulevard into the Central Channel	CB WET	220	266	300	
Flow from Central Channel Combined with Discharges from Phase IV Villages and Village 6 Discharge Point E14 at Approximately 650 feet North of Wilbur May Boulevard	C14	30	467	500	
Flow in Central Channel combined with Flow from Storm Drain Discharge Points D10 and D12 Located Approximately 350 Feet South of Carat Avenue	C10PRK	9.5	591	650	

^{1.} Peak flows calculated using the HEC-1 model and a precipitation depth 2.60 inches for the 100-year, 24-hour storm.

^{2.} Peak flows were entered into the HEC-RAS model at the cross sections indicated. The flow rates remained at the rate listed above in the downstream direction until the flow was increased at a downstream cross section. For example, at the farthest upstream cross section (#220) the flow rate was held constant at 300 cubic feet per second (cfs) downstream to cross section 30 where the flow rate was increased to 500 cfs.

3.0 HYDRAULIC ANALYSIS

In the original hydraulic analysis, a HEC-RAS model was developed with a single channel (i.e., Phase 3 Central Channel) to convey the 100-year, 24-hour peak flow from subwatershed W18RB. A channel alignment was proposed from the southern property boundary of the Double Diamond Ranch northward, around Villages 18 and 19, through culverts beneath Wilbur May Boulevard, and finally northward to a point where the channel would join the existing Central Channel.

In the revised hydraulic analysis that is part of this addendum, a HEC-RAS model was developed through the wetland area located east of Villages 18 and 19, and along the Central Channel north of Wilbur May Boulevard to a point approximately 200 feet downstream of the Carat Avenue crossing over the Central Channel (Figure 2). Modeling results are contained in Appendix B. The 100-year, 24-hour storm event was modeled using peak flow rates that increased in a downstream direction from 300 cubic feet per second (cfs) through the wetland to 700 cfs upstream of Carat Avenue. Flow rates used in the HEC-RAS model were greater that those calculated by the HEC-1 model and are summarized in Table 1.

When the wetland area is completed, a low-flow channel capable of conveying the 2-year, 24-hour peak flow will meander through the wetland to maintain vegetation. Flows in excess of the 2-year, 24-hour storm will be conveyed to the channel over-bank area in the surrounding wetland. The conveyance capacity of the low-flow channel will be minimal and consequently the channel was not included in the revised HEC-RAS model. Each cross section within the wetland was modeled with a horizontal bottom. The elevations of the wetland bottom that were modeled will result in an excavation depth of approximately 5 to 6 feet below the existing land surface.

3.1 HEC-RAS Cross Sections

Cross-section locations modeled in HEC-RAS are shown on Figure 2. Cross sections 10 through 100 were taken from the original model for the channel from the upstream ends of the culverts

beneath Wilbur May Boulevard, north, to the existing Central Channel. Cross sections 8.8 through 9.99 were added downstream of cross section 10 to a point downstream of Carat Avenue. Cross sections 105 through 220 were added in order to model the wetland from Wilbur May Boulevard to the northern property boundary of the Damonte Ranch.

Within the wetland area, additional cross sections were calculated by HEC-RAS using a program feature that interpolates cross sections. The interpolated cross sections are indicated by an asterisk next to the cross section number in the model output (Appendix B). The point where flow from the Damonte Ranch enters the wetland area (cross sections 220 through 214) was modeled as a trapezoidal channel with 3:1 side slopes and tops of the right banks set at the existing land surface elevation. This configuration reflects the grading plans south of the wetland area. The remaining cross sections in the wetland area were modeled across its entire width. Elevations at the ends of the cross-sections adjacent to Villages 18 and 19 (i.e., the western extent of cross sections 100 through 220) were set based upon the proposed grading plan for that area. Grading plans for Village 20, the recreation center, and the access road from Villages 18 and 19 to the recreation center, hereinafter known as the access road, have not been completed. Consequently, elevations at the eastern ends of cross sections were approximated. Side slopes of 3:1 were modeled at the western and eastern ends of the cross sections. The road deck elevation of the access road was approximated based upon the street improvement plan for Village 18.

The HEC-RAS modeling results demonstrate that the wetland, as modeled, has the capacity to convey 300 cfs because of the proposed excavation of the wetland below the existing grade. The Central Channel north of Wilbur May Boulevard will convey flow from the 100-year, 24-hour storm event provided that the culverts at Carat Avenue are sized properly (refer to Section 3.2). Cross-section and water-surface elevation data are summarized in Table 2.

Cross Section #	Downstream Distance to Next Cross Section (feet)	Bottom Elevation (feet, msl)	Existing Wetland Elevation ¹ (feet, msl)	100-Year Water-Surface Elevation (feet, msl)
220	50	4466.0	4469	4467.5
216	55	4465.6	4469	4466.8
214	40	4465.3	4468-70	4465.9
210	100.	4465.0	4468-71	4465.3
200	100	4464.0	4468-71	4464.4
190	100	4463.0	4467-70	4463.3
180	100	4462.0	4467-68	4462.3
170	100	4457.0	4467	4461.3
160	20	4456.0	4466-67	4461.3
155	30	4455.9	4465-67	4461.0
150	40	4455.8	4465-67	4459.3
145	60	4455.6	4465-67	4459.6
140	100	4455.4	4464-65	4459.6
130	100	4454.9	4464-65	4459.6
120	60	4454.5	4463-64	4459.6
110	70	4454.3	4463-64	4459.6
105	25	4454.0	4463-64	4459.5
100	115	4453.8	4463	4459.2
95	110	4453.3	NA	4455.1
90	30	4453.14	· NA	4455.0
80	100	4453.1	NA	4455.0
7.0	100	4453.0	. NA	4454.7
60	100	4452.9	NA	4454.5
50	100	4452.8	NA	4454.4
40	100	4452.7	NA	4454.2
30	100	4452.3	NA	4453.9
20	100	4451.9	NA	4453.5
10	100	4451.5	NA	4453.1

Cross Section #	Downstream Distance to Next Cross Section (feet)	Bottom Elevation (feet, msl)	Existing Wetland Elevation ¹ (feet, msl)	100-Year Water-Surface Elevation (feet, msl)
9.99	100	4451.1	NA	4452.6
9.98	100	4450.7	NA	4452.3
9.97	100	4450.3	NA	4451.9
9.96	100	4449.9	NA	4451.5
9.95	100	4449.5	NA	4451.1
9.94	100	4449.1	, NA	4450.7
9.70	100	4448.7	NA ·	4450.4
9.69	100	4448.3	NA	4450.1
9.68	100	4447.9	NA	4449.9
9.67	100	4447.5	NA	4449.8
9.66	100	4447.1	NA	4449.7
9,65	100	4446.7	NA	4449.6
9.64	100	4446.3	NA	4449.6
9.50	100	4445.9	NA	4449.6
9.45	100	4445.5	NA	4449.5
9.40	140	4445.1	NA	4449.5
9.32	40	4444.5	NA	4449.5
9.30	90	4444.4	NA	4449.1
9.2	80	4444.0	NA	4446.5
9.05	20	4443.7	NA	4445.5
9.00	100	4443.6	NA	4445.4
8.80	0	4443.2	NA	4445.0

^{1.} The wetland was modeled between cross sections 100 and 220. A trapezoidal channel was modeled downstream of Cross section 100.

Note: Elevation is in feet above mean sea level (msl). NA= Not Applicable

3.2 Culverts

In the revised HEC-RAS model, culverts were modeled beneath the wetland access road, beneath Wilbur May Boulevard, and beneath Carat Avenue. The proposed culvert locations are shown in Figure 2.

Culverts were included beneath the proposed access road through the wetland at two locations. The multiple opening routine in HEC-RAS was used to model these culverts. Two 5-foot diameter reinforced concrete pipe (RCP) culverts and one 2-foot diameter RCP were modeled between cross sections 150 and 155. The invert elevations of the 5-foot diameter RCPs were set at 1-foot below the bottom of a proposed storm drain connecting to the RCPs beneath the access road (4455.8 feet, msl at road centerline). The invert elevation of the 2-foot diameter RCP was set at the same elevation as the 5-foot diameter RCPs. The 2-foot diameter culvert was intended to convey low-flows to the eastern portion of the wetland located north of the access road in order to maintain wetland vegetation.

In the original HEC-RAS model, two 5-foot diameter RCPs beneath Wilbur May Boulevard were included between cross sections 95 and 100. These same culverts were included in the revised model at the original invert elevation (4453.6 feet, msl at center line of road).

In developing the revised HEC-RAS model, the invert elevations of the RCPs beneath Wilbur May Boulevard and the access road were assumed to be fixed. Additionally, the invert elevation (4466 feet, msl) of the channel bottom (cross section 220) at the Damonte Ranch was obtained from Odyssey Engineering, Inc. This is the approximate elevation of the Damonte Channel as it exits the subdivision at the Damonte Ranch.

Two types of culverts were modeled beneath Carat Avenue between HEC-RAS cross sections 9.3 and 9.2. Separate HEC-RAS models were developed for the two types of culverts (Appendix B). In the first model, five 5-foot diameter RCPs were modeled beneath Carat Avenue. The water-

surface elevations listed in Table 2 are based on this model. In the second model, four 5-foot wide by 5-foot high reinforced concrete box (RCB) culverts were modeled beneath Carat Avenue. The resulting water-surface elevations calculated by HEC-RAS were approximately the same as those listed in Table 2. Tabular output in Appendix B lists the water-surface elevations for both models. Either culvert configuration will allow approximately 1-foot of freeboard in the Central Channel at Carat Avenue.

3.3 Culvert Erosion Protection

Riprap erosion protection will be required downstream and upstream of the culverts beneath the wetland access road, Wilbur May Boulevard, and Carat Avenue. Design criteria for culvert outlet protection are specified in Section 807.3 and Figure 821 of the *Washoe County Hydrologic Criteria and Drainage Design Manual* (Washoe County, 1996) hereinafter referred to as the Washoe County Manual. The Washoe County Manual (Section 1102.3) requires riprap protection or an energy dissipator for velocities between 5 and 15 fps.

The 100-year, 24-hour storm peak flow that was calculated by the HEC-1 model was approximately 300 cfs through the wetland area. At the access road, the 5-foot diameter RCPs will convey approximately 280 cfs of the 300 cfs total. A flow velocity of 10.2 feet per second (fps) was calculated, by the HEC-RAS model, downstream of the 5-foot diameter RCPs at cross section 152 (Appendix B-Culvert Table). The following specifications for loose riprap were calculated based upon Section 807.3 of the Washoe County Manual. Downstream of the 5-foot diameter RCPs, a d₅₀ of 10 inches (type-M riprap) will be required. Approximately 75 feet of riprap apron will be required downstream of the culvert. An apron width of approximately 45 feet will be required if a well-defined channel does exist downstream of the culvert. If a well-defined channel does exist, then the apron should extend across the channel bottom and up the side slopes extending at least 1 foot above the tail water elevation (4459.0 feet). The flow velocity calculated for the 2-foot diameter RCP beneath the access road was 7.0 fps with a 20 cfs discharge capacity of the total of 300 cfs (Appendix B-Culvert Table). The corresponding riprap protection downstream of the 2-foot RCP would require

a d_{50} of approximately 4 inches for loose riprap (type VL), and an apron of approximately 40 feet in length and 20 feet in width.

The exit velocity calculated by the HEC-RAS model for the two RCPs beneath Wilbur May Boulevard was 10.5 fps for the 300 cfs discharge at cross section 97 (Appendix B-Culvert Table). The following riprap specifications were calculated using procedures outlined in the Washoe County Manual. If loose riprap is selected to protect the channel downstream of the culverts at Wilbur May Boulevard, a mean particle size (d_{50}) of 11 inches (type-M riprap) will be required. Approximately 75 feet of riprap apron would be required along the length of the channel downstream of the culverts, across the channel bottom, and up the side slopes extending at least 1 foot above the tail water elevation (4456.7 feet).

The exit velocity calculated by the HEC-RAS model for the five proposed RCPs beneath Carat Avenue was 9.6 fps for the 650 cfs discharge at cross section 9.29 (Appendix B-Culvert Table). If loose riprap is selected to protect the channel downstream of the Carat Avenue culverts, a mean particle size (d_{50}) of 10 inches (type-M riprap) will be required. Approximately 70 feet of riprap apron would be required along the length of the channel downstream of the culverts, across the channel bottom, and up the side slopes extending at least 1 foot above the tail water elevation (4447.3 feet).

Equivalent riprap sizes described for the outlets of each culvert listed above will also be required at the culvert inlets, but the dimensions of the aprons will be less.

Upstream of the access road, between cross sections 180 and 170, a 5-foot hydraulic drop over a 100-foot length was included in the HEC-RAS model. This hydraulic drop was modeled to match the culvert inverts at the access road and to minimize wetland excavation upstream of the access road. The velocity of water through this hydraulic drop was calculated by HEC-RAS to be 4.6 fps (i.e, at interpolated cross section 179*) or less across the width of the wetland. The calculated water velocities through the wetland were relatively slow (approximately 0.2 to 2.0 fps) because of the

wide flow area at cross sections 160, and 190 through 210. The hydraulic drop resulted in a slight increase in water velocity between cross sections 180 and 170. Although the slope of the drop is 5 percent, the velocity is low because the flow velocity is distributed over the entire cross section rather than being confined to a narrow channel. Erosion protection will not be required through the hydraulic drop located between cross sections 180 and 170, because of the low water velocity. The wetland vegetation will provide adequate erosion protection at this location.

4.0 CONCLUSIONS

A potential design for the conveyance of storm-water discharge through the wetland area to the east of Double Diamond Ranch Villages 18 and 19 is presented in this addendum report. Using the HEC-RAS program, a hydraulic model of the wetland was developed to simulate a discharge of 300 cfs which exceeds the discharge from the 100-year, 24-hour event (268 cfs) estimated by the HEC-1 model. The wetland land-surface elevations and the culverts that were modeled will allow containment and conveyance of discharge from the 100-year, 24-hour storm event from the Damonte Ranch, through the wetland area, and to the existing Central Channel located north of the wetland.

The Central Channel will have the capacity to convey flow from the 100-year, 24 hour storm event downstream of the wetland and through culverts beneath Carat Avenue. Flow through the channel will include final development along both sides of the channel downstream from Wilbur May Boulevard to Carat Avenue. The flow for final development calculated by the HEC-1 model was 591 cfs. A flow rate of 650 cfs was modeled for the channel in the vicinity of Carat Avenue. The channel will convey 650 cfs with approximately 1-foot of free board provided that the culverts at Carat Avenue are sized properly (i.e., five, 5-foot diameter RCPs or four, 5-foot by 5-foot RCBs).

APPENDIX A Hydrologic Analysis HEC-1 Modeling Results

FLOOD HYDROGRAPH PACKAGE (HEC-1)

JUN 1998

VERSION 4.1

RUN DATE 06APR00 TIME 14:45:40

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HYDROLOGIC ENGINEERING CENTER
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DAVIS, CALIFORNIA 95616
(916) 756-1104

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

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  1
            . ID
                   WHITES CREEK SUBBASIN W18RB-NORTH OF WHITES CREEK BRANCH #3 DIVERSION
              ID
                   ADD PHASE II CHANNEL TO EVALUATE CARAT AVENUE CULVERT
              ID 100-YEAR, 24-HOUR MODEL
              ID
                   MODEL INCLUDES DOUBLE DIAMOND DEVELOPMENT PHASE II (VILLAGES 5 & 6 AND PARKS)
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                   , PHASE III (VILLAGES 16, 17, 18, AND 19), AND PHASE IV (VILLAGES 7, 8, 9,
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 40
              LS
                             80
              UD
 41
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43	KM	BETWEEN VILLAGES 18/19 AND VILLAGE 20
44	HC	4
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	*	
45	KK	PH-IV PHASE IV DOUBLE DIAMOND DEVELOPMENT (VILLAGES 7,8,9,21,22,&23).
46	км	VILLAGE 20 WAS MODELED ABOVE WITH FLOW ENTERING THE WETLAND SOUTH
47	KM	OF WILBUR MAY BLVD. DETAILED DRAINAGE PLANS WERE NOT AVAILABLE
48	км	AND AS A RESULT THE PHASE IV VILLAGES LIST FOR PH-IV WERE COMBINED.
49	км	AS PLANS ARE DEVELOPED, THE VILLAGES CAN BE MODELED SEPARATELY.
50	ВА	0.1931
51	LS	92
52	ŲD	0.31
	÷	
	•	
53	KK	E14 HYDROGRAPH FROM VILLAGE 6 DRAINAGE POINT E14
54	KM	CALCULATE RUNOFF FROM SUBBASIN E14
Š5	ВА	.025
56	· LS	92
57	מט	.225
	*	
58	KK	C14
59	KM	COMBINE RUNOFF FROM E14 WITH CENTRAL CHANNEL FLOW (FLOW FROM RT1617 & PH-IV)
60	HC	3
	*	
61	KK	E14-E1
62	КМ	ROUTE FLOW TO E1 ALONG CENTRAL CHANNEL
63	RD	400 .004 .030 TRAP 100 3
64	KK	E1
65	KM	CALCULATE RUNOFF FROM SUBBASIN E1-VILLAGE 5
66 67	•	.0058
68	. nd	92 .135
00	. 00	.135
-		
69	кк	Cl
70	KM	COMBINE RUNOFF FROM E1 WITH CENTRAL CHANNEL FLOW
71	нс	2
	*	*
72	KK	E1-E2
73	KM	ROUTE FLOW TO E2 ALONG CENTRAL CHANNEL
74	RD.	300 .004 .030 TRAP 100 3
_	. *	

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LINE
             KK E2
 75
 76
               KM
                    CALCUALTE RUNOFF FROM SUBBASIN E2-VILLAGE 5
 77
              ВА
                     .003
 78
              LS
                               92
              Œ
 79
                     .118
 80
               ΚK
 81
               KM
                   COMBINE RUNOFF FROM E2 WITH CENTRAL CHANNEL FLOW
              HC
 82
 83
               KK
 84
               KM
                   ROUTE FLOW TO E3 ALONG CENTRAL CHANNEL
 85
               ŔD
                     300
                             .004
                                     .030
                                                     TRAP
                                                              100
 86
              KK
                       E3
 87
              KΜ
                   CALCULATE RUNOFF FROM SUBBASIN E3-VILLAGE 5
 88
              BA
 89
              LS
                               92
              UD
 90
                     .119
 91
              KK
 92
              KM
                   COMBINE RUNOFF FROM E3 WITH CENTRAL CHANNEL FLOW
              HC .
 94
              ĸк
                   E3-E4
              KM
                   ROUTE FLOW TO E4 ALONG CENTRAL CHANNEL
 95
 96
              RD
                             .004
                                   .030
                                                   TRAP
                                                              100
 97
              KK
 98
              KM
                   CALCULATE RUNOFF FROM SUBBASIN E4-VILLAGE 5
 99
              ва
                    .003
              LS
100
                               92
              UD
101
                     .113
102
              KK
103
              КМ
                   COMBINE RUNOFF FROM E4 WITH CENTRAL CHANNEL FLOW
104
              HC
                       2
105
              KK
                    . D10
106
                   CALCULATE RUNOFF FROM SUBBASIN D10
107
              KM
                   SUBBASIN D10 IS LOCATED ALONG DOUBLE DIAMOND PKWY. THE AREA DRAINED IS
108
              KM
                   COMPRISED OF PORTIONS OF VILLAGES 5,6,13,14,15,16 & 17 THAT BORDER THE PKWY.
109
              KM
                   THE D10 SYSTEM IS A PARALLEL STORM DRAIN SYSTEM
110
              KM
                   ALONG DOUBLE DIAMOND PARKWAY THAT DRAINS TO AN OPEN
111
                   CHANNEL ALONG THE SOUTH EDGE OF THE PARK LOCATED IMMEDIATELY SOUTHEAST OF
                   THE INTERSECTION OF CARAT AV. AND DOUBLE DIAMOND PKWY.
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LINE .	ID.	12345678910
113	ВА	.122
114	LS	92
115	(סט	.277
	*	
116	KK	D12
117	KM	CALCULATE RUNOFF FROM SUBBASIN D12-VILLAGE 5
118	BA	0.0166
119	LS	92.
120	UD	0.173
	*	
121	KK	PARK
122	KM	CALCULATE RUNOFF FROM PARK JUST SOUTH OF CARAT AVE
123	· BA	.0078
124	LS	80
125	UD	.14
•	. •	
126	KK	C10PRK
127	KM	COMBINE HYDROGRAPHS FROM PARK, D10, D12 AND CENTRAL CHANNEL
128	HC	4
	•	
129	KK	PK-CAR
130	КМ	ROUTE FLOW TO CARAT AVE ALONG CENTRAL CHANNEL
131	RD	300 .004 .030 TRAP 100 3
132	ZZ	

SCHEMATIC DIAGRAM OF STREAM NETWORK

(--->) DIVERSION OR PUMP FLOW

٠,	(.) CONNECTOR	(<) RETURN OF DIVERTED OR PUMPED FLOW
14	W18RB	•
	• .	
30	. V18-1	9
34	•	. V20
	•	•
	•	
38	•	WET
42	CB WET	
	•	
45	. PH-I	v
	•	•
53	•	. E14
	•	•
58	C14	•
	v .	
61	V E14-E1	
64	. 8	1
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60		
69	C1 V	•
	v	
72	E1-E2	
75	. Е	2
		•
80	C2	
	v v .	
83	E2-E3	
	•	
86	. E	3
	•	
91	C3	
•	· v	

(V) ROUTING

105 . D10

.

121 . PARK

126 C10PRK.....

126 CIUPRK.....

V 129 PK-CAR

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

FLOOD HYDROGRAPH PACKAGE (HEC-1)

JUN 1998

VERSION 4.1

RUN DATE 06APR00 TIME 14:45:40

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616

(916) 756-1104

DOUBLE DIAMOND SUBDIVISION-PROJECT #9908

WHITES CREEK SUBBASIN W18RB-NORTH OF WHITES CREEK BRANCH #3 DIVERSION

ADD PHASE II CHANNEL TO EVALUATE CARAT AVENUE CULVERT

100-YEAR, 24-HOUR MODEL

MODEL INCLUDES DOUBLE DIAMOND DEVELOPMENT PHASE II (VILLAGES 5 & 6 AND PARKS)

, PHASE III (VILLAGES 16, 17, 18, AND 19), AND PHASE IV (VILLAGES 7, 8, 9,

20, 21, 22, AND 23) PLUS WETLAND BETWEEN VILLAGES 18/19 & 20.

USE SUBBASIN AREAS FROM MACKAY & SOMPS

NIMBUS ENGINEERS, RENO, NEVADA

FILENAME: C:\HEC1\9908\CARATDD.DAT

12 IO OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL

IPLOT 0 PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 4 MINUTES IN COMPUTATION INTERVAL

IDATE 1AUG98 STARTING DATE

ITIME 1200 STARTING TIME

NQ 361 NUMBER OF HYDROGRAPH ORDINATES

NDDATE 2AUG98 ENDING DATE NDTIME 1200 ENDING TIME

ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .07 HOURS

TOTAL TIME BASE 24.00 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES

PRECIPITATION DEPTH INCHES

LENGTH, ELEVATION FEET

FLOW CUBIC FEET PER SECOND

STORAGE VOLUME ACRE-FEET

SURFACE AREA ACRES

TEMPERATURE DEGREES FAHRENHEIT

W18RB * WHITES CREEK SUBBASIN W18RB-NORTH BOUNDARY OF WHITES CK MEADOW SUBDIV.

DAMONTE RANCH NORTH OF WHITES CK. BRANCH #3 AND SOUTH OF DOUBLE DIAMOND

13 IN TIME DATA FOR INPUT TIME SERIES

JXMIN 15 TIME INTERVAL IN MINUTES

JXDATE 1AUG98 STARTING DATE

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JXTIME
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1200 STARTING TIME

SUBBASIN RUNOFF DATA

В	Δ

SUBBASIN CHARACTERISTICS

TAREA

.23 SUBBASIN AREA

PRECIPITATION DATA

17 PB	STORM	2.60	BASIN TO	TAL PRECI	PITATION		-			
18 PI	INCREMENTAL	PRECIPITAT	FION PATTE	RN						
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28 LS

SCS LOSS RATE

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STRTL

.35 INITIAL ABSTRACTION

CRVNBR

85.00 CURVE NUMBER

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RTIMP

.00 PERCENT IMPERVIOUS AREA

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29 UD

SCS DIMENSIONLESS UNITGRAPH

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UNIT HYDROGRAPH

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24 END-OF-PERIOD ORDINATES

34.	105.	225.	316.	340.	316.	265.	191.	133.	95.
70.	50.	36.	26.	19.	14.	10.	7.	5	4.
3.	2.	1.	1.						

HYDROGRAPH AT STATION W18RB

TOTAL RAINFALL = 2.60, TOTAL LOSS = 1.34, TOTAL EXCESS = . FLOW TIME MAXIMUM AVERAGE FLOW (HR) (CFS) 6-HR 24-HR 72-HR 24.00-HR 157. 12.20 8. (CFS) 26. 8. 8. (INCHES) 1.024 1.255 1.255 1.255 (AC-FT) 13. 16. 16. 16.

CUMULATIVE AREA =

DOUBLE DIAMOND VILLAGES 18 & 19

.23 SQ MI

SUBBASIN RUNOFF DATA

31 BA

SUBBASIN CHARACTERISTICS

.05 SUBBASIN AREA

PRECIPITATION DATA

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t					U	NIT HYDROG	RAPH				
			,		20 END	-OF-PERIOD	ORDINATES				
1	14.	44.	83.	97.	89.	70.	44.	. 30.	20.	14.	
	9.	6.	4.	3.	2.	1.	1.	1.,	. 0.	0.	
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		HYDROGE	RAPH AT ST	'ATION V	V18-19			, ·			
	•			'							
TOTAL R	AINFALL =	2.60. TO	TAL LOSS	<u> </u>	l, TOTAL E	XCESS =	1.79				
		, 10	2000		-, .v.au E						
PEAK FLOW	TIME .			Maves	MUM AVERAG	יים ארים מיים איים					
(CFS)	(HR)	4	e m				24 :00 ***				
		(070)	6-HR		4-HR	72-HR	24.00-HR	. * .			
58.	12.13	(CFS)	8.		3.	3.	3⁻.				
	•	(INCHES)	1.426		. 784	1.784	1.784	· .			
		(AC-FT)	4.		5.	5.	_. 5.	•			
		CUMULATI	VE AREA =	.05	SQ MI						•
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34 KK	* V2	:O· *	DOUBLE DI	AMOND VII	LAGE 20			•			
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17 PB		STORM	2.60	BASIN TO	TAL PRECI	PITATION				*	
18 PI	INC	REMENTAL P	RECIPITAT	ION PATTE	RN	•		•			
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36 LS

SCS LOSS RATE

STRTL

.17 INITIAL ABSTRACTION

CRVNBR

92.00 CURVE NUMBER

JE. OU CORVE

RTIMP

.00 PERCENT IMPERVIOUS AREA

UD

SCS DIMENSIONLESS UNITGRAPH

TLAG

.21 LAG

UNIT HYDROGRAPH

18 END-OF-PERIOD ORDINATES

15. 50. 84. 88. 72. 46. 29. 19. 12. 5. 3. 2. 1. 1. 1. 0. 0.

HYDROGRAPH AT STATION

V20

TOTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS. = 1.7

TIME PEAK FLOW MAXIMUM AVERAGE FLOW (CFS) (HR) 6-HR 24-HR 72-HR 24.00-HR 12.13 (CFS) 7. 2. 2. 2. (INCHES) 1.426 1.784 1.784 1.784 (AC-FT) 3. 4. 4. 4.

CUMULATIVE AREA = .05 SQ MI

SUBBASIN RUNOFF DATA

BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

17 PB STORM 2.60 BASIN TOTAL PRECIPITATION

| I | NCREMENTAL | PRECIPIT | ATION PATTE | ERN . | | - | | | | |
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0 LS SCS LOSS RATE

STRTL .50 INITIAL ABSTRACTION

CRVNBR 80.00 CURVE NUMBER

.00 .00 .00

RTIMP .00 PERCENT IMPERVIOUS AREA

SCS DIMENSIONLESS UNITGRAPH

TLAG .26 LAG

UNIT HYDROGRAPH
21 END-OF-PERIOD ORDINATES

.00

3. 10. 20. 25. 24. 20. 14. 10. 7. 5. 3. 2. 2. 1. 1. 1. 0. 0. 0. 0.

.00 .00

Ο.

HYDROGRAPH AT STATION WET

2.60, TOTAL LOSS = 1.64, TOTAL EXCESS = OTAL RAINFALL =

EAK FLOW MAXIMUM AVERAGE FLOW TIME (CFS) (HR) 24-HR 72-HR 6-HR 24.00-HR 12.13 (CFS) 1. 0.. 0. 8. 0. (INCHES) .957 .782 .957 . 957 (AC-FT) 1. 1. 1..

> CUMULATIVE AREA = .02 SQ MI

CR WET *

COMBINE W18RB, V18-19, V20, & WET RUNOFF HYDROGRAPHS IN THE WETLAND

BETWEEN VILLAGES 18/19 AND VILLAGE 20

44 HC

HYDROGRAPH COMBINATION

ICOMP .

4 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CE WET

EAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 24-HR 72-HR 6-HR 24.00-HR 266. 12.13 (CFS) 42. 13. 13. 13. (INCHES) 1.125 1.393 1.393 1.393 (AC-FT) 21. 26. 26.

> CUMULATIVE AREA = .35 SQ MI

5 KK

PH-IV *

PHASE IV DOUBLE DIAMOND DEVELOPMENT (VILLAGES 7,8,9,21,22,&23).

VILLAGE 20 WAS MODELED ABOVE WITH FLOW ENTERING THE WETLAND SOUTH OF WILBUR MAY BLVD. DETAILED DRAINAGE PLANS WERE NOT AVAILABLE AND AS A RESULT THE PHASE IV VILLAGES LIST FOR PH-IV WERE COMBINED. AS PLANS ARE DEVELOPED, THE VILLAGES CAN BE MODELED SEPARATELY.

SUBBASIN RUNOFF DATA

SUBBASIN CHARACTERISTICS

TAREA

.19 SUBBASIN AREA

PRECIPITATION DATA

| | STORM | 2.60 | BASIN T | TOTAL PREC | IPITATION | • | | | | |
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| | RTIMP | | | IMPĒRVIOU | IS AREA | | | | | • |
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UNIT HYDROGRAPH
25 END-OF-PERIOD ORDINATES

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 170.
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 271.
 259.
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HYDROGRAPH AT STATION PH-IV

17 PB

18 PI

51 LS

. 52 UD

63.

OTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS = 1.79

PEAK FLOW TIME MAXIMUM AVERAGE FLOW . 6-HR (CFS) (HR) 24-HR 72-HR 24.00-HR . 180. 12.20 (CFS) 30. 9. 9. 9.

(INCHES) 1.426 1.782 1.782 1.782 (AC-FT) 15. 18. 18. 18.

CUMULATIVE AREA = ..19 SQ MI

HYDROGRAPH FROM VILLAGE 6 DRAINAGE POINT E14

CALCULATE RUNOFF FROM SUBBASIN E14

SUBBASIN RUNOFF DATA

55 BA

SUBBASIN CHARACTERISTICS

TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

17 PB

STORM 2.60 BASIN TOTAL PRECIPITATION

18 PI

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.17 INITIAL ABSTRACTION CRVNBR 92.00 CURVE NUMBER .00 PERCENT IMPERVIOUS AREA SCS DIMENSIONLESS UNITGRAPH UD TLAG .22 LAG UNIT HYDROGRÁPH 19 END-OF-PERIOD ORDINATES 29. ' 18. 12: HYDROGRAPH AT STATION TOTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS = 1.79 TIME PEAK FLOW MAXIMUM AVERAGE FLOW (HR) (CFS) 6-HR 24-HR 72-HR 12.13 27. (CFS) 4. 1. 1. 1. (INCHES) 1.426 1.784 1.784 1.784 (AC-FT) 2. 2. CUMULATIVE AREA = .03 SQ MI COMBINE RUNOFF FROM E14 WITH CENTRAL CHANNEL FLOW (FLOW FROM RT1617 & PH-IV) 60 HC HYDROGRAPH COMBINATION ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE HYDROGRAPH AT STATION EAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 6 - HR 24 - HR 72-HR 24.00-HR 12.:13 467. (CFS) 76. 24. 24. 24. (INCHES) 1.240 1.543 1.543 1.543

47.

38.

47.

(AC-FT)

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ROUTE FLOW TO E1 ALONG CENTRAL CHANNEL HYDROGRAPH ROUTING DATA MUSKINGUM-CUNGE CHANNEL ROUTING L 400. CHANNEL LENGTH .0040 SLOPE .030 CHANNEL ROUGHNESS COEFFICIENT .00 CONTRIBUTING AREA SHAPE TRAP CHANNEL SHAPE WD 100.00 BOTTOM WIDTH OR DIAMETER 3.00 SIDE SLOPE COMPUTED MUSKINGUM-CUNGE PARAMETERS COMPUTATION TIME STEP ELEMENT AT.PHA DT DX TIME TO VOLUME MAXIMUM PEAK CELERITY (MIN) (FT) (CFS) (MIN) (IN) MAIN .19 1.60 1.55 200.00 466.80 731.09 INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL .19 1.60 4.00 -464.72 732.00 TUITY SUMMARY (AC-FT) - INFLOW= .4670E+02 EXCESS= .0000E+00 OUTFLOW= .4666E+02 BASIN STORAGE= .8610E-01 PERCENT ERROR=

HYDROGRAPH AT STATION E14-E1

| PEAK FLOW | TIME | | | MAXIMUM AVER | ACE ELON | |
|-----------|-------|-----------|----------|--------------|-------------------|-----------------|
| (CFS) | (HR) | | 6-HR | 24-HR | AGE FLOW
72-HR | 24.00-HR |
| 465. | 12.20 | (CFS) | 76. | 24. | 72-AR
24. | 24.00-HR
24. |
| | | (INCHES) | 1.239 | 1.541 | 1.541 | 1.541 |
| | | (AC-FT) | 38. | 47. | 47. | 47. |
| | | CUMULATIV | E AREA = | .57 SQ MI | • . | |

CALCULATE RUNOFF FROM SUBBASIN E1-VILLAGE 5

SUBBASIN RUNOFF DATA

E14-E1 *

66 BA SUBBASIN CHARACTERISTICS

E1

64 KK

TAREA .01 SUBBASIN AREA

STORM

17 PB

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                 SCS LOSS RATE
67 LS
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                                               INITIAL ABSTRACTION
                       CRVNBR
                                       92.00
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                        RTIMP
                                               PERCENT IMPERVIOUS AREA
                                         .00
68 UD
                 SCS DIMENSIONLESS UNITGRAPH
                         TLAG
                                         .14 LAG
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2.60 BASIN TOTAL PRECIPITATION

UNIT HYDROGRAPH

12 END-OF-PERIOD ORDINATES

0.

15. 16. 10. 5. 3. 1. 1. 0.

HYDROGRAPH AT STATION

5.

E1

TAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS = 1.79

EAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 6 - HR 24.00-HR 24-HR 72-HR 8. 12.07 (CFS) 1. 0. . 0 . ٥.

(INCHES) 1.427 1.785 1.785 0. (AC-FT) 1. 1. CUMULATIVE AREA = .01 SQ MI . C1 * COMBINE RUNOFF FROM E1 WITH CENTRAL CHANNEL FLOW HYDROGRAPH COMBINATION · ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE HYDROGRAPH AT STATION PEAK FLOW TIME ' MAXIMUM AVERAGE FLOW (CFS) (HR) 6-HR 24-HR 72-HR 24.00-HR 12.20 (CFS) 469. 77,. 24. 24. 24. (INCHES) 1.241 1.544 1.544 1.544 47. (AC-FT) 38. 47. 47. CUMULATIVE AREA = .57 SQ MI E1-E2 * ROUTE FLOW TO E2 ALONG CENTRAL CHANNEL HYDROGRAPH ROUTING DATA MUSKINGUM-CUNGE CHANNEL ROUTING 300. CHANNEL LENGTH .0040 SLOPE .030 CHANNEL ROUGHNESS COEFFICIENT .00 CONTRIBUTING AREA CA TRAP CHANNEL SHAPE 100.00 BOTTOM WIDTH OR DIAMETER 3.00 SIDE SLOPE COMPUTED MUSKINGUM-CUNGE PARAMETERS

71 HC

COMPUTATION TIME STEP ELEMENT ALPHA M. DT PEAK TIME TO VOLUME MAXIMUM PEAK CELERITY (MIN) (MIN) (IN)

(FPS)

(CFS) (FT)

MAIN .19 1.60 1.16 300.00 465.88 732.63 1.54 4.32

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .19 1.60 4.00 465.24 732.00 1.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4722E+02 EXCESS= .0000E+00 OUTFLOW= .4720E+02 BASIN STORAGE= .6902E-01 PERCENT ERROR=

HYDROGRAPH AT STATION E1-E2

PEAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 72-HR 6-HR 24-HR 24.00-HR (CFS) 12.20 465. 77. 24. 24. (INCHES) 1.242 1.544 1.544 1.544

CUMULATIVE AREA = .57 SQ MI

38.

* * * * *

18 PI

CALCUALTE RUNOFF FROM SUBBASIN E2-VILLAGE 5

-47.

SUBBASIN RUNOFF DATA

(AC-FT)

77 BA SUBBASIN CHARACTERISTICS

TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

17 PB STORM 2.60 BASIN TOTAL PRECIPITATION

INCREMENTAL PRECIPITATION PATTERN .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 . 00 .00 .00 .00 .00 : 00 . 00 . 00 .00 .00 .00 .00 .00 .00 .00 .00 . 0,0 .00 .00 .00 .00 .00 .00 . .00 .00 .00 .00 .00 . .00 .0,0 .00 .00 .00 .00 .00 .00 . '00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 ..00 . 00 1.00 .00 .00 .00 .00 .00 .00 .00 : 00 ..00 .00 .00 .00 .01 .00 .00 .01 .01 .01 .01 .01 .01 .02 .03 .03 .03 .06 .07 .07 .07

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78 LS

SCS LOSS RATE

STRTL

.17 INITIAL ABSTRACTION

CRVNBR '

92.00 CURVE NUMBER

RTIMP

.00 PERCENT IMPERVIOUS AREA

79 UD

SCS DIMENSIONLESS UNITGRAPH

TLAG

12 LA

UNIT HYDROGRAPH

11 END-OF-PERIOD ORDINATES

i. 9. 8. 4. 2. 1. 0. 0. 0. 0

HYDROGRAPH AT STATION

E2

TOTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS = 1.79

PEAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 6-HR . 24-HR 72-HR 24.00-HR 0. 12.00 . (CFS) 0. 0. 0. (INCHES) 1.427 1.786 1.786 1.786 (AC-FT) 0. 0. 0.

CUMULATIVE AREA = .00 SQ MI

80 KK · * C2

COMBINE RUNOFF FROM E2 WITH CENTRAL CHANNEL FLOW

HC

HYDROGRAPH COMBINATION

ICOMP

2 NUMBER OF HYDROGRAPHS TO COMBINE

...

HYDROGRAPH AT STATION

C2

TIME MAXIMUM AVERAGE FLOW as) (HR) 6 - HR 24-HR 72-HR 24.00-HR 467. 12.20 (CFS) 77. 24. 24. . 24. (INCHES) 1.242 1.545 1.545 1.545 (AC-FT) 38. 47. 47.

CUMULATIVE AREA =

.58 SQ MI

83 KK * E2-E3

ROUTE FLOW TO E3 ALONG CENTRAL CHANNEL

HYDROGRAPH ROUTING DATA

85 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L 300. CHANNEL LENGTH

S .0040 SLOPE

N .030 CHANNEL ROUGHNESS COEFFICIENT

CA .00 CONTRIBUTING AREA

SHAPE TRAP CHANNEL SHAPE

WD 100.00 BOTTOM WIDTH OR DIAMETER

Z 3.00 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

COMPUTATION TIME STEP

| | | | | 0101 | | | | |
|---------|-------|------|-------|--------|--------|---------|--------|----------|
| ELEMENT | ALPHA | M | DT | DX . | PEAK | TIME TO | VOLUME | MAXIMUM |
| | | | | | • | PEAK | | CELERITY |
| | | | (MIN) | (FT) | (CFS) | (MIN) | (IN) | (FPS) |
| | | | • | | - | | | |
| MAIN | .19 | 1.60 | 1.16 | 300.00 | 463.23 | 732:45 | 1.54 | 4.31 |

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .19 1.60 4.00 461.44 732.00 1.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4749E+02 EXCESS= .0000E+00 OUTFLOW= .4747E+02 BASIN STORAGE= .7183E-01 PERCENT ERROR= -.1

HYDROGRAPH AT STATION E2-E3

| • | K FLOW | TIME | | | MAXIMUM AVE | RAGE FLOW | |
|---|--------|-------|----------|-------|-------------|-----------|----------|
| 1 | :FS) | (HR) | | 6-HR | 24-HR | 72-HR | 24.00-HR |
| ŀ | 461. | 12.20 | - (CFS) | 77. | 24. | 24. | 24. |
| , | | | (INCHES) | 1.243 | 1.544 | 1.544 | 1.544 |
| | | | (AC-FT) | 38. | 47 | 47. | 47. |

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CUMULATIVE AREA = .58 SQ MI
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* 86 KK * E3

18 PI

CALCULATE RUNOFF FROM SUBBASIN E3-VILLAGE 5

SUBBASIN RUNOFF DATA

88 BA SUBBASIN CHARACTERISTICS

TAREA

.00 SUBBASIN AREA

PRÉCIPITATION DATA

17 PB STORM 2.60 BASIN TOTAL PRECIPITATION

INCREMENTAL PRECIPITATION PATTERN
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SCS LOSS RATE

STRTL CRVNBR

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.17 INITIAL ABSTRACTION

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RVNBR 92.00 CURVE NUMBER

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RTIMP .00 PERCENT IMPERVIOUS AREA

90 UD

З.

SCS DIMENSIONLESS UNITGRAPH

TLAG

.12 LAG

UNIT HYDROGRAPH

11 END-OF-PERIOD ORDINATES

0.

3. 8. 7. 3. 2. 1. 0. 0.

HYDROGRAPH AT STATION

,

TOTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS = 1.79

 PEAK FLOW
 TIME
 MAXIMUM AVERAGE FLOW

 (CFS)
 (HR)
 6-HR
 24-HR
 72-HR
 24.00-HR

12.00 (CFS) 0. 0. 0. 0. 0. (INCHES) 1.427 1.786 1.786

(AC-FT) 0. 0. 0. 0.

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CUMULATIVE AREA = .00 SQ MI

кк • сз •

COMBINE RUNOFF FROM E3 WITH CENTRAL CHANNEL FLOW

93 HC HYDROGRAPH COMBINATION

ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION C3

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 24.00-HR

463. 12.20 (CFS) 77. 24. 24. 24.

(INCHES) 1.243 1.545 1.545 1.545

(AC-FT) 38. 48. 48. 48.

CUMULATIVE AREA = .58 SQ MI

4 KK * E3-E4 *

94 KK * E3-E4 *

HYDROGRAPH ROUTING DATA

| 3D | MUSKINGUM-CUNGE | CHANNEL | ROUTING | |
|----|-----------------|---------|---------|------|
| | T | 260 | CHANNET | 7 00 |

360. CHANNEL LENGTH

Ś .0040 SLOPE

.030 CHANNEL ROUGHNESS COEFFICIENT

CA .00 CONTRIBUTING AREA

TRAP CHANNEL SHAPE · WD 100.00 BOTTOM WIDTH OR DIAMETER

3.00 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

COMPUTATION TIME STEP

| ELEMENT ` | ALIPHA | M | DT | DX | PEAK | TIME TO | VOLUME | MUMIXAM | |
|-----------|--------|------|-------|--------|--------|---------|--------|----------|--|
| | | | | | | PEAK | | CELERITY | |
| • | | | (MIN) | (FT) | (CFS) | (MIN) | (IN) | (FPS) | |
| * | 0 | | | | | | | | |
| MAIN | .19 | 1.60 | 1.40 | 360:00 | 460.01 | 733.94 | 1.54 | 4.30 | |

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

454.28 736.00 1.60 4.00 MAIN .19

ONTINUITY SUMMARY (AC-FT) - INFLOW= .4772E+02 EXCESS= .0000E+00 OUTFLOW= .4769E+02 BASIN STORAGE= .8885E-01 PERCENT ERROR=

HYDROGRAPH AT STATION E3-E4

| PEAK FLOW | TIME | | | MAXIMUM AVE | RAGE FLOW | • |
|-----------|-------|----------|-------|-------------|-----------|----------|
| (CFS) | (HR) | | 6-HR | 24-HR | 72-HR | 24.00-HR |
| 454. | 12.27 | (CFS) | 77. | 24. | 24. | 24. |
| | | (INCHES) | 1.243 | 1.545 | 1.545 | 1.545 |
| • | * | (AC-FT) | 38 | . 48 | 4.9 | . 48 |

CUMULATIVE AREA =

CALCULATE RUNOFF FROM SUBBASIN E4-VILLAGE 5

SUBBASIN RUNOFF DATA

97 KK

BA

SUBBASIN CHARACTERISTICS

.00 SUBBASIN AREA

PRECIPITATION DATA

2.60 BASIN TOTAL PRECIPITATION STORM

| 18 PI | INCREMENTAL | PRECÍPITA | TION PATTE | RN | | | | | | • |
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| 100 LS | SCS LOSS RATE | | | | | - | | | | |
| , | STRTL | .17 | | ABSTRACTIO | N | | | | | |
| • | CRVNBR | 92.00 | CURVE NU | MBER . | | | | | | |
| 1 | RTIMP | | PERCENT | IMPERVIOUS | AREA | | | | | • |
| • | | | | | | • | | | | |
| 101 UD | SCS DIMENSIONLE | ESS UNITGR | APH | | | - | - | ÷ | | |
| • | TLAG | .11 | LAG | | | | | | | |
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| | | | | UN | IT HYDROGRA | APH | | | | |
| · | • | | | 10 END- | OF-PERIOD (| ORDINATES | | | | |
| | 4. 10. | 8. | 4. | . 2. | 1. | 0. | 0. | 0. | 0. | |
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HYDROGRAPH AT STATION

TOTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS = 1.79

PEAK FLOW TIME MAXIMUM AVERAGE FLOW CFS) (HR) 6-HR 24-HR 72-HR 24.00-HR 12.00 (CFS) ٥. 0. 0. . 0. 1.786 (INCHES) 1.427 1.786 1.786 (AC-FT) Ó. 0. 0. .0.

CUMULATIVE AREA = .00 SQ MI

COMBINE RUNOFF FROM E4 WITH CENTRAL CHANNEL FLOW HYDROGRAPH COMBINATION ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE HYDROGRAPH AT STATION PEAK FLOW TIME MAXIMUM AVERAGE FLOW (HR) (CFS) 6-HR 24-HR 72-HR 24.00-HR 12.27 (CFS) 455. 78. 24. 24. 24 . (INCHES) 1.244 1.546 1.546 1.546 (AC-FT) 39. 48. 48. CUMULATIVE AREA = .58 SQ MI CALCULATE RUNOFF FROM SUBBASIN D10 SUBBASIN D10 IS LOCATED ALONG DOUBLE DIAMOND PKWY. THE AREA DRAINED IS COMPRISED OF PORTIONS OF VILLAGES 5,6,13,14,15,16 & 17 THAT BORDER THE PKWY. THE D10 SYSTEM IS A PARALLEL STORM DRAIN SYSTEM ALONG DOUBLE DIAMOND PARKWAY THAT DRAINS TO AN OPEN CHANNEL ALONG THE SOUTH EDGE OF THE PARK LOCATED IMMEDIATELY SOUTHEAST OF THE INTERSECTION OF CARAT AV. AND DOUBLE DIAMOND PKWY. SUBBASIN RUNOFF DATA SUBBASIN CHARACTERISTICS TAREA .12 SUBBASIN AREA PRECIPITATION DATA STORM 2.60 BASIN TOTAL PRECIPITATION. INCREMENTAL PRECIPITATION PATTERN .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00

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| SCS LOSS RATE | | | | | | - | | ; | |
| STRTL | .17 | TNITMENT | ABSTRACTIO | | | | | | |
| CRVNBR | 92.00 | CURVE NU | | | | • | | | |
| RTIMP | .00 | | IMPERVIOUS | 2 - 3 0 0 3 | | | | • | |
| KIIII | | FERCENT | IMPERVIOUS | AREA . | | | | | |
| SCS DIMENSION | LESS UNITGR | АРН | | | | | • | | |
| TLAG | .28 | LAG | | | ,* | | | | |
| • | | | | | | , | | | • |
| | | | | *** | | | | • | |
| | | | • | | | | | | |
| | | | UÌ | IIT HYDROGR | АРН | | | | |

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|---|----------------------------|--|--|
| | • . | | |
| | UNIT HYDROGRAPH | | |
| • | 23 END-OF-PERIOD ORDINATES | | |

| 22. | 68. | 139. | 183. | 189. | 165. | 128. | 85 | 60. · | 43. |
|-----|-----|------|------|------|------|------|------|-------|-----|
| 30. | 21. | 15. | 10. | 7. | 5. | 4. | . 3. | 2. | 1. |
| 1. | 1. | 0. | | | | - | | • | |

HYDROGRAPH AT STATION TOTAL RAINFALL = 2.60, TOTAL LOSS = .81, TOTAL EXCESS =

114. LS

| PEAK FLOW | TIME | | | MAXIMUM AVE | AGE FLOW | |
|-----------|-------|----------|-------|-------------|----------|----------|
| (CFS) | (HR) | | 6'∸HR | 24-HR | 72-HR | 24.00-HR |
| 119. | 12.13 | (CFS) | 19. | 6. | 6. | 6. |
| | | (INCHES) | 1.426 | 1.783 | 1.783 | 1.783 |
| 1 | | (AC-FT) | 9. | 12. | 12. | 12. |

CUMULATIVE AREA =

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116 KK * D12
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18 PI

· CALCULATE RUNOFF FROM SUBBASIN D12-VILLAGE 5

SUBBASIN RUNOFF DATA

118 BA SUBBASIN CHARACTERISTICS

TAREA

.02 SUBBASIN AREA

PRECIPITATION DATA

17 PB STORM 2.60 BASIN TOTAL PRECIPITATION

INCREMENTAL PRECIPITATION PATTERN .00 .00 .00 .00 .00 . 00 .00 .00 .00 .00 .00 .00 .00 .00 .00

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.17 INITIAL ABSTRACTION

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CRVNBR 92.00 CURVE NUMBER

RTIMP .00 PERCENT IMPERVIOUS AREA

SCS DIMENSIONLESS UNITGRAPH

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SCS LOSS RATE

UD

TLAG .17 LAG

15 END-OF-PERIOD ORDINATES

8. 29. 34. 39. 21. 12. 1. - 1.. ٥.

2.

. HYDROGRAPH AT STATION

TOTAL RAINFALL = 2.60, TOTAL LOSS = 81, TOTAL EXCESS = 1.79

PEAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) · (HR) 6-HR 24-HR 72 - HR 24.00-HR 20. 12.07 (CFS) 3. 1. (INCHES) 1.427 1.785 1.785 1.785 (AC-FT)

> CUMULATIVE AREA = .02 SQ MI

121 KK PARK

BA

CALCULATE RUNOFF FROM PARK JUST SOUTH OF CARAT AVE

.00

.00

SUBBASIN RUNOFF DATA

SUBBASIN CHARACTERISTICS

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..00

TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

17 PB STORM 2.60 BASIN TOTAL PRECIPITATION

INCREMENTAL PRECIPITATION PATTERN .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 - 00 ..00 .00 .00 .00 .00 .00 .00. .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 . 00 .00 .00 .00 .00 .00 . 00 .00 -.00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 . 00 . 00' .00 .,00 .00 .00 .00 .00 .00 ..00 .00 .01 .01 .01 .01 .01 .01 .01 .02 .03 .07 .07 .03 .03 .06 .07 .01 ..01 .01 .01 .01 .01 .0i .01 .01 .01 .01 .00 .00 .00 .01 . 00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .0000 .00 -00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 .00 . 0,0 .00 .00 .00 .00 .00 .00 .00 .00 .00

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| | | .00 | .00 | .00 | .00 | .00 | .00 | .00 | | |
| | | | | | | | | | • | |
| 24 LS | scs | LOSS RATE | | | • | • | | | | |
| | | STRTL | .50 | INITIAL | ABSTRACTIO | NC | | - | | |
| | | CRVNBR | 80.00 | CURVE N | UMBER | | | | | |
| | | RTIMP | .00 | PERCENT | IMPERVIOU: | S AREA | | • | | |
| | | | | | | | | • | | |
| 25 UD | SCS | DIMENSIONLE | SS UNITGR | APH | | | | | | |
| • • | | TLAG | .14 | LAG | | | • | | | |
| | | • | | | | | • | | | - |
| | • | • | | | | *** | | • | | |
| • | | | | | | | | | | |
| | | | | | tn | NIT HYDROGR | RAPH | | | |
| | | | | | | -OF-PERIOD | | | | |
| | 6. | 20. | 21. | 1.4 | 7. | | | | | • |
| • | 0. | 0. | 21. | . 14. | /. | 4. | 2. | 1. | 1. | 0. |
| | 0. | 0. | | | | | | | | |
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| | | | | | | | | · | | |
| | | HYDROGR | APH AT ST | ATION | PARK | | | | | |
| | | | | | | | | | | |
| TOTAL F | AINFALL = | 2.60, TO | TAL LOSS | = 1.64 | , TOTAL EX | CESS = | . 96 | | • | |
| | - | | | | | ٠ | | • | | |
| K FLOW | TIME | | | MAXIN | MUM AVERAGI | FLOW | | • | | |
| (CFS) | (HR) | | 6-HR | . 24 | -HR | 72-HR | 24.00-HR | | • | |
| 6. | 12.07 | (CFS) | 1. | | 0. | 0. | 0. | | | |
| _ | | (INCHES) | . 783 | • | . 958 | .958 | . 958 | | | |
| • | | (AC-FT) | 0. | - | 0. | 0. | 0. | | | |
| | | | | | | | | | | |
| | • | CUMULATIV | /E AREA = | .01 | SQ MI | | | | | |
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| 6 KK | * C10P | RK * | | | | | | | • | |
| | • | * . | | | | | | | | |
| | ******* | ***** | | | | | • | | | |
| _ | | COMBIN | E HYDROGI | RAPHS FRO | M PARK, DI | 0, D12 AND | CENTRAL C | HANNEL | | |
| | • | | | | • | | | | | |
| 8 HC . | HYDR | OGRAPH COMBI | NATION | | • | | | | | |
| | | ICOMP | | NUMBER C | F HYDROGPA | PHS TO COM | BINE | • | | • |
| | | | • | | | | | | | |

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HYDROGRAPH AT STATION C10PRK

124 LS

125 UD

126 KK

28 HC

PEAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 6 - HR 72-HR 24.00-HR 24-HR 591. 12.20 (CFS) 100. 31. 31. 31.

(INCHES) 1.273 1.585 1.585 1.585 (AC-FT) 49. 62. 62. 62.

CUMULATIVE AREA = .73 SQ MI

PK-CAR *

ROUTE FLOW TO CARAT AVE ALONG CENTRAL CHANNEL

HYDROGRAPH ROUTING DATA

131 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L 300. CHANNEL LENGTH
S .0040 SLOPE

N .030 CHANNEL ROUGHNESS COEFFICIENT

CA .00 CONTRIBUTING AREA

SHAPE TRAP CHANNEL SHAPE

WD 100.00 BOTTOM WIDTH OR DIAMETER

Z 3.00 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

COMPUTATION TIME STEP

ELEMENT ALPHA M DT DX PEAK TIME TO VOLUME MAXIMUM PEAK CELERITY (MIN) · (FT) (CFS) (MIN) (IN) (FPS) MAIN .19 1.60 1.06 300.00 587.97 733.19

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .19 1.60 4.00 583.23 732.00 1.58

CONTINUITY SUMMARY (AC-FT) - INFLOW= .6156E+02 EXCESS= .0000E+00 OUTFLOW= .6153E+02 BASIN STORAGE= .8385E-01 PERCENT ERROR= -.

HYDROGRAPH AT STATION PK-CAR

PEAK FLOW TIME MAXIMUM AVERAGE FLOW (CFS) (HR) 6-HR 72-HR 24-HR 24.00-HR 583. 12.20 31. (CFS) 100. 31. 31. (INCHES) 1.273 1.584 1.584 1.584 (AC-FT) 49. 62. 62. 62.

CUMULATIVE AREA = .73 SQ MI

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

| OPERATION | STATION | PEAK
FLOW | TIME OF | AVERAGE
6-HOUR | FLOW FOR MAXI | MUM PERIOD , | BASIN | MAXIMUM | TIME OF |
|---------------|---------|--------------|---------|-------------------|---------------|--------------|-------|---------|-----------|
| | | 120" | · · | 0-HOOK | 24-HOOK | 72-ROUR | AREA | STAGE | MAX STAGE |
| HYDROGRAPH AT | W18RB | 157. | 12.20 | 26. | 8. | 8. | . 23 | | |
| HYDROGRAPH AT | V18-19 | 58. | 12.13 | 8. | 3. | . з. | .05 | | |
| HYDROGRAPH AT | V20 | 50. | 12.13 | 7. | 2. | 2. | . 05 | | |
| HYDROGRAPH AT | WET | 8. | 12.13 | 1. | 0. | 0. | . 02 | | |
| 4 COMBINED AT | CB WET | 266. | 12.13 | 42. | 13. | 13. | .35 | | |
| HYDROGRAPH AT | PH-IV | 180. | 12.20 | 30. | 9. | 9. | .19 | | |
| HYDROGRAPH AT | E14 | 27. | 12.13 | 4. | 1. | 1. | .03 | - | |
| 3 COMBINED AT | C14 | 467. | 12.13 | 76. | 24. | 24. | .57 | | |
| ROUTED TO | E14-E1 | 465. | 12.20 | 76. | 24. | 24. | . 57 | | |
| HYDROGRAPH AT | E1 | 8. | 12.07 | 1. | 0. | , o. | .01 | | |
| 2 COMBINED AT | Ċ1 | 469. | 12.20 | 77. | 24. | 24. | . 57 | - | |
| ROUTED, TO | E1-E2 | 465. | 12.20 | 77. | 24. | 24. | .57 | | |
| HYDROGRAPH AT | E2 | 4. | 12.00 | 0. | 0. | . 0. | .00 | | |
| 2 COMBINED AT | C2 | 467. | 12.20 | 77. | 24. | 24. | .58 | - | |
| ROUTED TO | E2-E3 | 461. | 12.20 | .77. | 24. | 24. | .58 | | |
| HYDROGRAPH AT | E3 | 3., | 12.00 | 0. | 0. | 0. | .00 | | |
| 2 COMBINED AT | C3 | 463 | 12.20 | 77. | 24. | 24. | . 58 | | |
| ROUTED TO | E3-E4 | 454. | 12.27 | 77. | 24. | 24. | .58 | | |
| HYDROGRAPH AT | E4 | à. | 12.00 | 0. | 0. | ٠٥. | .00 | | |
| 2 COMBINED AT | C4 | 455. | 12.27 | 78. | 24. | 24. | . 58 | • | |
| HYDROGRAPH AT | D10 | 119 | 12.13 | 19. | 6. | 6. | . 12 | | • |
| HYDROGRAPH AT | D12 | 20. | 12.07 | 3 | 1. | 1. | . 02 | | |
| HYDROGRAPH AT | PARK | 6. | 12.07 | 1. | ó. | 0. | ,01 | | • |
| 4 COMBINED AT | Cloprk | . 591. | 12.20 | 100. | 31. | 31. | . 73 | | |
| ROUTED TO | PK-CAR | 583. | 12.20 | 100. | 31. | 31. | .73 | | |
| | | | | | | | • | | |

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

INTERPOLATED TO

| _ | ISTAQ | ELEMENT | DT | · PEAK | TIME TO | VOLUME | DΤ | INTERPO | LATED TO N INTERVAL TIME TO | VOLUME | | |
|------------|---------|-----------|------------|---------------|--------------|------------|----------------|------------|-----------------------------|-------------------|--------|---|
| | | | | - | PEAK | V 0201.2 | | | PEAK | VOLONIZ | | |
| | • | | (MIN) | (CFS) | (MIN) | (IN) | (MIN) | CFS) | (MIN) | (IN) | | |
| | E14-E1 | MANE | 1.55 | 466.80 | 731.09 | 1.54 | 4.00 | 464.72 | 732.00 | 1.54 | | |
| CONTINUITY | SUMMARY | (AC-FT) - | INFLOW= .4 | 670E+02 E | KCESS= .0000 | E+00 OUTFL | OW= .4666
: | E+02 BASIN | STORAGE= | .8610E-01 PERCENT | ERROR= | 1 |
| 1 | E1-E2 | MANE | 1.16 | 465.88 | 732.63 | 1.54 | 4.00 | 465.24 | 732.00 | 1.54 | | |
| CONTINUITY | SUMMARY | (AC-FT) - | INFLOW= .4 | 722E+02 EX | (CESS≃ .0000 | E+00 OUTFL | O₩= .4720 | E+02 BASIN | STORAGE= | .6902E-01 PERCENT | ERROR= | 1 |
| | E2-E3 | MANE | 1.16 | 463.23 | 732.45 | 1.54 | 4.00 | 461.44 | 732.00 | 1.54 | • | |
| CONTINUITY | SUMMARY | (AC-FT) - | INFLOW= .4 | 749E+02 EX | (CESS= .0000 | E+00 OUTFL | O₩ = .4747 | E+02 BASIN | STORAGE= | .7183E-01 PERCENT | ERROR= | 1 |
| | E3-E4 | · MANE | 1.40 | 460.01 | 733.94 | 1.54 | 4.00 | 454.28 | 736.00 | 1.54 | | |
| CONTINUITY | SUMMARY | (AC-FT) - | INFLOW= .4 | 772E+02 EX | (CESS= .0000 | E+00 OUTFL | OW= .4769 | E+02 BASIN | STORAGE= | .8885E-01 PERCENT | ERROR= | 1 |
| -
1 | PK-CAR | MANE | 1.06 | 587.97 | 733.19 | 1.58 | 400 | 583.23 | 732.00 | 1.58 | | |
| CONTINUITY | SUMMARY | (AC-FT) - | INFLOW= .6 | 156E+02 EX | (CESS= .0000 | E+00 OUTFL | DW= .6153 | E+02 BASIN | STORAGE= | .8385E-01 PERCENT | ERROR= | 1 |

*** NORMAL END OF HEC-1 ***

APPENDIX B Hydraulic Analysis HEC-RAS Modeling Results

Option #1:

Five, 5-foot Diameter RCP Culverts at Carat Avenue

Project: ddcarat1.prj

Project Title: Double D-Carat Ave w/ 5 RCP Culverts

Project Directory: m:\jobs\9908\hydro\ras\wetland-CaratAv\

roject Plans

Plan (current)

Title: Central Chan. to Carat Ave-5 RCP Culverts

Short ID: DDCarat-5RCP

File: m:\jobs\9908\hydro\ras\wetland-CaratAv\ddcarat1.p01

Geometry:

Title:Central Chan. to Carat Av.-5 RCP culverts

File:m:\jobs\9908\hydro\ras\wetland-CaratAv\ddcarat1.g02

Flow:

Title:Wetland 300 base + 400 upstr.of Carat

File:m:\jobs\9908\hydro\ras\wetland-CaratAv\ddcarat1.f01

Current Plan Statistics

Number of:

Cross Sections = 147

User Input XSs = 50

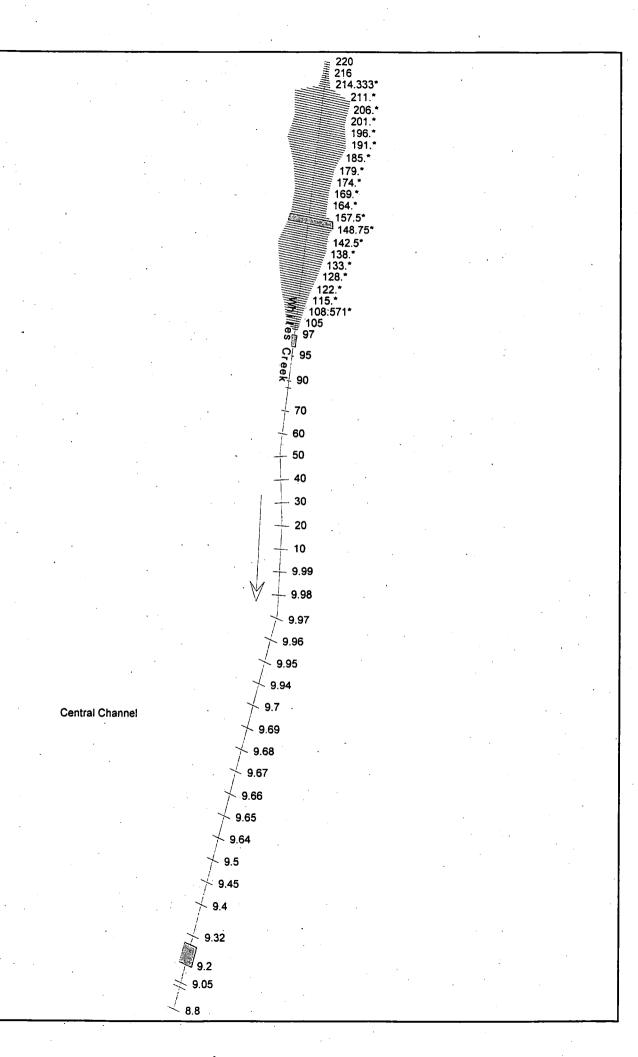
Interpolated = 97

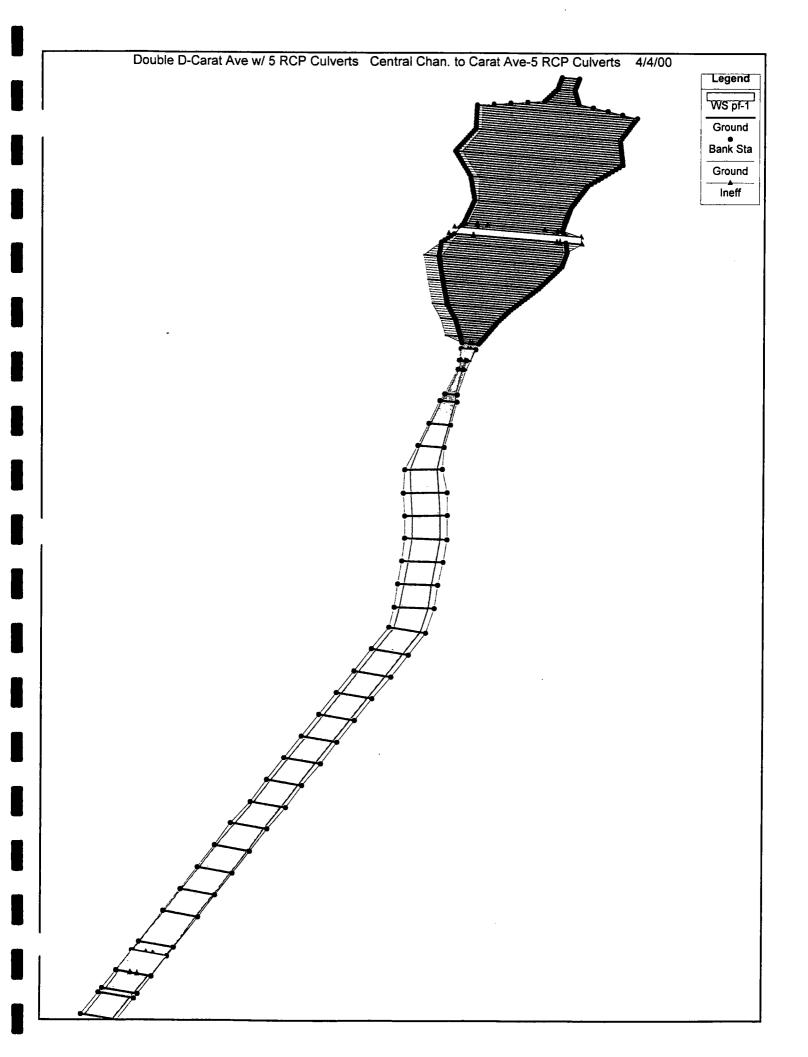
Culverts = 2

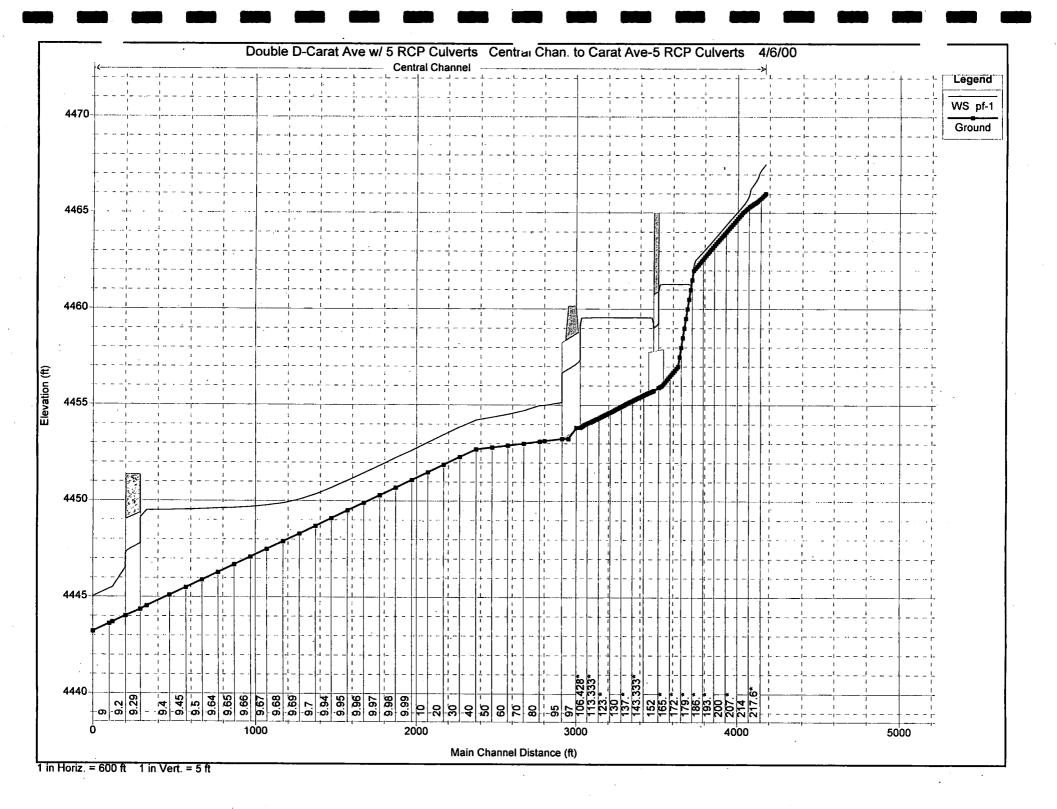
Bridges = 0

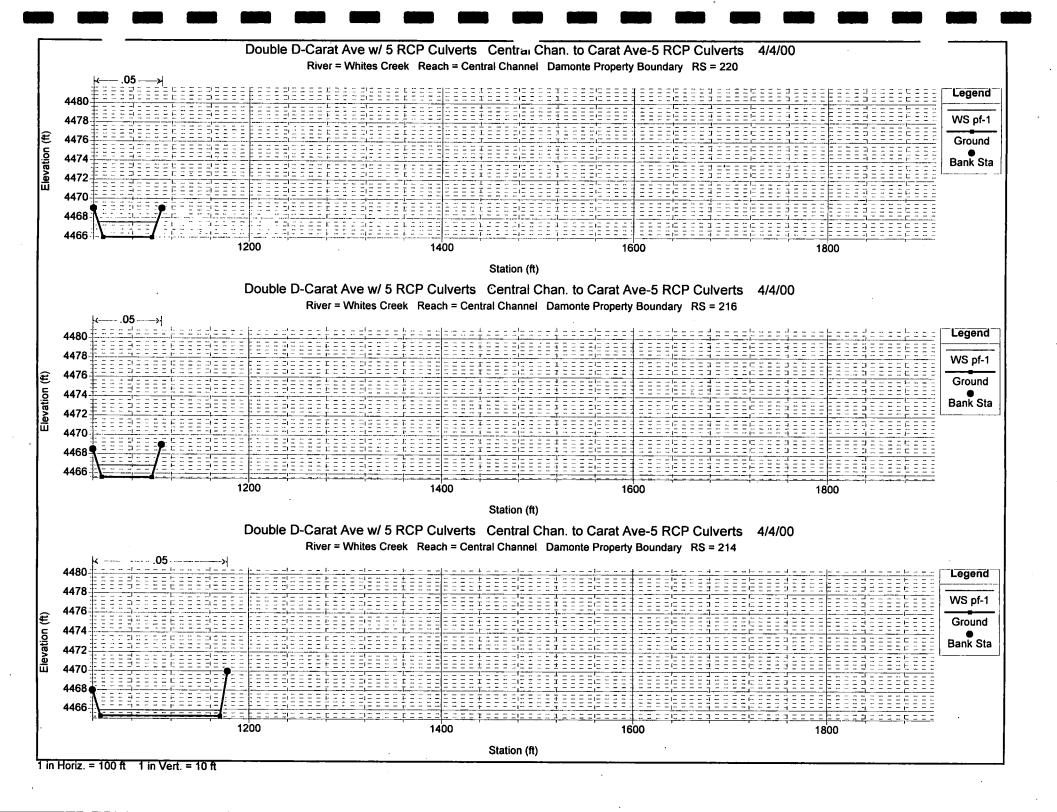
Mulitple Openings = 1

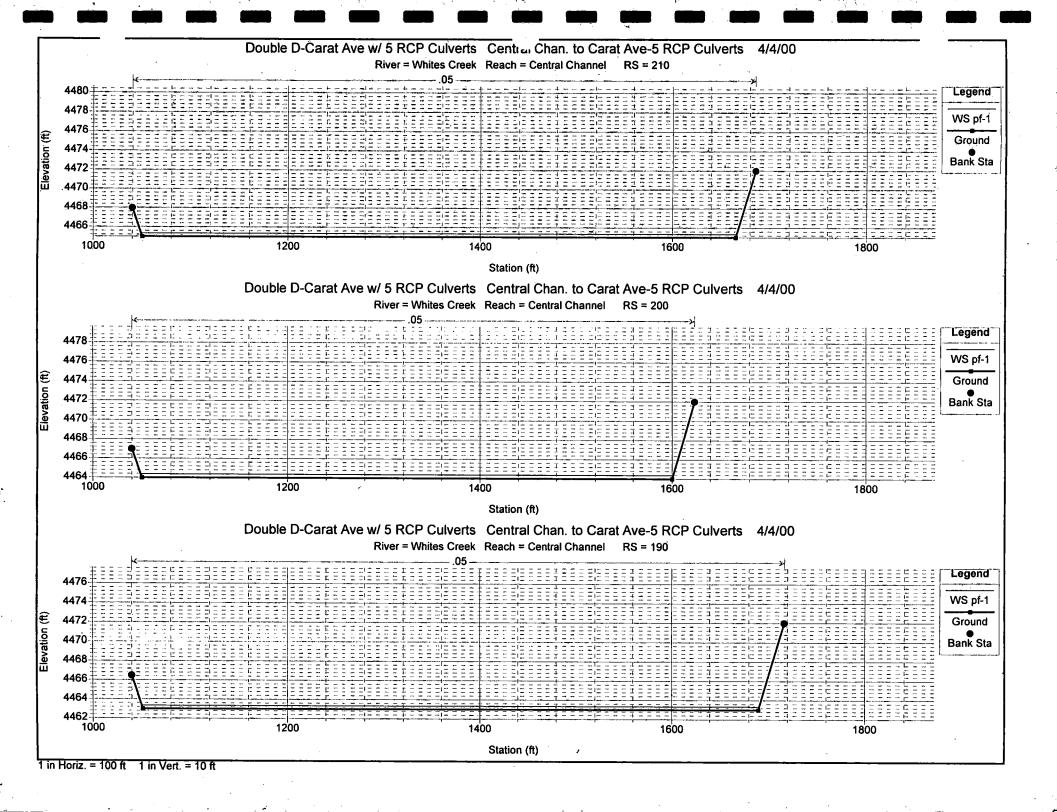
Inline Weirs = 0

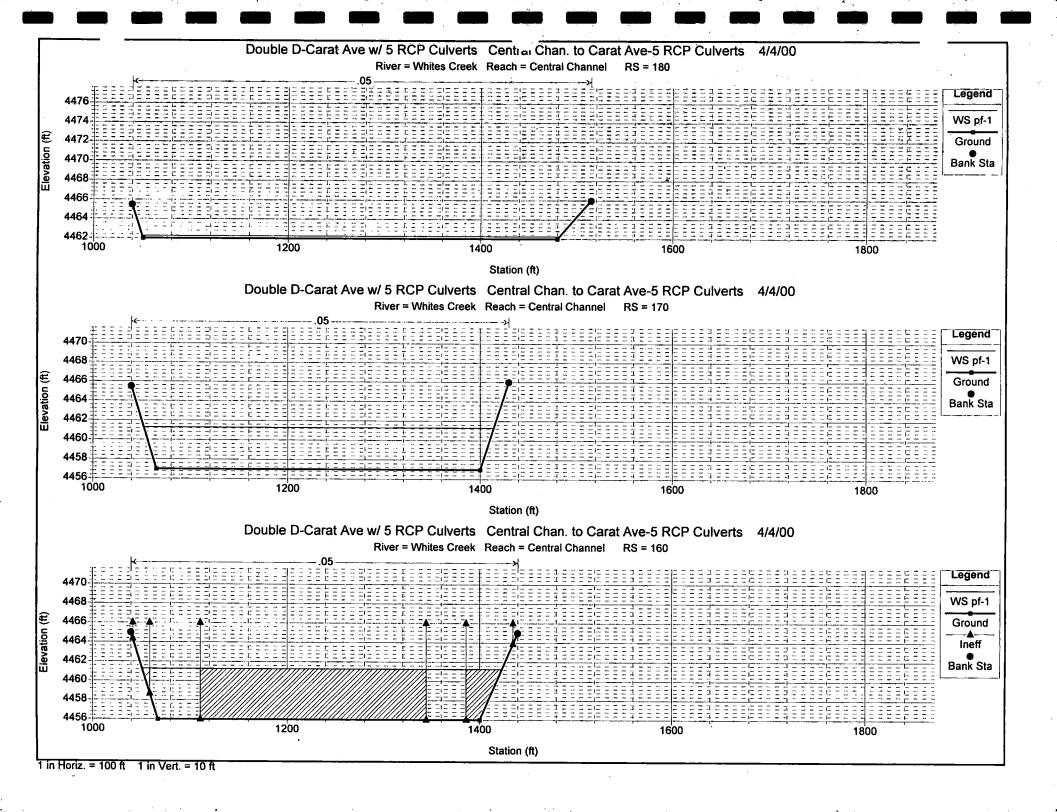


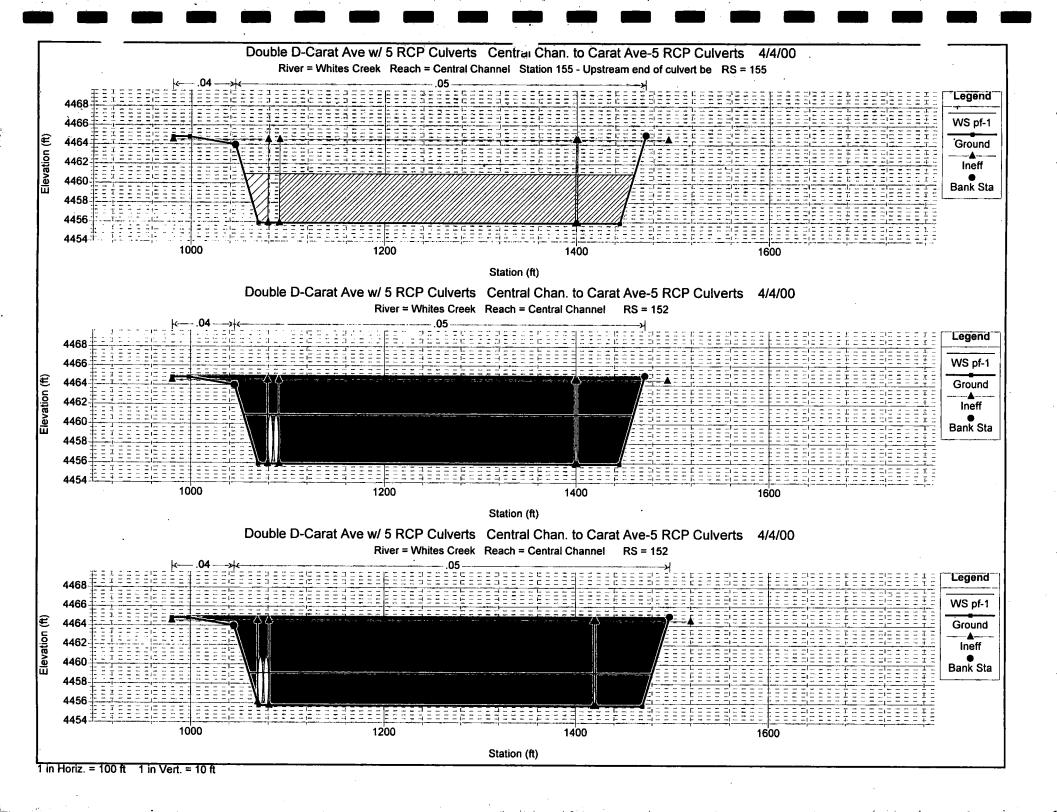


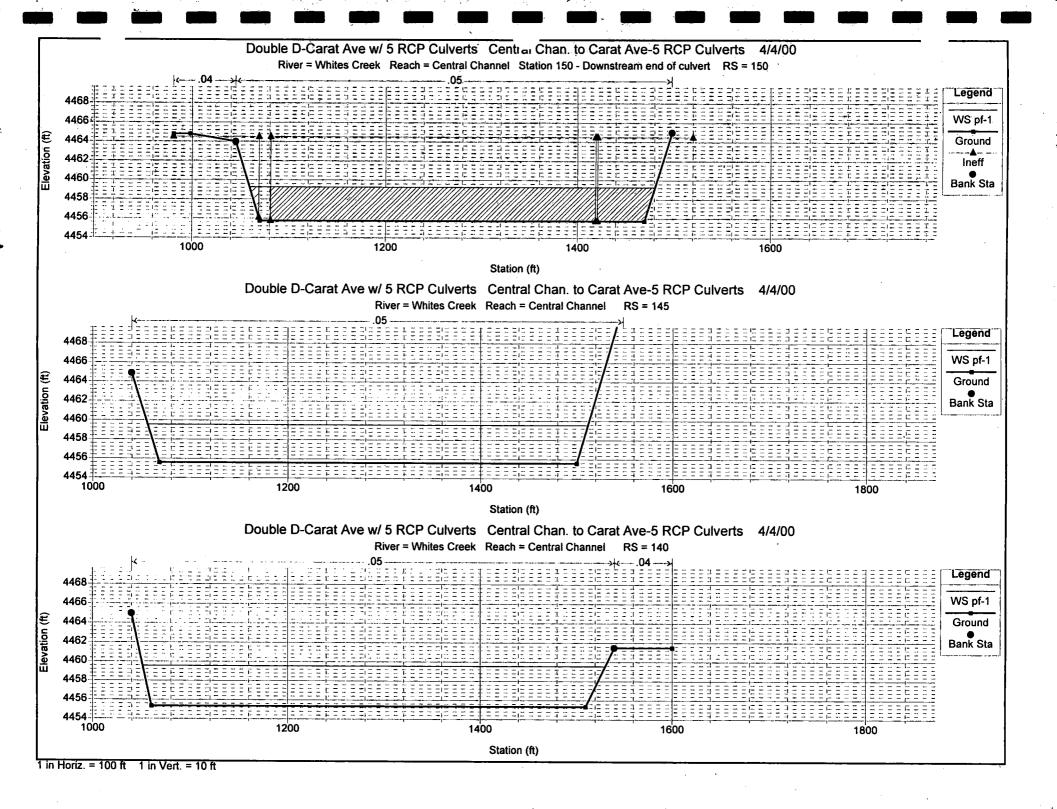


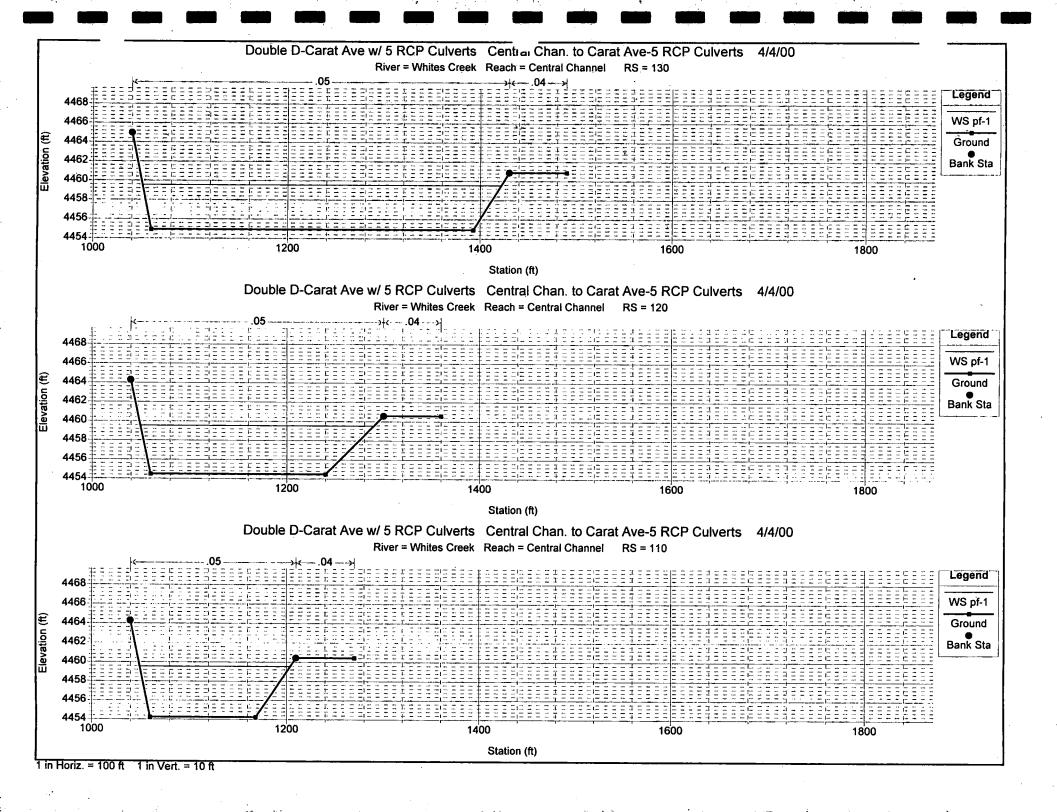


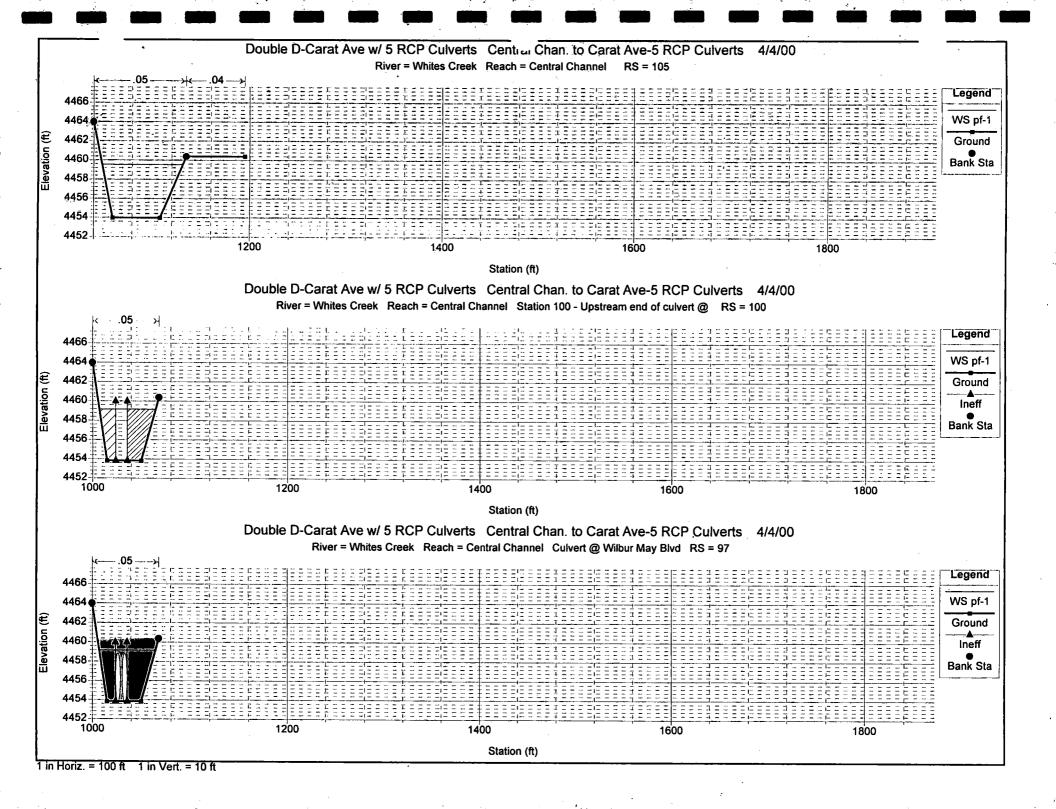


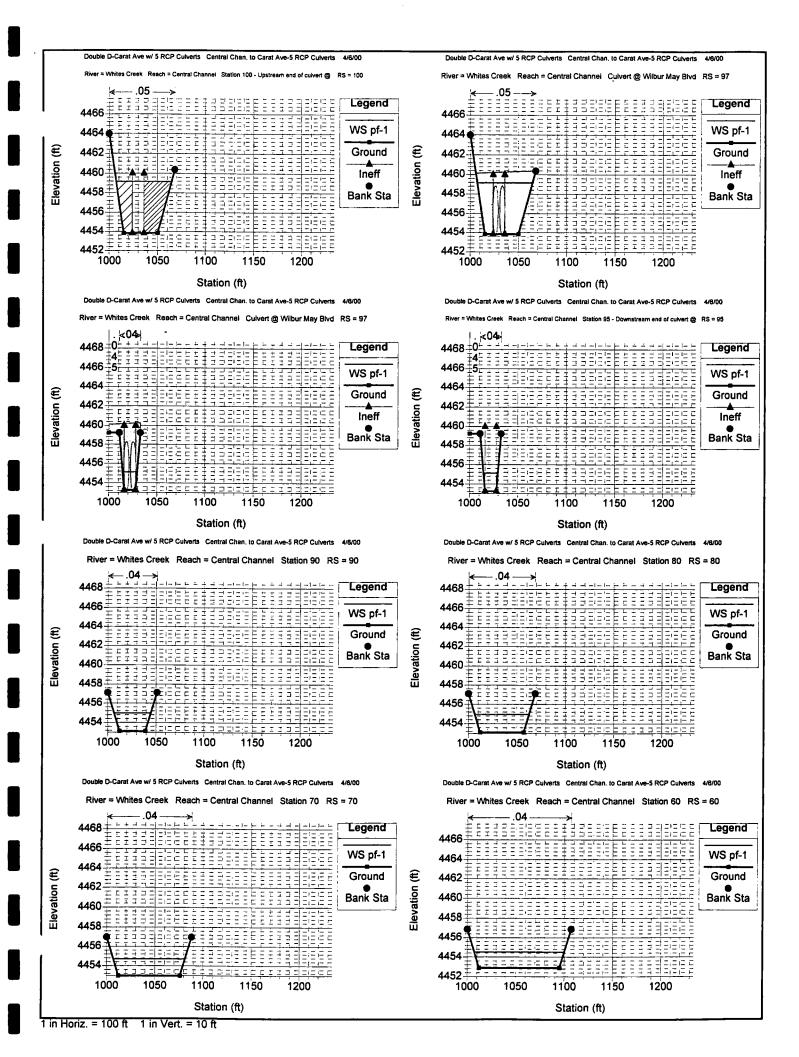


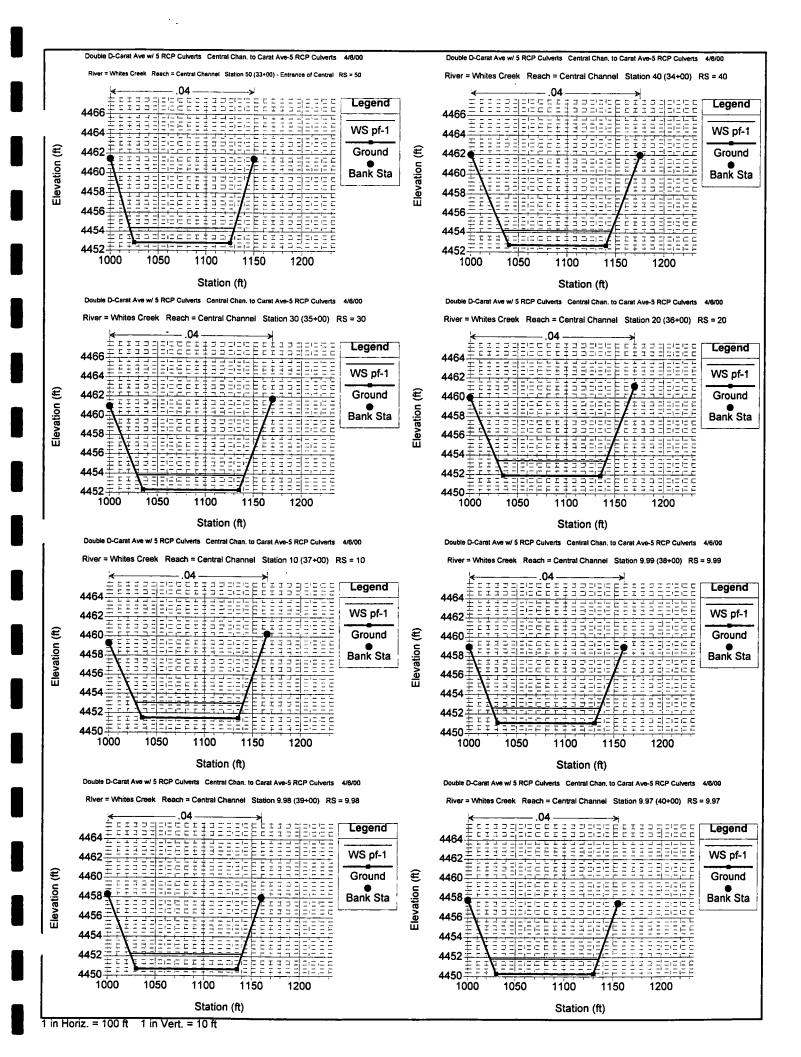


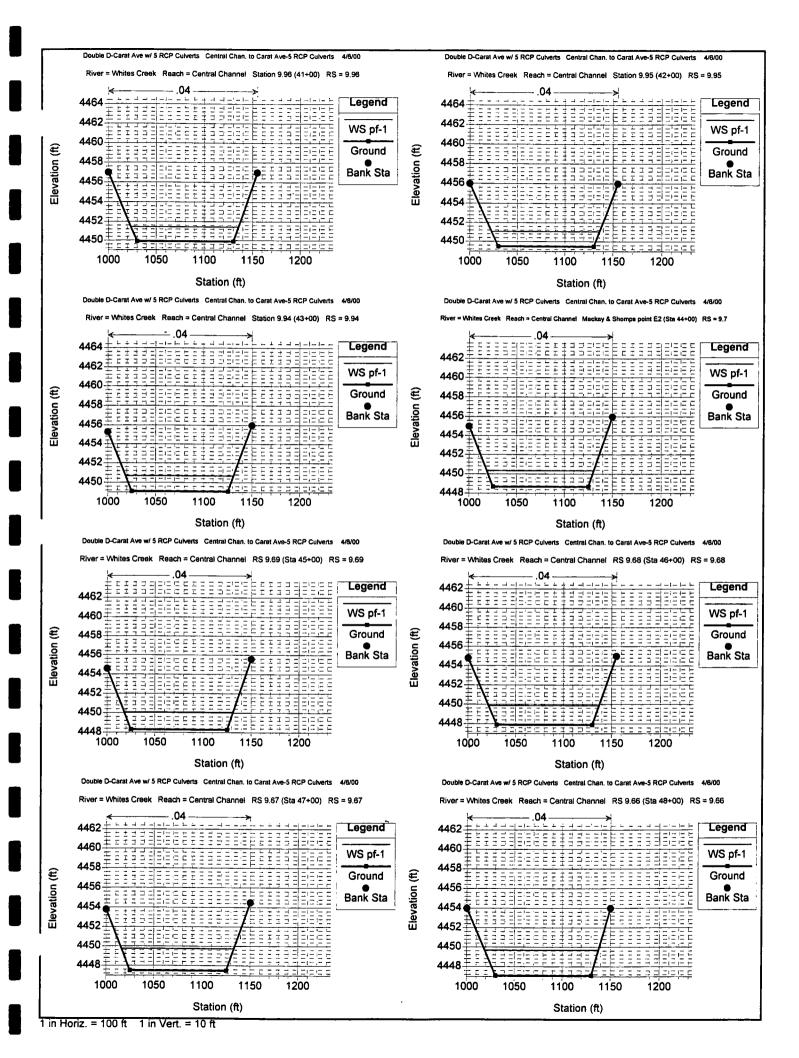


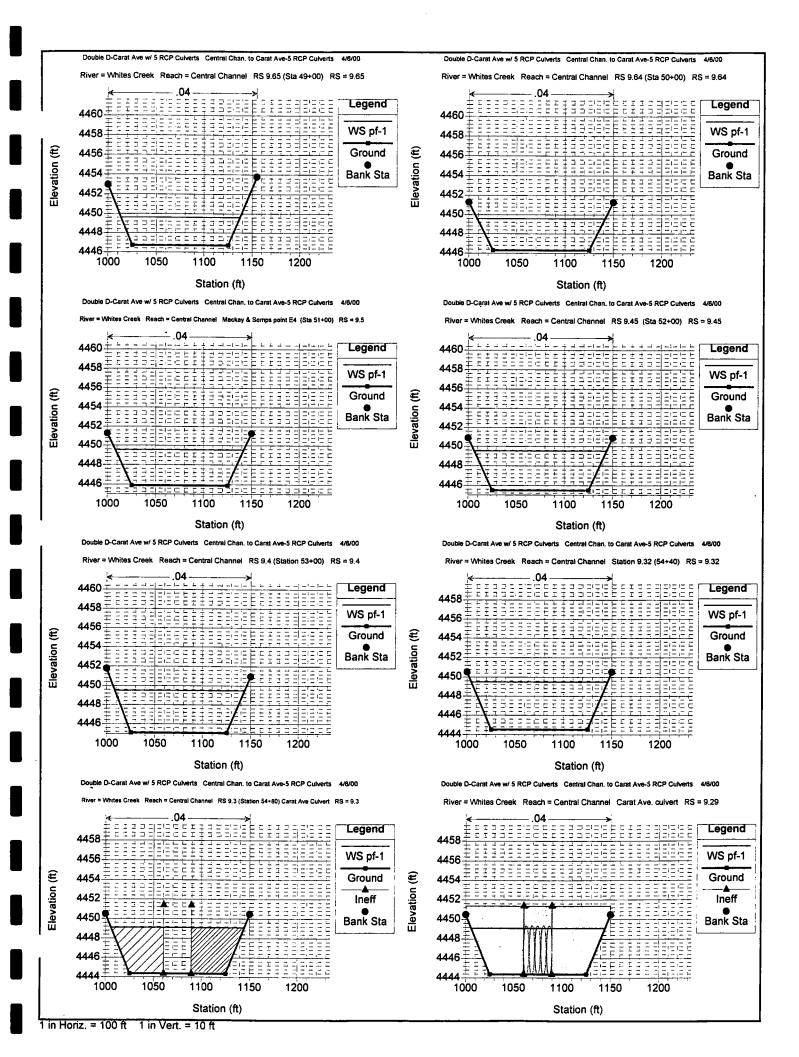


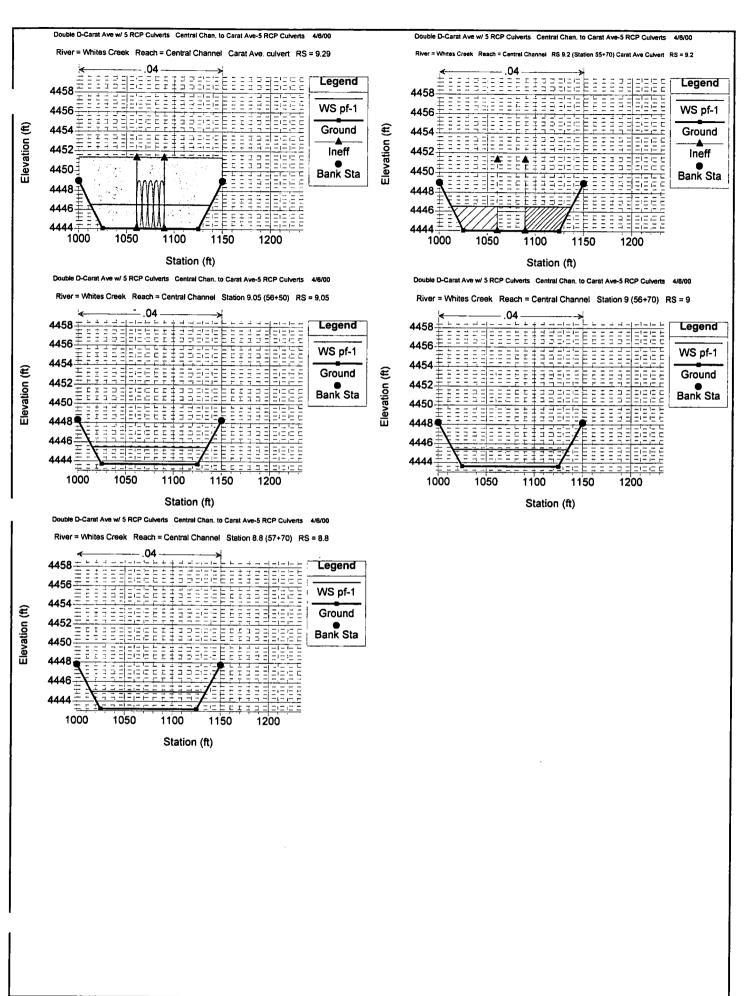












| | River Sta | Q Total | Length Chni | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Stope | Vel Chnl | Flow Area | Top Width | Froude # Chl |
|---------------------|-----------|-----------|-------------|-----------|-----------|----------------|-----------|------------|----------|-----------|-----------|--------------|
| | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Central Channel | 220 | 300.00 | 10.00 | 4466.00 | 4467.53 | 4467.01 | 4467.73 | 0.009187 | 3.55 | 84.47 | 60.22 | 0.53 |
| entral Channel | 219.2* | 300.00 | 10.00 | 4465.92 | 4467.44 | | 4467.64 | 0.009489 | 3.59 | 83.59 | 60,11 | 0.54 |
| ntral Channel | 218.4* | 300.00 | 10.00 | 4465.84 | 4467.33 | | 4467.54 | 0.009914 | 3.64 | 82.43 | 59.97 | 0.55 |
| Intral Channel | 217.6* | 300.00 | 10.00 | 4465.76 | 4467.22 | | 4467.43 | 0.010735 | 3.73 | 80,37 | 59.75 | 0.57 |
| entral Channel | 216.8* | 300.00 | 10.00 | 4465.68 | 4467.08 | | 4467.31 | 0.012353 | 3.90 | 76.86 | 59.40 | 0.60 |
| Central Channel | 216 | 300.00 | | 4465.60 | 4466.82 | | 4467.13 | 0.019582 | 4.51 | 66.45 | 58.35 | 0.75 |
| entral Channel | 215.666* | 300.00 | | 4465.55 | 4466.69 | | 4466.93 | 0.016414 | 4.00 | 75.04 | 69.36 | 0.66 |
| Central Channel | 215,333 | 300.00 | | 4465.50 | 4466.57 | | | | | | | |
| Central Channel | 215.* | 300.00 | | | | | 4466.77 | 0.014466 | 3.63 | 82.71 | 80.52 | 0.63 |
| entral Channel | | | | 4465.45 | 4466.45 | | 4466.63 | 0.013234 | 3.35 | 89.49 | 91.78 | 0.60 |
| | 214.686* | 300.00 | | 4465.40 | 4466.35 | | 4466.50 | 0.012517 | 3.15 | 95.31 | 103.10 | 0.58 |
| entral Channel | 214,333* | 300.00 | | 4465.35 | 4466.24 | | 4466.38 | 0.012310 | 3.00 | 99.87 | 114.48 | 0.57 |
| entral Channel 🧠 | 214 | 300.00 | | 4465.30 | 4465.89 | 4465.87 | 4466.15 | 0.040588 | 4.15 | 72.22 | 124.73 | 0.96 |
| entrat Channel | 213.* | 300.00 | 10.00 | 4465.22 | 4465.71 | | 4465.81 | 0.018375 | 2.49 | 120.49 | 247.79 | 0.63 |
| entral Channel | 212.* | 300.00 | 10,00 | 4465.15 | 4465.57 | | 4465.63 | 0.013831 | 1.95 | 154.15 | 370.85 | 0.53 |
| entral Channel . | 211.* | 300.00 | 10.00 | 4465.08 | 4465.44 | | 4465.49 | 0.012195 | 1.67 | 179.52 | 493.94 | 0.49 |
| entrat Channel | 210 | 300.00 | 10.00 | 4465.00 | 4465.34 | | 4465.37 | 0.009827 | 1.43 | 209.37 | 617.15 | 0.43 |
| entral Channel | 209.* | 300.00 | 10.00 | 4464.90 | 4465.24 | _ | 4465.27 | 0.009802 | 1.44 | 208.65 | 610.67 | 0.4 |
| entral Channel 🐫 | 208,* | 300.00 | 10.00 | 4464.80 | 4465.14 | | 4465.18 | 0.009780 | 1.44 | 207.90 | 604,18 | 0.43 |
| entral Channel | 207.* | 300.00 | 10.00 | 4464.70 | 4465.05 | | 4465.08 | 0.009808 | 1.45 | 206.83 | 597.70 | 0.43 |
| entral Channel | 206.* | 300.00 | 10.00 | 4464.60 | 4464.95 | | 4464.98 | 0.009793 | 1.46 | 206.02 | 591.21 | 0.43 |
| entral Channel | 205.* | 300.00 | 10.00 | 4464.50 | 4464.85 | | 4464.89 | 0.009738 | 1.46 | 205.46 | 584.73 | 0.43 |
| entral Channel | 204.* | 300.00 | 10.00 | 4464.40 | 4464.75 | | 4464.79 | 0.009732 | 1.47 | 203.48 | 578.25 | 0.43 |
| entral Channel | 203. | 300.00 | 10.00 | 4464.30 | 4464.66 | | 4464.69 | 0.009732 | 1.47 | 203.96 | 571.76 | 0.40 |
| entral Channel | 202 | 300.00 | 10.00 | 4464.20 | 4464.56 | | 4464.59 | 0.009732 | 1.47 | 203.96 | 565.28 | |
| entral Channel | 201.* | 300.00 | 10.00 | 4464,10 | 4464.46 | | 4464.59 | 0.009732 | 1.48 | | | 0.44 |
| entrat Channel | + | | | | | | | | | 201.49 | 558.79 | 0.44 |
| | 199.* | 300.00 | 10.00 | 4464.00 | 4464.36 | | 4464.39 | 0.010244 | 1.52 | 197.80 | 552.27 | 0.45 |
| entral Channet | 198.* | 300.00 | 10.00 | 4463.90 | 4464.26 | | 4464.29 | 0.010242 | 1.51 | 199.07 | 561.14 | 0.4 |
| entral Channel | | 300.00 | 10.00 | 4463.80 | 4464.15 | | 4464.19 | 0.010201 | 1.50 | 200.56 | 570.02 | 0.4 |
| entral Channel* | 197.* | 300.00 | 10.00 | 4463.70 | 4464.05 | | 4464.08 | 0.010216 | 1.49 | 201.72 | 578.89 | 0.44 |
| entral Channel | 196.* | 300.00 | 10.00 | 4463.60 | 4463.95 | | 4463.98 | 0.010238 | 1.48 | 202.82 | 587.76 | 0.44 |
| entral Channel | 195.* | 300.00 | 10.00 | 4463.50 | 4463.84 | | 4463.88 | 0.010220 | 1.47 | 204.14 | 596.64 | 0.44 |
| entral Channel | 194.* | 300.00 | 10.00 | 4463.40 | 4463.74 | | 4463.77 | 0.010209 | 1.46 | 205.42 | 605.51 | 0.44 |
| entral Channel | 193.* | 300.00 | 10.00 | 4463.30 | 4463.64 | | 4463.67 | 0.010156 | 1.45 | 206.94 | 614.39 | 0.44 |
| entral Channel 🖖 | 192. | 300.00 | 10.00 | 4463.20 | 4463.53 | 1 | 4463.57 | 0.010208 | 1.44 | 207.82 | 623.26 | 0.44 |
| entral Channel 🤙 | 191. | 300.00 | 10.00 | 4463.10 | 4463.43 | | 4463.46 | 0.010217 | 1.44 | 208.94 | 632.14 | 0.44 |
| entral Channel 🟅 | 190 | 300.00 | 10.00 | 4463.00 | 4463.34 | i | 4463.37 | 0.009416 | 1.39 | 215.32 | 641.07 | 0.42 |
| ntral Channel | 189.* | 300.00 | 10.00 | 4462.90 | 4463.24 | | 4463.27 | 0.009368 | 1.41 | 212.82 | 620.20 | 0.42 |
| entral Channel 👍 | 188.* | 300.00 | 10.00 | 4462.80 | 4463.15 | | 4463.18 | 0.009227 | 1.42 | 210.88 | 599.37 | 0.42 |
| entral Channet : 15 | 187.* | 300.00 | 10.00 | 4462.70 | 4463.06 | | 4463.09 | 0.009089 | 1,44 | 208.87 | 578.56 | 0.42 |
| entral Channel 4 | 186.* | 300.00 | 10.00 | 4462.60 | 4462.97 | | 4463.00 | 0.009035 | 1.45 | 206.20 | 557.76 | 0.42 |
| entral Channel | 185.* | 300.00 | 10.00 | 4462.50 | 4462.88 | | 4462.91 | 0.008948 | 1.47 | 203.69 | 537.01 | 0.42 |
| entral Channel | 184.* | 300.00 | 10.00 | 4462.40 | 4462.79 | | 4462.82 | 0.008907 | 1.49 | 200.78 | 516.29 | 0.42 |
| entral Channel | 183.* | 300.00 | 10.00 | 4462.30 | 4462.70 | | 4462.74 | 0.008807 | 1.51 | 198.20 | 495.64 | 0.42 |
| entral Channel | 182. | 300.00 | 10.00 | 4462.20 | 4462.61 | | 4462.65 | 0.008796 | 1.54 | 194.94 | 475.05 | 0.42 |
| entrat Channel | 181.* | 300.00 | 10.00 | 4462.10 | 4462.52 | | 4462,56 | 0.008790 | 1.57 | 191,24 | 454.54 | 0.42 |
| entral Channel | 180 | 300.00 | 10.00 | 4462.00 | 4462.25 | 4462.25 | 4462.37 | 0.058383 | | | | |
| entral Channel | | 300.00 | 10.00 | 4461.50 | 4461.65 | 4462.25 | 4461.98 | 0.056363 | 2.82 | 106.36 | 431.94 | 1.00 |
| | | | | | | | | | 4.61 | 65.08 | 421.27 | 2.07 |
| entral Charmel | | 300.00 | 10.00 | 4461.00 | 4461.25 | 4461.25 | 4461.38 | 0.064300 | 2.96 | 101.45 | 412.63 | 1.05 |
| entral Channel | 177.* | 300.00 | 10.00 | 4460.50 | 4461.28 | 4460.76 | 4461.29 | 0.001443 | 0.95 | 315.51 | 407.92 | 0.19 |
| entral Channel | 176.* | 300.00 | 10.00 | 4460.00 | 4461.28 | <u> </u> | 4461.29 | 0.000289 | 0.59 | 508.28 | 402.31 | 0.09 |
| | 175.*> | 300.00 | 10.00 | 4459.50 | 4461.28 | | 4461.28 | 0.000101 | 0.43 | 692.94 | 396.25 | 0.06 |
| entrat Channel | 174.* | 300.00 | 10.00 | 4459.00 | 4461.28 | | 4461.28 | 0.000046 | 0.35 | 869.46 | 389.83 | 0.04 |
| | 173.* | 300.00 | 10.00 | 4458.50 | 4461.28 | | 4461.28 | 0.000025 | 0.29 | 1037.70 | 383.14 | 0.03 |
| entral Channel | 172.* | 300.00 | 10.00 | 4458.00 | 4461.28 | | 4461.28 | 0.000015 | 0.25 | 1197.52 | 376.22 | 0.02 |
| entrat Channel | 171. | 300.00 | 10.00 | 4457.50 | 4461.28 | | 4461.28 | 0.000010 | 0.22 | 1348.82 | 369.12 | 0.02 |
| intral Channel | 170- | 300.00 | 10.00 | 4457.00 | 4461.28 | | 4461.28 | 0.000007 | 0.20 | 1491.55 | 361.86 | 0.02 |
| entral Channel | 169.* | 300.00 | 10.00 | 4456.90 | 4461.28 | i | 4461.28 | 0.000006 | 0.20 | 1528.05 | 362.80 | 0.02 |
| entral Channel | 168.* | 300.00 | 10.00 | 4456.80 | 4461.28 | | 4461.28 | 0.000006 | 0.19 | 1564.68 | 363.77 | 0.02 |
| entral Channel : | 167.* | 300.00 | 10.00 | 4456.70 | 4461,28 | | 4461.28 | 0.000006 | 0.19 | 1601.26 | 364.75 | 0.02 |
| entral Chemnel | 166.* | 300.00 | 10.00 | 4456.60 | 4461.28 | · | 4461.28 | 0.000005 | 0.18 | 1638.15 | 365.76 | 0.02 |
| intrat Channel | 165.* | 300.00 | 10.00 | 4456.50 | 4461.28 | | 4461.28 | 0.000005 | 0.18 | 1675.17 | 366.80 | 0.01 |
| entral Channel: | 164.* | 300.00 | 10.00 | 4456.40 | 4461.28 | | 4461.28 | 0.000004 | 0.18 | 1712.34 | 367.85 | 0.01 |
| entral Channel | 163." | 300.00 | 10.00 | 4456.30 | 4461.28 | | 4461.28 | 0.000004 | 0.18 | | 368.94 | 0.01 |
| entral Charvnel | 162.* | 300.00 | 10.00 | 4456.20 | 4461.28 | | 4461.28 | 0.000004 | | 1749.65 | | |
| entral Channet | 161.* | 300.00 | | : | | | | | 0.17 | 1786.93 | 370.04 | 0.01 |
| | | | 10.00 | 4456.10 | 4461.28 | | 4461.28 | 0.000004 | 0.16 | 1824.53 | 371.16 | 0.01 |
| entral Channel | 160 | 300.00 | 10.00 | 4456.00 | 4461.27 | 4456.72 | 4461.28 | 0.000049 | 0.62 | 485.17 | 372.27 | 0.05 |
| ntral Channel | 157.5* | 300.00 | 10.00 | 4455.95 | 4461.28 | | 4461.28 | 0.0000031 | 0.15 | 1983.70 | 390.11 | 0.01 |
| entral Channel | 155 | 300.00 | 30.00 | 4455.90 | 4460.97 | 4458.32 | 4461.26 | 0.002317 | 4.22 | 71.03 | 406.09 | 0.33 |
| entret Channel | 152 | Mult Open | | | | - | | | | - 1 | | |
| entrat Channel | 150 | 300.00 | 10.00 | 4455.75 | 4459.26 | 4458.18 | 4459.84 | 0.008024 | 6.12 | 49.01 | 421.27 | 0.58 |
| entral Channel 🛝 | 148.75* | 300.00 | 10.00 | 4455.71 | 4459.55 | - | 4459.55 | 0.000007 | 0.19 | 1612.19 | 431.18 | 0.02 |
| | 147.5* | 300.00 | 10.00 | 4455.67 | 4459.55 | + | 4459.55 | 0.000006 | 0.18 | 1660.41 | 439.37 | 0.02 |
| | 146.25* | 300.00 | 10.00 | 4455.64 | 4459.55 | - - | 4459.55 | 0.000006 | 0.18 | 1704.74 | | 0.02 |
| ~ | 145. | 300.00 | 10.00 | | | <u>i</u> - | | | | | 447.52 | |
| | 144.166* | 300.00 | | 4455.60 | 4459.55 | | 4459.55 | 0.000006 | 0.17 | 1754.18 | 455.71 | 0.02 |
| | | | 10.00 | 4455.56 | 4459.55 | | 4459.55 | 0.000005 | 0.17 | 1784.17 | 458.83 | 0.02 |
| | 143.333* | 300.00 | 10.00 | 4455.52 | 4459.55 | 1 | 4459.55 | 0.000005 | 0.17 | 1814.72 | 462.11 | 0.01 |
| entral Channel | 142.5° | 300.00 | 10.001 | 4455.48 | 4459.55 | | 4459.55 | 0.000005 | 0.16 | 1845.94 | 465.59 | 0.01 |

HEC-RAS Plan: DDCarat-5RCP River: Whites Creek Reach: Central Channel (Continued)

| | n DDCarai | | ver: Whites C | | | | | | | | | |
|---------------------------------|-------------|-----------------|---------------|--------------------|--------------------|-------------|--------------------|------------|--------------|--------------------|------------------|--------------|
| Reach | River Sta | Q Total | Length Chni | Min Ch Ei | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Stope | Vel Chni | Flow Area | Top Width | Froude # Chi |
| Central Channel | 141.666* | (cfs)
300.00 | (ft)
10.00 | (ft)
4455.43 | (R)
4459.55 | (ft) | (ft)
4459.55 | (ft/ft) | (ft/s) | (sq ft) | (ft) | |
| Central Channel | 140.833* | 300.00 | 10.00 | 4455,39 | | | 4459.55 | 0.000005 | 0.16 | 1882.64 | 469.44 | 0.01 |
| "entral Channel | 140 | 300.00 | 10.00 | 4455.35 | 4459.55 | | 4459.55 | 0.000004 | 0.16 | 1916.28
1952.33 | 473.82
479.21 | 0.01
0.01 |
| antral Channel | 139.* | 300.00 | 10.00 | 4455.31 | | | 4459.55 | 0.000004 | 0.15 | 1922.99 | 468.30 | 0.01 |
| Central Channel | 138.* | 300.00 | 10.00 | 4455.27 | 4459.55 | | 4459.55 | 0.000004 | 0.16 | 1892.76 | 457.41 | 0.01 |
| Central Channel | 137.* | 300.00 | 10.00 | 4455.22 | | | 4459.55 | 0.000004 | 0.16 | 1865.93 | 446.56 | 0.0 |
| Central Channel | 136.* | 300.00 | 10.00 | 4455.18 | | - | 4459.55 | 0.000004 | 0,16 | 1833.85 | 435.69 | 0.01 |
| Central Channel | 135.* | 300.00 | 10.00 | 4455.14 | 4459.55 | | 4459.55 | 0.000005 | 0.17 | 1800.89 | 424.84 | 0.01 |
| Central Channel | 134.* | 300.00 | 10.00 | 4455.10 | | | 4459.55 | 0.000005 | 0.17 | 1767.07 | 414.00 | 0.01 |
| Central Channel | 133.* | 300.00 | 10.00 | 4455.06 | | | 4459.55 | 0.000005 | 0.17 | 1732.37 | 403.18 | 0.01 |
| Central Channel | 132.* | 300.00 | 10.00 | 4455.01 | 4459.55 | | 4459.55 | 0.000005 | 0.18 | 1700.70 | 392.40 | 0.01 |
| Central Channel | 131. | 300.00 | 10.00 | 4454.97 | 4459.55 | | 4459.55 | 0.000005 | 0.18 | 1663.98 | 381.61 | 0.02 |
| Central Channel | 130 | 300.00 | 10.00 | 4454.93 | 4459.55 | | 4459.55 | 0.000005 | 0.18 | 1626.57 | 370.83 | 0.02 |
| Central Channel | 129.* | 300.00 | 10.00 | 4454.89 | 4459.55 | | 4459.55 | 0.000006 | 0.19 | 1574.22 | 357.63 | 0.02 |
| Central Channel | 128.* | 300.00 | 10.00 | 4454.84 | 4459.55 | | 4459.55 | 0.000006 | 0.20 | 1524.18 | 344.48 | 0.02 |
| Central Channel | 127.* | 300.00 | 10.00 | 4454.80 | 4459.55 | | 4459.55 | 0.000007 | 0.20 | 1469.52 | 331.33 | 0.02 |
| Central Channel | 126. | 300.00 | 10.00 | 4454.76 | 4459.55 | | 4459.55 | 0.000007 | 0.21 | 1413.79 | 318.20 | 0.02 |
| Central Channel | 125.* | 300.00 | 10.00 | 4454.71 | 4459.55 | | 4459.55 | 0.000008 | 0.22 | 1359.78 | 305.13 | 0.02 |
| Central Channel | 124.* | 300.00 | 10.00 | 4454.67 | 4459.55 | | 4459.55 | 0.000008 | 0.23 | 1301.74 | 292.05 | 0.02 |
| Central Channel | 123.* | 300.00 | 10.00 | 4454.63 | 4459.55 | | 4459.55 | 0.000009 | 0.24 | 1242.64 | 279.00 | 0.02 |
| Central Channel | 122.* | 300.00 | 10.00 | 4454.59 | 4459.55 | | 4459.55 | 0.000010 | 0.25 | 1182.45 | 265.96 | 0.02 |
| Central Channel | 121.* | 300.00 | 10.00 | 4454.54 | 4459.55 | | 4459.55 | 0.000011 | 0.27 | 1123.45 | 252.99 | 0.02 |
| Central Channel | 120 | 300.00 | 10.00 | 4454.50 | 4459.55 | | 4459.55 | 0.000013 | 0.28 | 1060.98 | 240.00 | 0.02 |
| | 118,333* | 300.00 | 10.00 | 4454.46 | 4459.55 | | 4459.55 | 0.000014 | 0.30 | 1002.61 | 225.78 | 0.03 |
| Central Channel Central Channel | 116.666° | 300.00 | 10.00 | 4454.42 | 4459.55 | | 4459.55 | 0.000016 | 0.32 | 943.33 | 211.60 | 0.03 |
| Central Channel | 113,333* | 300.00 | 10.00 | 4454.38 | 4459.55 | | 4459.55 | 0.000018 | 0.34 | 882.72 | 197.32 | 0.03 |
| Central Channel | 111.686* | 300.00 | 10.00 | 4454.33 | 4459.55 | | 4459.55 | 0.000021 | 0.36 | 822.67 | 183.10 | 0.03 |
| Central Channel | 110 | 300.00 | 10.00 | 4454.29
4454.25 | 4459.55
4459.55 | | 4459.55
4459.55 | 0.000024 | 0.39 | 759.54 | 168.76 | 0.03 |
| Central Channel | 109,285* | 300.00 | 10.00 | 4454.21 | 4459.55 | | 4459.55 | 0.000029 | 0.43 | 695.46
650.39 | 154.45
144.21 | 0.04 |
| Central Channel | 108.571* | 300,00 | 10.00 | 4454.17 | 4459.55 | | 4459.55 | 0.000038 | 0.50 | 604.42 | 133.92 | 0.04 |
| Central Channel | 107,857* | 300.00 | 10.00 | 4454.13 | 4459.55 | | 4459.55 | 0.000045 | 0.54 | 557.83 | 123.66 | 0.04 |
| Central Channel | 107.142° | 300.00 | 10.00 | 4454.10 | 4459.55 | | 4459.55 | 0.000054 | 0.59 | 509.36 | 113.37 | 0.05 |
| Central Channel | 106.428* | 300.00 | 10.00 | 4454.06 | 4459.54 | | 4459.55 | 0.000067 | 0.65 | 461.30 | 103.10 | 0.05 |
| Central Channel | 105,714* | 300.00 | 10.00 | 4454.02 | 4459.54 | | 4459.55 | 0.000084 | 0.73 | 412.29 | 92.77 | 0.06 |
| Central Channel | 105 | 300.00 | 8.33 | 4453.98 | 4459.54 | | 4459.55 | 0.000111 | 0.83 | 362.58 | 82.47 | 0.07 |
| entral Channel | 103,333* | 300.00 | 8.33 | 4453.93 | 4459.54 | | 4459.55 | 0.000132 | 0.90 | 331.63 | 74.66 | 0.08 |
| antral Channel | 101.668* | 300.00 | 8.33 | 4453.88 | 4459.53 | | 4459.55 | 0.000160 | 1.00 | 299.97 | 66.84 | 0.08 |
| Central Channel | 100 | 300.00 | 115.00 | 4453.83 | 4459.17 | 4456.51 | 4459.51 | 0.002659 | 4.68 | 64.08 | 57.51 | 0.36 |
| Central Channel | 97 | Culvert | | | | | | | | | | |
| Central Channel | 95 | 300.00 | 110.00 | 4453.25 | 4455.14 | 4455.93 | 4457.86 | 0.054386 | 13.24 | 22.66 | 15.15 | 0.36 |
| Central Channel | 90 | 300.00 | 30.00 | 4453.14 | 4454.99 | 4454.61 | 4455.37 | 0.010019 | 4.99 | 60.13 | 38.09 | 0.70 |
| Central Channel | 80 | 300.00 | 100.00 | 4453.11 | 4454.97 | | 4455.13 | 0.003724 | 3.18 | 94.35 | 56.19 | 0.43 |
| Central Channel | 70
60 | 300.00 a | 100.00 | 4453.00 | 4454.71 | | 4454.81 | 0.002534 | 2.54 | 118.25 | 74.26 | 0.35 |
| Central Channel | 50 | 300.00 | 100.00 | 4452.90
4452.80 | 4454.52 | | 4454.59
4454.42 | 0.001841 | 2.11 | 142.12 | 92.71 | 0.30 |
| | 40 | 300.00 | | 4452.70 | 4454.37
4454.22 | | | 0.001417 | 1.83 | 163.98 | 109.05
112.24 | 0.26 |
| | 30 | 500.00 | | 4452.30 | 4453.85 | | 4454.27
4454.00 | 0.004009 | 1.86
3.04 | 161.04
164.73 | 111.98 | 0.27 |
| <u> </u> | 20 | 500.00 | 100.00 | 4451.90 | 4453.45 | | 4453.60 | 0.003995 | 3.03 | 165.24 | 112.57 | 0.44 |
| Central Channel | 10 | 500.00 | 100.00 | 4451.50 | 4453.05 | | 4453.19 | 0.003933 | 3.04 | 164.52 | 112.24 | 0.44 |
| | 9.99 | 500.00 | 100.00 | 4451.10 | 4452.63 | | 4452.78 | 0.004214 | 3.08 | 162.08 | 111.63 | 0.45 |
| | 9.98 | 500.00 | 100,00 | 4450.70 | 4452.25 | | 4452.38 | 0.003679 | 2.91 | 171.70 | 116.43 | 0.42 |
| Central Channel | 9.97 | 500.00 | 100.00 | 4450.30 | 4451.86 | | 4452.00 | 0.004003 | 3.04 | 164.61 | 111.62 | 0.44 |
| Central Channel | 9.96 | 500.00 | 100.00 | 4449.90 | 4451.46 | | 4451.60 | 0.003979 | 3.03 | 165.16 | 112.07 | 0.44 |
| | 9.95 | 500.00 | 100.00 | 4449.50 | 4451.07 | | 4451.21 | 0.003877 | 2.99 | 167.13 | 113.26 | 0.43 |
| ` <u>-</u> | 9.94 | 500.00 | 100.00 | 4449.10 | 4450.69 | | 4450.83 | 0.003696 | 2.96 | 168.93 | 112.19 | 0.43 |
| | 9.7 | 500.00 | 100.00 | 4448.70 | 4450.35 | | 4450.48 | 0.003274 | 2.85 | 175.22 | 112.21 | 0.40 |
| | 9.69 | 500.00 | 100.00 | 4448.30 | 4450.08 | | 4450.18 | 0.002562 | 2.64 | 189.25 | 113.13 | 0.36 |
| | 9.68 | 500.00 | 100.00 | 4447.90 | 4449.88 | | 4449.97 | 0.001760 | 2.34 | 213.65 | 115.60 | 0.30 |
| | 9.67 | 500.00 | 100.00 | 4447.50 | 4449.76 | | 4449.82 | 0.001137 | 2.04 | 244.83 | 117.01 | 0.25 |
| | 9.66 | 500.00 | 100,00 | 4447.10 | 4449.68 | | 4449.73 | 0.000725 | 1.77 | 281.90 | 118.68 | 0.20 |
| | 9.65 | 500.00 | 100.00 | 4446.70 | 4449.63 | | 4449.67 | 0.000463 | 1.52 | 328.13 | 124.01 | 0.17 |
| | 9.64 | 500.00 | 100.00 | 4446.30 | 4449.60 | | 4449.63 | 0.000300 | 1.30 | 384.49 | 133.00 | 0.13 |
| | 9.5′ | 650.00 | 100.00 | 4445.90 | 4449.56 | | 4449.59 | 0.000359 | 1.52 | 427.52 | 133.85 | 0.15 |
| | 9.45 | 650.00 | 100.00 | 4445.50 | 4449.53 | | 4449.56 | 0.000256 | 1.36 | 478.36 | 137.33 | 0.13 |
| | 9.4 | 650.00 | 140.00 | 4445.10 | 4449.51 | - 1 | 4449.54 | 0.000191 | 1.25 | 518.77 | 135.16 | 0.11 |
| | 9.32 | 650.00 | 40.00 | 4444.54 | 4449.49 | | 4449.51 | 0.000127 | 1.09 | 597.58 | 141.22 | 0.09 |
| | 9.3
9.29 | 650.00 | 90.00 | 4444.36 | 4449.12 | 4446.85 | 4449.47 | 0.002001 | 4.70 | 138.16 | 138.80 | 0.38 |
| | 9.29 | Culvert | 80.00 | 4444.00 | 446.50 | 4440.50 | | 0.040050 | | 76.66 | 405.04 | |
| | 9.05 | 650.00 | 80.00 | 4444.02 | 4446.53 | 4446.53 | 4447.77 | 0.016858 | 8.92 | 72.90 | 125.24 | 0.99 |
| | 9.05 | 650.00 | 20.00 | 4443.70 | 4445.50 | 4444.77 | 4445.67 | 0.004003 | 3.28 | 198.00 | 119.60 | 0.45 |
| | 8.8 | 650.00 | 100.00 | 4443.62 | 4445.42 | 4444.30 | 4445.59 | 0.004001 | 3.28 | 198.07 | 119,69 | 0.45 |
| | <u> </u> | 030.00 | | 4443.22 | 4445.02 | 4444.29 | 4445.19 | 0.004005 | 3.28 | 198.01 | 119.68 | 0.45 |

HEC-RAS Plan: DDCarat-5RCP River: Whites Creek Reach: Central Channel C4 / Vert Table

| Reach | | River Sta | E.G. US. | W.S. US. | E.G. IC | E.G. OC | Min Top Rd | Culv Q | Q Weir | Delta WS | Culv Vel In | Culv Vel Out |
|-----------------|------|--------------|----------|----------|---------|---------|------------|--------|--------|----------|-------------|--------------|
| | | | (ft) | (ft) | (ft) | (ft) | (ft) | (cfs) | (cfs) | (ft) | (ft/s) | (ft/s) |
| Central Channel | 152 | Cuty Grp #1 | 4461.26 | 4460.93 | 4461.26 | 4461.23 | 4465.00 | 277.89 | | 1.85 | 9.85 | 10.20 |
| Central Channel | 152 | Culv Grp #2 | 4461.26 | 4461.19 | 4458.85 | 4461.26 | 4465.00 | 22.11 | | 1.47 | 7.04 | 7.04 |
| entral Channel | 97 | W.May-5'RCPs | 4459.51 | 4459.17 | 4459.51 | 4459.43 | 4460.20 | 300.00 | | 4.03 | 10.18 | 10.48 |
| entral Channel | 9.29 | Carat-5'RCPs | 4449,47 | 4449.12 | 4449.47 | 4449.45 | 4451.36 | 650.00 | | 2.59 | 9.08 | 9.58 |

Option #2:

Four, 5-foot by 5-foot RCB Culverts at Carat Avenue

Project: ddcarat3.prj

Project Title: Double D-Carat Ave w/ 4RCB Culverts

Project Directory: m:\jobs\9908\hydro\ras\wetland-CaratAv\

roject Plans

Plan (current)

Title: Central Chan. to Carat Ave-4RCB Culverts

Short ID: DDCarat-4RCB

File: m:\jobs\9908\hydro\ras\wetland-CaratAv\ddcarat3.p01

Title:Central Chan. to Carat Av.-4RCB culverts

File:m:\jobs\9908\hydro\ras\wetland-CaratAv\ddcarat3.g02

Flow:

Title:Wetland 300 base + 400 upstr.of Carat

File:m:\jobs\9908\hydro\ras\wetland-CaratAv\ddcarat3.f01

Current Plan Statistics

Number of:

Cross Sections = 147

User Input XSs = 50

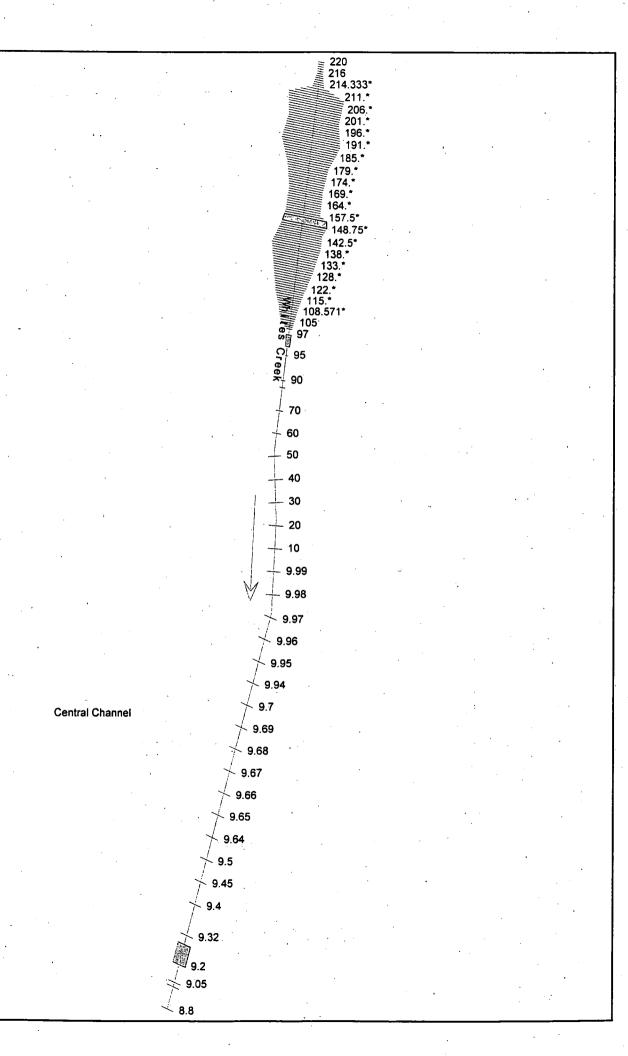
Interpolated = 97

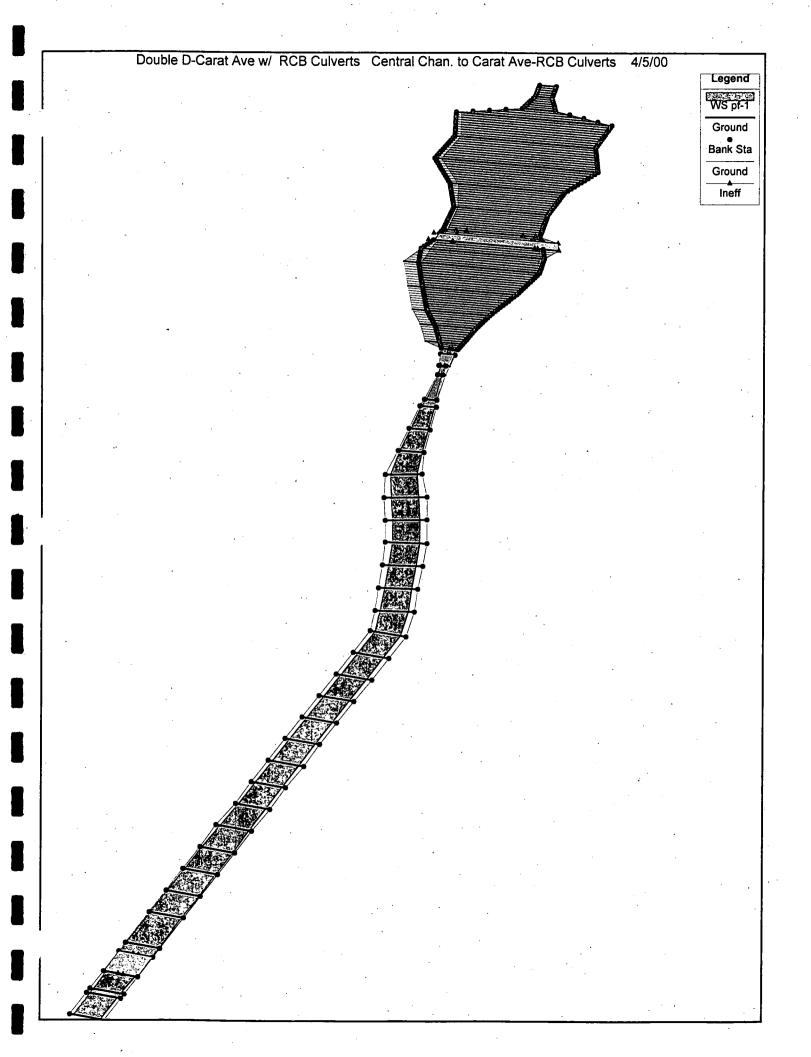
2

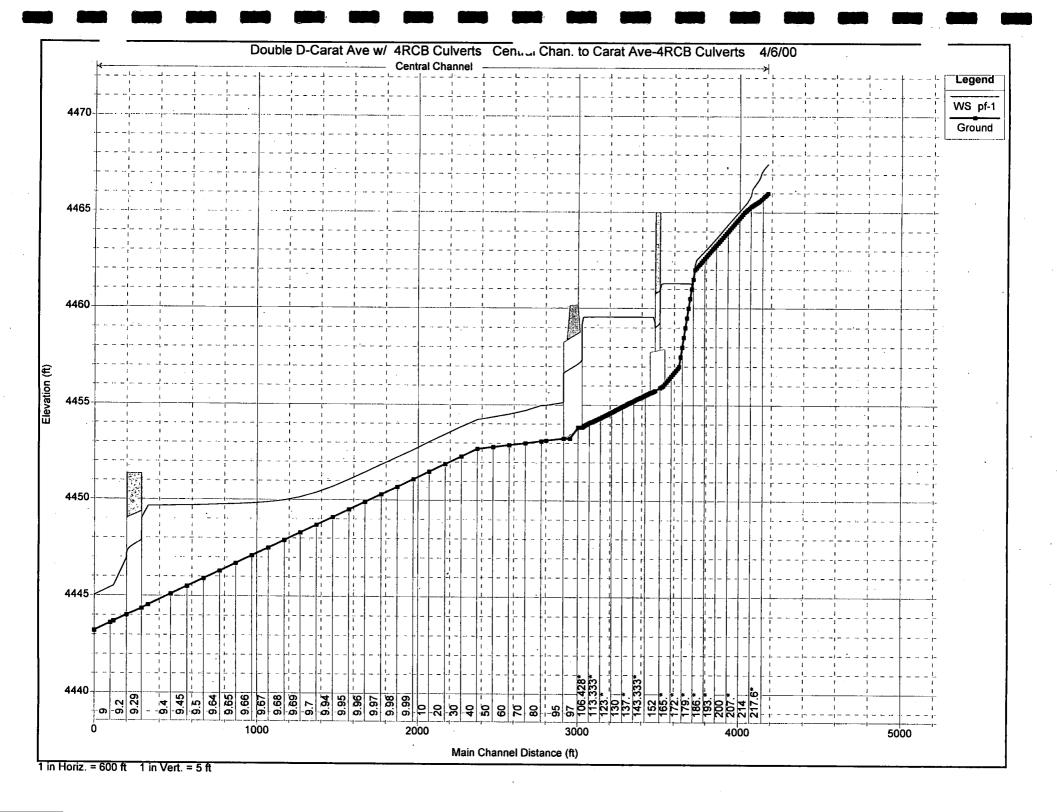
Culverts Bridges

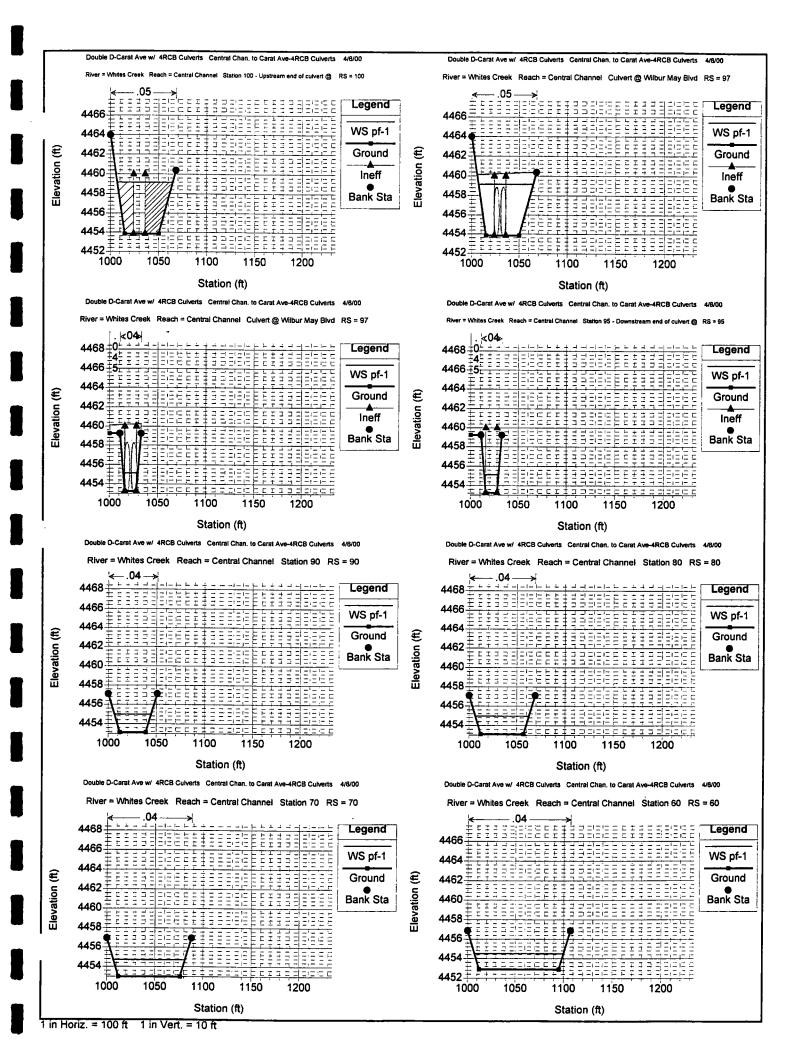
Mulitple Openings =

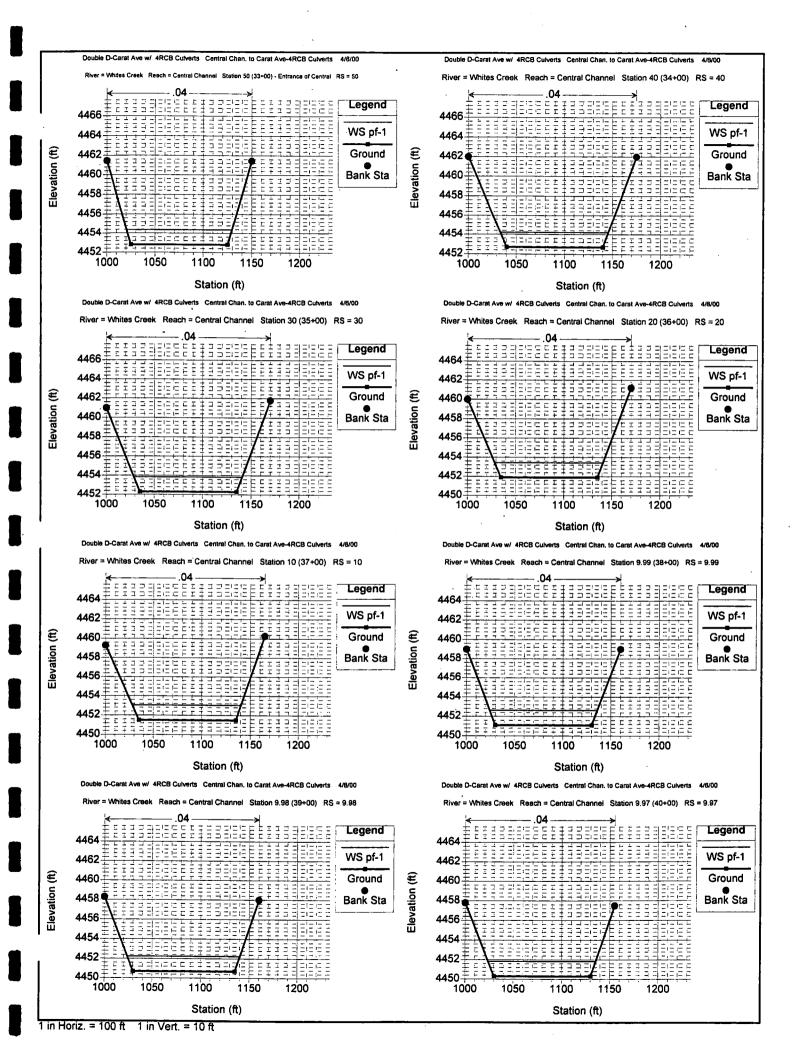
Inline Weirs

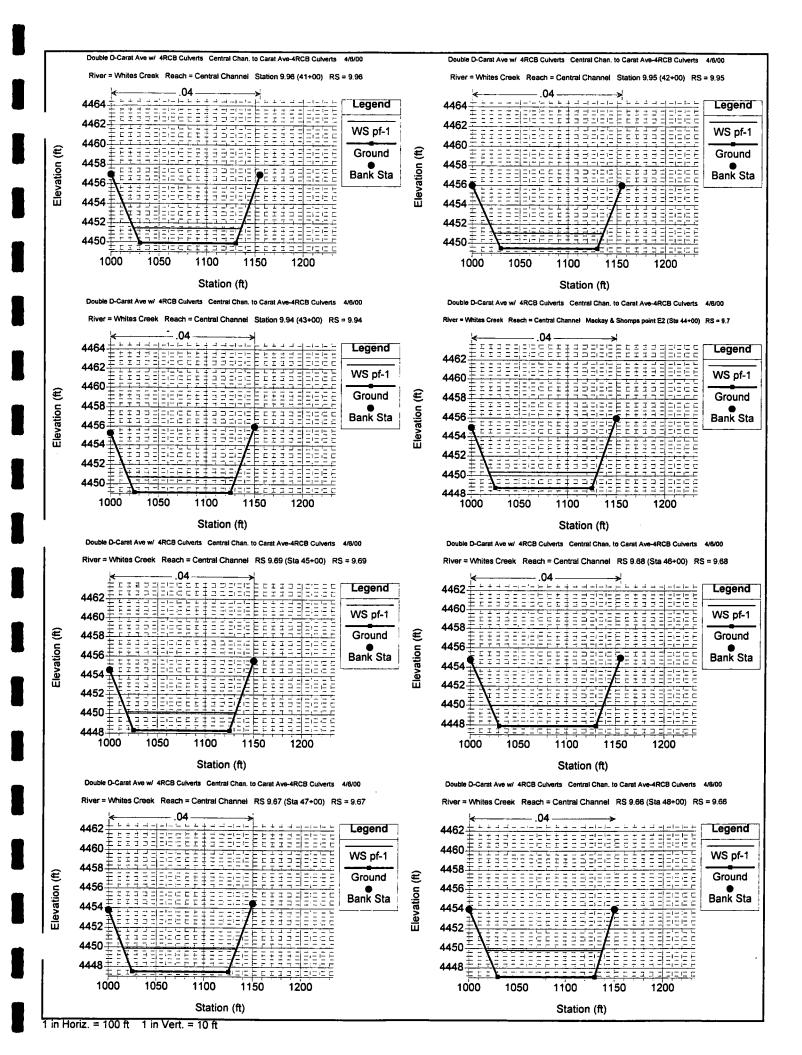


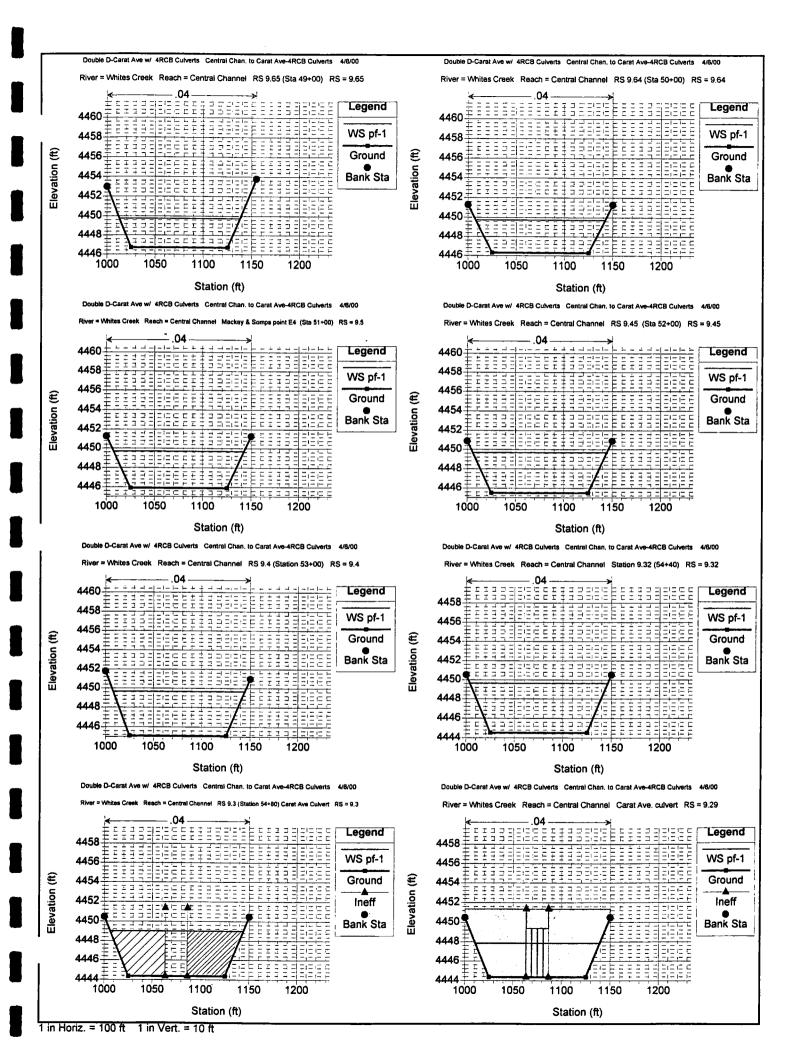


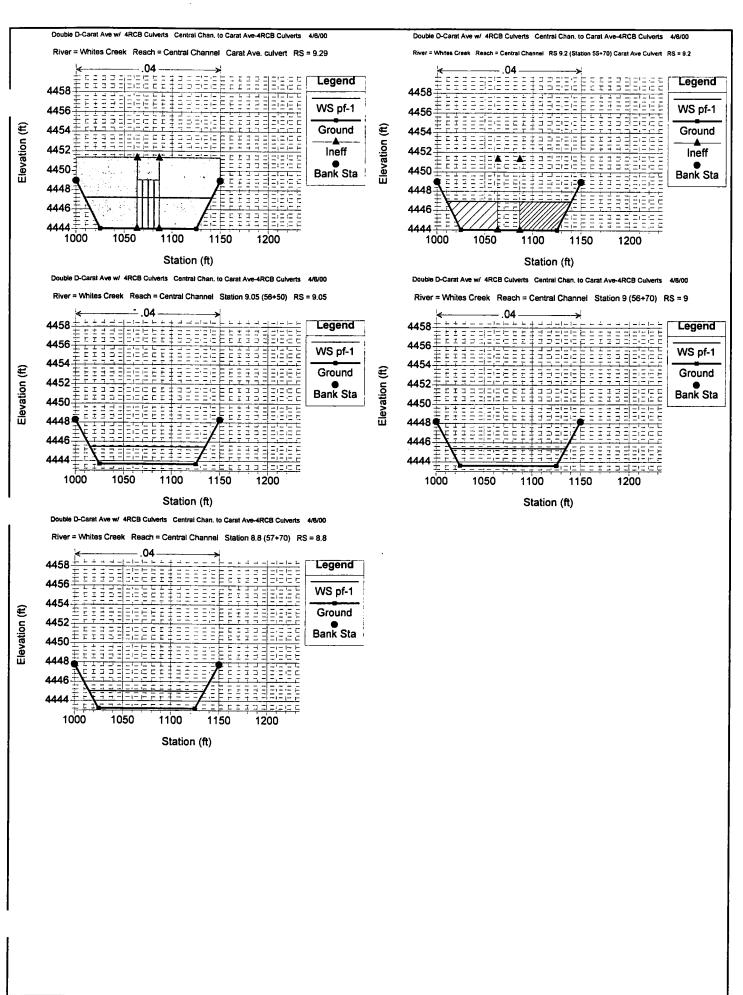












| Reach | River Sta | Q Total | eek Reach: Cent | Min Ch Ei | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vei Chni | Flow Area | Top Width | Froude # Chi |
|-------------------|----------------|------------------|-----------------|--------------------|--------------------|--------------|--------------------|------------|----------|---------------------------------|------------------|--------------|
| 1.000. | | (cfs) | (ft) | (ft) | (ft) | (ft) | (ft) | (ft/ft) | (ft/s) | (sq ft) | (ft) | FIOUGH # CIN |
| Central Channel | 220 | 300.00 | 10.00 | 4466.00 | 4467.53 | 4467.01 | 4467.73 | <u></u> | 3.55 | 84.47 | 60.22 | 0.53 |
| Central Channel | 219.2* | 300.00 | 10.00 | 4465.92 | 4467.44 | | 4467.64 | <u> </u> | 3.59 | 83.59 | 60.11 | |
| *entral Channel | 218.4* | 300.00 | 10.00 | 4465.84 | 4467.33 | | 4467.54 | | 3.64 | 82.43 | 59.97 | · |
| entral Channel | 217.6* | 300.00 | 10.00 | 4465.76 | 4467.22 | | 4467.43 | | 3.73 | 80.37 | 59.75 | 0.57 |
| Central Channel | 216.8" | 300.00 | 10.00 | 4465.68 | 4467.08 | | 4467,31 | | 3.90 | 76.86 | 59.40 | 0.60 |
| Central Channel | 216 | 300.00 | 9.17 | 4465.60 | 4466.82 | | 4467.13 | | 4.51 | 66.45 | 58.35 | 0.75 |
| Central Channel | 215.666* | 300.00 | <u>L</u> . | 4465.55 | 4466.69 | | 4466.93 | 0.016414 | 4.00 | 75.04 | 69.36 | 0.68 |
| Central Channel | 215.333* | 300.00 | 9.17 | 4465.50 | 4466.57 | | 4466.77 | | 3.63 | 82.71 | 80.52 | 0.63 |
| Central Channel | 215.* | 300.00 | 9.17 | 4465.45 | 4466.45 | | 4466.63 | 0.013234 | 3.35 | 89.49 | 91.78 | 0.60 |
| Central Channel | 214.666* | 300.00 | 9.17 | 4465.40 | 4466.35 | - | 4466.50 | | 3.15 | 95,31 | 103,10 | 0.58 |
| Central Channel | 214.333* | 300.00 | 9.17 | 4465.35 | 4466.24 | | 4466.38 | 0.012310 | 3.00 | 99.87 | 114,48 | 0.57 |
| Central Channel | 214 | 300.00 | 10.00 | 4465.30 | 4465.89 | 4465.87 | 4466.15 | 0.040588 | 4.15 | 72.22 | 124.73 | 0.96 |
| Central Channel | 213,* | 300.00 | 10.00 | 4465.22 | 4465.71 | | 4465.81 | 0.018375 | 2.49 | 120.49 | 247.79 | 0.63 |
| Central Channel | 212.* | 300.00 | 10.00 | 4465,15 | 4465.57 | | 4465.63 | 0.013831 | 1.95 | 154.15 | 370.85 | 0.53 |
| Centrel Channel | 211.*, | 300.00 | 10.00 | 4465.08 | 4465.44 | | 4465.49 | 0.012195 | 1.67 | 179.52 | 493.94 | 0.49 |
| | 210 | 300.00 | 10,00 | 4465.00 | 4465.34 | | 4465.37 | 0.009827 | 1.43 | 209.37 | 617.15 | 0.43 |
| | 209. | 300.00 | 10.00 | 4464.90 | 4465.24 | | 4465.27 | 0.009802 | 1,44 | 208.65 | 610.67 | 0.43 |
| | 208. | 300.00 | 10.00 | 4464.80 | 4465.14 | | 4465.18 | 0.009780 | 1.44 | 207.90 | 604.18 | 0.43 |
| | 207.* | 300.00 | 10.00 | 4464.70 | 4465.05 | | 4465.08 | 0.009808 | 1.45 | 206.83 | 597.70 | 0.43 |
| | 206. | 300.00 | 10.00 | 4464.60 | 4464.95 | | 4464.98 | 0.009793 | 1.46 | 206.02 | 591.21 | 0.43 |
| | 205.* | 300.00 | 10.00 | 4464.50 | 4464.85 | | 4464.89 | 0.009738 | 1.46 | 205.46 | 584.73 | 0.43 |
| | 204. | 300.00 | 10.00 | 4464.40 | 4464.75 | | 4464.79 | 0.009732 | 1.47 | 204.59 | 578.25 | 0.43 |
| | 203. | 300.00 | 10.00 | 4464.30 | 4464.66 | | 4464.69 | 0.009686 | 1.47 | 203,96 | 571.76 | 0.43 |
| | 202.* | 300.00 | 10.00 | 4464.20 | 4464.56 | | 4464.59 | 0.009732 | 1.48 | 202.74 | 565.28 | 0.44 |
| | 201. | 300.00 | 10.00 | 4464.10 | 4464.46 | | 4464.50 | 0.009782 | 1.49 | 201.49 | 558.79 | 0.44 |
| | 2000 | 300.00 | 10.00 | 4464.00 | 4464.36 | | 4464.39 | 0.010244 | 1.52 | 197.80 | 552.27 | 0.45 |
| | 199.*
198.* | 300.00
300.00 | 10.00 | 4463.90 | 4464.26 | | 4464.29 | 0.010242 | 1.51 | 199.07 | 561.14 | 0.45 |
| | 197.* | 300.00 | 10.00 | 4463.80
4463.70 | 4464.15 | | 4464.19 | 0.010201 | 1.50 | 200.56 | 570.02 | 0.44 |
| | 196.* | 300.00 | 10.00 | | 4464.05 | | 4464.08 | 0.010216 | 1.49 | 201.72 | 578.89 | |
| | 195.* | 300.00 | 10.00 | 4463.60
4463.50 | 4463.95
4463.84 | | 4463.98 | 0.010238 | 1.48 | 202.82 | 587.76 | 0.44 |
| | 194.* | 300.00 | 10.00 | 4463.40 | 4463.74 | | 4463.88
4463.77 | 0.010220 | 1.47 | 204.14
205.42 | 596.64 | 0.44
0.44 |
| | 193,* | 300.00 | 10.00 | 4463.30 | 4463.64 | | 4463.77 | 0.010209 | 1.46 | 205.42 | 605.51
614.39 | 0.44 |
| | 192.* | 300.00 | 10.00 | 4463.20 | 4463.53 | | 4463.57 | 0.010138 | 1.43 | 207.82 | 623.26 | 0.44 |
| | 191.* | 300.00 | 10.00 | 4463.10 | 4463.43 | | 4463.46 | 0.010207 | 1.44 | 208.94 | 632.14 | 0.44 |
| | 190 | 300.00 | 10.00 | 4463.00 | 4463.34 | | 4463,37 | 0.009416 | 1.39 | 215.32 | 641,07 | 0.42 |
| | 189.** | 300.00 | 10.00 | 4462.90 | 4463.24 | | 4463.27 | 0.009368 | 1.41 | 212.82 | 620.20 | 0.42 |
| | 188.* | 300.00 | 10.00 | 4462.80 | 4463.15 | | 4463.18 | 0.009227 | 1.42 | 210.88 | 599.37 | 0.42 |
| Central Channel | 187.* | 300.00 | 10.00 | 4462.70 | 4463.06 | | 4463.09 | 0.009089 | 1.44 | 208.87 | 578.56 | 0.42 |
| Central Channel | 186.* | 300.00 | 10.00 | 4462.60 | 4462.97 | | 4463.00 | 0.009035 | 1.45 | 206.20 | 557.76 | 0.42 |
| Central Channel | 185.* | 300.00 | 10,00 | 4462.50 | 4462.88 | | 4462.91 | 0.008948 | 1.47 | 203.69 | 537.01 | 0.42 |
| Central Channel | 184.* | 300.00 | 10.00 | 4462.40 | 4462.79 | | 4462.82 | 0.008907 | 1.49 | 200.78 | 516.29 | 0.42 |
| Central Channel | 183.* | 300.00 | 10.00 | 4462.30 | 4462.70 | | 4462.74 | 0.008807 | 1.51 | 198.20 | 495.64 | 0.42 |
| Central Channel | 162.* | 300.00 | 10.00 | 4462.20 | 4462.61 | | 4462.65 | 0.008796 | 1.54 | 194.94 | 475.05 | 0.42 |
| Central Channel | 181.* | 300.00 | 10.00 | 4462.10 | 4462.52 | | 4462.56 | 0.008840 | 1.57 | 191.24 | 454.54 | 0.43 |
| 1.7.11 | 180 | 300.00 | 10.00 | 4462.00 | 4462.25 | 4462.25 | 4462.37 | 0.058383 | 2.82 | 106.36 | 431.94 | 1.00 |
| Central Channel | 179. | 300.00 | 10.00 | 4461.50 | 4461.65 | 4461.75 | 4461.98 | 0.290332 | 4.61 | 65.08 | 421.27 | 2.07 |
| | 176.* | 300.00 | 10.00 | 4461.00 | 4461.25 | 4461.25 | 4461.38 | 0.064300 | 2.96 | 101.45 | 412.63 | 1.05 |
| i | 177,* | 300.00 | 10.00 | 4460.50 | 4461.28 | 4460.76 | 4461.29 | 0.0014431 | 0.95 | 315.51 | 407.92 | 0.19 |
| | 176.* | 300.00 | 10.00 | 4460.00 | 4461.28 | | 4461.29 | 0.000289 | 0.59 | 508.28 | 402.31 | 0.09 |
| | 175.* | 300.00 | 10.00 | 4459.50 | 4461.28 | | 4461.28 | 0.000101 | 0.43 | 692.94 | 396.25 | 0.06 |
| | 174.* | 300.00 | 10.00 | 4459.00 | 4461.28 | | 4461.28 | 0.000046 | 0.35 | 869.46 | 389.83 | 0.04 |
| | 173.* | 300.00 | 10.00 | 4458.50 | 4461.28 | | 4461.28 | 0.000025 | 0.29 | 1037.70 | 383.14 | 0.03 |
| | 172* | 300.00 | 10.00 | 4458.00 | 4461.28 | | 4461.28 | 0.000015 | 0.25 | 1197.52 | 376.22 | 0.02 |
| | 171.** | 300.00 | 10.00 | 4457.50 | 4461.28 | | 4461.28 | 0.000010 | 0.22 | 1348.82 | 369.12 | 0.02 |
| | 169.* | 300.00 | 10.00 | 4457.00 | 4461.28 | | 4461.28 | 0.000007 | 0.20 | 1491.55 | 361.86 | 0.02 |
| | 168.* | 300.00 | 10.00 | 4456.90 | 4461.28 | | 4461.28 | 0.000006 | 0.20 | 1528.05 | 362.80 | 0.02 |
| | 167.* | 300.00 | 10.00 | 4456.80
4456.70 | 4461.28 | i | 4461.28 | 0.000006 | 0.19 | 1564.68 | 363.77 | 0.02
0.02 |
| | 166.* | 300.00 | 10.00 | 4456.60 | 4461.28
4461.28 | | 4461.28
4461.28 | 0.000006 | 0.19 | 1601.26 ₁
1638.15 | 364.75
365.76 | 0.02 |
| | 165.*1 | 300.00 | 10.00 | 4456.50 | 4461.28 | | 4461.28 | 0.000005 | | 1675.17 | 365.76 | 0.02 |
| | 164.* | 300.00 | 10.00 | 4456.50 | 4461.28 | + | 4461.28 | 0.000005 | 0.18 | 1712.34 | 367.85 | 0.01 |
| | 163.** | 300.00 | 10.00 | 4456.40 | 4461.28 | | 4461.28 | 0.000004 | 0.18 | 1712.34 | 368.94 | 0.01 |
| | 162. | 300.00 | 10.00 | 4456.30 | 4461.28 | | 4461.28 | 0.000004 | 0.17 | 1786.93 | 370.04 | 0.01 |
| | 161. | 300.00 | 10.00 | 4456.10 | 4461.28 | | 4461.28 | 0.000004 | 0.17 | 1824.53 | 371.16 | 0.01 |
| | 160 | 300.00 | 10.00 | 4456.00 | 4461.27 | 4456.72 | 4461.28 | 0.000049 | 0.16 | 485.17 | 371.10 | 0.05 |
| | 157.5* | 300.00 | 10.00 | 4455.95 | 4461.28 | 1100.12 | 4461.28 | 0.000003 | 0.02 | 1983.70 | 390.11 | 0.03 |
| <u> </u> | 155 | 300.00 | 30.00 | 4455.90 | 4460.97 | 4458.32 | 4461.26 | 0.002317 | 4.22 | 71.03 | 406.09 | 0.33 |
| | 152 | Mult Open | 30.00 | | | | | 5.552517 | 7.44 | . 1.03 | , | 3.30 |
| | 150 | 300.00 | 10.00 | 4455.75 | 4459.26 | 4458.18 | 4459.84 | 0.008024 | 6.12 | 49.01 | 421.27 | 0.58 |
| the second second | 148.75* | 300.00 | 10.00 | 4455.71 | 4459.55 | | 4459.55 | 0.000024 | 0.19 | 1612.19 | 431.18 | 0.02 |
| | 147.5* | 300.00 | 10.00 | 4455.67 | 4459.55 | | 4459.55 | 0.000007 | 0.19 | 1660.41 | 439.37 | 0.02 |
| | 146.25* | 300.00 | 10.00 | 4455.64 | 4459.55 | | 4459.55 | 0.000006 | 0.18 | 1704.74 | 447.52 | 0.02 |
| | 145 | 300.00 | 10.00 | 4455.60 | 4459.55 | | 4459.55 | 0.000006 | 0.17 | 1754.18 | 455.71 | 0.02 |
| | 144.168* | 300.00 | 10.00 | 4455.56 | 4459.55 | | 4459.55 | 0.000005 | 0.17 | 1784.17 | 458.83 | 0.02 |
| | 143.333* | 300.00 | 10.00 | 4455.52 | 4459.55 | | 4459.55 | 0.000005 | 0.17 | 1814.72 | 462.11 | 0.01 |
| | 142.5" | 300.00 | 10.00 | 4455.48 | 4459.55 | | 4459.55 | 0.000005 | 0.16 | 1845.94 | 465.59 | 0.01 |
| | | | . ,,,,,,, | 7-00.40 | 7,00.00 | | | 0.000003 | J. 10 | 1073.34 | 703.331 | 0.01 |

HEC-RAS Plan: DDCarat-4RCB River: Whites Creek Reach: Central Channel (Continued)

| HEC-R | AS Plan | n: DDCarat
River Sta | -4RCB Riv | ver: Whites C | | | | | | | | | |
|--|---|-------------------------|------------------|-----------------|-------------------------------|-------------------------------|--------------------|-------------------------------|----------------------------------|----------------------|----------------------------|----------------------------|----------------------|
| | ARCA1 | MARI 200 | Q Total
(cfs) | Length Chni | Min Ch El | W.S. Elev | Crit W.S. | E.G. Elev | E.G. Slope | Vel Chril | Flow Area | Top Width | Froude # Chi |
| Central C | hannel | 141.666° | 300.00 | (ft)
10.00 | (ft)
4455.43 | (ft)
4459.55 | (批) | (ft)
4459.55 | (ft/ft)
0.000005 | (ft/s)
0.16 | (sq ft) | (ft) | 0.01 |
| Central C | | 140.633* | 300.00 | | 4455.39 | L | | 4459.55 | 0.000004 | 0.16 | 1882.64
1916.28 | 469.44
473.82 | 0.01 |
| Pentral C | | 140 | 300.00 | | | 4459.55 | | 4459.55 | 0.000004 | 0.15 | 1952.33 | 479.21 | 0.01 |
| | hannel | 139.* | 300.00 | | | 4459.55 | | 4459.55 | 0.000004 | 0.16 | 1922.99 | 468.30 | 1 |
| Central C | hannel | 138.* | 300.00 | | | 4459.55 | - | .4459.55 | 0.000004 | 0.16 | 1892.76 | 457.41 | 0.01 |
| Central C | hanne! | 137.* | 300.00 | 10.00 | | 4459.55 | | 4459.55 | 0.000004 | 0.16 | 1865.93 | 446.56 | 0.01 |
| Central C | hannel | 136.* | 300.00 | 10.00 | 4455.18 | 4459.55 | | 4459.55 | 0.000004 | 0.16 | 1833.85 | 435.69 | 0.01 |
| Central C | hannel | 135.* | 300.00 | 10.00 | 4455.14 | 4459.55 | | 4459.55 | 0.000005 | 0.17 | 1800.89 | 424.84 | 0.01 |
| Central C | hannel | 134.* | 300.00 | 10.00 | 4455.10 | 4459.55 | · | 4459.55 | 0.000005 | 0.17 | 1767.07 | 414.00 | 0.01 |
| Central C | | 133.* | 300.00 | 10.00 | | 4459.55 | | 4459.55 | 0.000005 | 0.17 | 1732.37 | 403.18 | 0.01 |
| Central C | | 132.* | 300.00 | 10.00 | | 4459.55 | | 4459.55 | 0.000005 | 0.18 | 1700.70 | 392.40 | 0.01 |
| Central C | | 131.* | 300.00 | 10.00 | <u> </u> | 4459.55 | | 4459.55 | 0.000005 | 0.18 | 1663.98 | 381.61 | 0.02 |
| Central C | | 130
129. | 300.00 | | | | | 4459.55 | 0.000005 | 0.18 | 1626.57 | | 0.02 |
| Central C | | 128.* | 300.00 | 10.00 | | 4459.55
4459.55 | | 4459.55 | 0.000006 | 0.19 | 1574.22 | 357.63 | 0.02 |
| Central C | | 127.* | 300.00 | 10.00 | | | | 4459.55
4459.55 | 0.000006 | 0.20 | 1524.18 | 344.48 | 0.02 |
| Central C | | 126.* | 300.00 | | 4454.76 | | | 4459.55 | 0.000007 | 0.20 | 1469.52
1413.79 | 331.33
318.20 | 0.02
0.02 |
| | | 125.* | 300.00 | 10.00 | | 4459.55 | | 4459.55 | 0.000007 | 0.21 | 1359.78 | 305.13 | 0.02 |
| Central C | hannel | 124.* | 300.00 | 10.00 | 4454.67 | 4459.55 | | 4459.55 | 0.000008 | 0.23 | 1301.74 | 292.05 | 0.02 |
| Central C | | 123.* | 300.00 | 10.00 | | 4459.55 | , | 4459.55 | 0.0000091 | 0.24 | 1242.64 | 279.00 | 0.02 |
| Central C | hannel | 122.* | 300.00 | 10.00 | 4454.59 | 4459.55 | | 4459.55 | 0.000010 | 0.25 | 1182.45 | 265.96 | 0.02 |
| Central C | | 121. | 300.00 | 10.00 | 4454.54 | 4459.55 | | 4459.55 | 0.000011 | 0.27 | 1123.45 | 252.99 | 0.02 |
| Central C | | 120 | 300.00 | 10.00 | 4454.50 | 4459.55 | | 4459.55 | 0.000013 | 0.28 | 1060.98 | 240.00 | 0.02 |
| Central C | | 118.333* | 300.00 | | 4454.46 | 4459.55 | | 4459.55 | 0.000014 | 0.30 | 1002.61 | 225.78 | 0.03 |
| Central C | | 116.666° | 300.00 | 10.00 | 4454.42 | | | 4459.55 | 0.000016 | 0.32 | 943.33 | 211.60 | 0.03 |
| Central C | | 115.*
113.333 | 300.00 | 10.00 | 4454.38
4454.33 | 4459.55
4459.55 | | 4459.55 | 0.000018. | 0.34 | 882.72 | 197.32 | 0.03 |
| Central C | | 111.666* | 300.00 | 10.00 | 4454.33
4454.29 | 4459.55
4459.55 | | 4459.55
4459.55 | 0.000021 | 0.36 | 822.67
759.54 | 183.10
168.76 | 0.03 |
| Central C | | 110 | 300.00 | 10.00 | 4454.25 | 4459.55 | | 4459.55 | 0.000024 | 0.39 | 695,46 | 154.45 | 0.03 |
| Central C | | 109.285* | 300.00 | 10.00 | | 4459.55 | | 4459.55 | 0.000033 | 0.46 | 650.39 | 144.21 | 0.04 |
| Central C | hannel | 108.571* | 300.00 | 10.00 | 4454.17 | 4459.55 | | 4459.55 | 0.000038 | 0.50 | 604.42 | 133.92 | 0.04 |
| Central C | hannel :: | 107.857* | 300.00 | 10.00 | 4454.13 | 4459.55 | | 4459.55 | 0.000045 | 0.54 | 557.83 | 123.66 | 0.04 |
| Central C | hannel 🐤 | 107.142° | 300.00 | 10.00 | 4454.10 | 4459.55 | | 4459.55 | 0.000054 | 0.59 | 509.36 | 113.37 | 0.05 |
| Central C | | 106.428* | 300.00 | | 4454.06 | 4459.54 | | 4459.55 | 0.000067 | 0.65 | 461.30 | 103.10 | 0.05 |
| Central C | | 105,714* | 300.00 | | 4454.02 | 4459.54 | | 4459.55 | 0.000084 | 0.73 | 412.29 | 92.77 | 0.06 |
| Central C | | 105
103,333° | 300.00 | 8.33 | 4453.98 | 4459.54 | | 4459.55 | 0.000111 | 0.83 | 362.58 | 82.47 | 0.07 |
| مستونينسا | | 101.666* | 300.00 | 8.33
8.33 | 4453.93
4453.88 | 4459.54
4459.53 | | 4459.55 | 0.000132 | 0.90 | 331.63 | 74.66 | 80.0 |
| Central C | 17 17 Nov. 18 18 18 18 18 18 18 18 18 18 18 18 18 | 100 T | 300.00 | 115,00 | 4453.83 | 4459.53 | 4456.51 | 4459.55
4459.51 | 0.000160 | 1.00
4.68 | 299.97
64.08 | 66.84
57.51 | 0.08 |
| Central C | | 97 | Culvert - | 110.00 | 4400.00 | 7703.17 | 4-30.51 | 7700.01 | 0.002039 | 4.00 | 04,00 | 57.51 | 0.30 |
| Central C | | 95 | 300.00 | 110.00 | 4453.25 | 4455.14 | 4455.93 | 4457.86 | 0.054386 | 13.24 | 22.66 | 15.15 | 0.36 |
| Central C | hannel + | 90 | 300.00 | 30.00 | 4453.14 | 4454.99 | 4454.61 | 4455.37 | 0.010019 | 4.99 | 60.13 | 38.09 | 0.70 |
| Central C | | 80 | 300.00 | 100.00 | 4453.11 | 4454.97 | · · · · · · i | 4455.13 | 0.003724 | 3.18 | 94.35 | 56.19 | 0.43 |
| Central C | | 70 | 300.00 | 100.00 | 4453.00 | 4454.71 | | 4454.81 | 0.002534 | 2.54 | 118.25 | 74.26 | 0.35 |
| Central C | | 60 | 300.00 | 100.00 | 4452.90 | 4454.52 | | 4454.59 | 0.001841 | 2.11 | 142.12 | 92.71 | 0.30 |
| Central C | | 50 | 300.00 | 100.00 | 4452.80 | 4454.37 | | 4454.42 | 0.001417 | 1.83 | 163.98 | 109.05 | 0.26 |
| Central C | | 40
30 | 300.00 | 100.00 | 4452.70 | | | 4454.27 | 0.001561 | 1.86 | 161.04 | 112.24 | 0.27 |
| Central C | | 20 | 500.00
500.00 | 100.00 | 4452.30
4451.90 | | | 4454.00
4453.60 | 0.004009 | 3.04 | 164.73
165.24 | 111.98
112.57 | 0.44
0.44 |
| | hannel | | 500.00 | 100.00 | 4451.50 | 4453.05 | | 4453.19 | 0.003993 | 3.04 | 164.52 | 112.24 | 0.44 |
| Central C | | 9,98 | 500.00 | | 4451.10 | 4452.63 | | 4452.78 | 0.004214 | 3.08 | 162.08 | 111.63 | 0.44 |
| Central C | hannel | 9.98 | 500.00 | | 4450.70 | 4452.25 | | 4452.38 | 0.003683 | 2.91 | 171.64 | 116.43 | 0.42 |
| Central C | | 9.97 | 500.00 | 100.00 | 4450.30 | 4451.86 | | 4452.00 | 0.003999 | 3.04 | 164.66 | 111.63 | 0.44 |
| Central C | | 9.96 | 500.00 | 100.00 | 4449.90 | 4451.46 | | 4451.60 | 0.003962 | 3.02 | 165.38 | 112.08 | 0.44 |
| Central C | | 9.95 | 500.00 | 100.00 | 4449.50 | 4451.07 | | 4451.21 | 0.003825 | 2.98 | 167.85 | 113.32 | 0.43 |
| Central C | | 9.94 | 500.00 | 100.00 | 4449.10 | 4450.71 | | 4450.84 | 0.003565 | 2.93 | 170.85 | 112.32 | 0.42 |
| Central C | | 9.7 | 500.00 | 100.00 | 4448.70 | 4450.39 | i | 4450.51 | 0.003029 | 2.78 | 179.55 | 112.49 | 0.39 |
| Central C | | 9.69
9.68 | 500.00 | | 4448.30 | 4450.15 | | 4450.25 | 0.002251 | 2.54 | 197.11 | 113.64 | 0.34 |
| Central C | | 9.67 | 500.00 | 100.00 | 4447.90
4447.50 | 4449.98
4449.88 | | 4450.06
4449.93 | 0.001494 | 2.22 | 225.03 | 116.37 | 0.28 |
| Central C | | 9.66 | 500.00 | 100.00 | 4447.10 | 4449.88 | - ! | 4449.93 | 0.000955 | 1.93 | 258.76
297.55 | 117.91 | 0.23 |
| Central C | | 9.65 | 500.00 | 100.00 | 4446.70 | 4449.77 | | 4449.80 | 0.000395 | 1.45 | 345.47 | 125.15 | 0.15 |
| description of the last of the | hannel | | 500.00 | 100.00 | 4446.30 | 4449.74 | | 4449.77 | 0.000353 | 1.45 | 403.691 | 134.44 | 0.13 |
| Central C | | 9.5 | 650.00 | 100.00 | 4445.90 | 4449.71 | | 4449.74 | 0.000312 | 1.45 | 447.55 | 135.23 | 0.14 |
| Central C | hannel | 9.45 | 650.00 | 100.00 | 4445.50 | 4449.68 | | 4449.71 | 0.000225 | 1.30 | 499.32 | 138.73 | 0.12 |
| Central C | | 9.4 | 650.00 | 140.00 | 4445.10 | 4449.67 | | 4449.69 | 0.000170 | 1.20 | 539.72 | 136.39 | 0.11 |
| Central C | | 9.32 | 650.00 | 40.00 | 4444.54 | 4449.65 | | 4449.67 | 0.000114 | 1.05 | 619.74 | 142.52 | 0.09 |
| Central C | | 9.3 | 650.00 | 90.00 | 4444.36 | 4449.03 | 4447.27 | 4449.60 | 0.003395 | 6.05 | 107.45 | 138.04 | 0.49 |
| Central C | | 9.29 | Culvert | | | | | | ; | | | ! | |
| Central C | | 9.2 | 650.00 | 80.00 | 4444.02 | 4446.95 | 4446.95 | 4448.39 | 0.016005 | 9.63 | 67.48 | 129.46 | 0.99 |
| | | | | | | | | | | | | | |
| *entral C | hannel ! | 9.05 | 650.00 | 20.00 | 4443.70 | 4445.50 | 4444,77 | 4445.67 | 0.004003 | 3.28 | 198.00 | 119.60 | 0.45 |
| | hannel ! | | | 20.00
100.00 | 4443.70
4443.62
4443.22 | 4445.50
4445.42
4445.02 | 4444.77
4444.29 | 4445.67
4445.59
4445.19 | 0.004003
0.004001
0.004005 | 3.28
3.28
3.28 | 198.00
198.07
198.01 | 119.60
119.69
119.68 | 0.45
0.45
0.45 |

HEC-RAS Plan: DDCarat-4RCB River: Whites Creek Reach: Central Channel Culvert Table

| Reach | | River Sta | E.G. US. | W.S. U\$. | E.G. IC | E.G. OC | Min Top Rd | Culv Q | Q Weir | Delta WS | Culv Vel In | Culv Vel Out |
|-----------------|------|--------------|----------|-----------|---------|---------|------------|--------|--------|----------|-------------|--------------|
| | | <u> </u> | (ft) | (ft) | (ft) | (ft) | (ft) | (cfs) | (cfs) | (ft) | (fl/s) | (ft/s) |
| Central Channel | 152 | Culv Grp #1 | 4461.26 | 4460.93 | 4461.26 | 4461.23 | 4465.00 | 277.89 | | 1.85 | 9.85 | 10.20 |
| Central Channel | 152 | Culv Grp #2 | 4461.26 | 4461.19 | 4458.85 | 4461.26 | 4465.00 | 22.11 | | 1.47 | 7.04 | 7.04 |
| entral Channel | 97 | W.May-5'RCPs | 4459.51 | 4459.17 | 4459.51 | 4459.43 | 4460.20 | 300.00 | | 4.03 | 10.18 | 10.48 |
| entrai Channel | 9.29 | Carat5x5RCBs | 4449.60 | 4449.03 | 4449.40 | 4449.60 | 4451.36 | 650.00 | | 2.08 | 9.27 | 10.15 |





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