

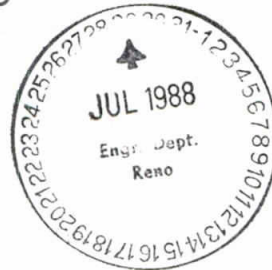
# HYDROLOGY REPORT

FOR

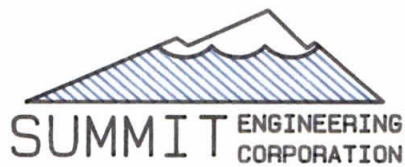
## THE VILLAGES UNIT 2 & 3

INCLUDE IN TITLE: DONNER SPRINGS  
RIO POCO

PREPARED FOR



PREPARED BY



JOB NO. 3274

JULY 1988

## INTRODUCTION

The Villages Units 2 and 3 are located on the south side of Rio Poco Road. Creekside Circle intersects Rio Poco Road and runs through The Villages Unit 2. Bayride Circle intersects Rio Poco Road and runs through The Villages Unit 3. The Villages Units 2 and 3 are contained within Assessor's Parcel Number 21-047-06. The Villages Units 2 and 3 are located in portions of sections 32 and 33 T19N, R20E. (Reference Figure 1 for a vicinity map)

The Villages Unit 1 is located north of The Villages Unit 2. Donner Springs Subdivision Unit No. 3A, Unit No. 5, and Donner Creek Village Condominiums are located to the northeast across Rio Poco Road from The Villages Units 2 and 3. The Bella Vista Ranch lies to the east of The Villages Unit 3. Rattlesnake Mountain lies to the south of The Villages Units 2 and 3.

The site is presently covered by weeds and sagebrush. The site generally slopes toward Rio Poco Road with steeper terrain toward the south. There are dirt piles scattered throughout the site. There are two buildings on the site which will be removed.

There are some minor ditches on the site. All but a portion of one of these will be filled in. The portion of the one that is not filled will be connected to the ditch that will be constructed with The Villages Unit 3. The existing channel that runs parallel to Rio Poco Road in The Villages Unit 2 will remain undisturbed. This

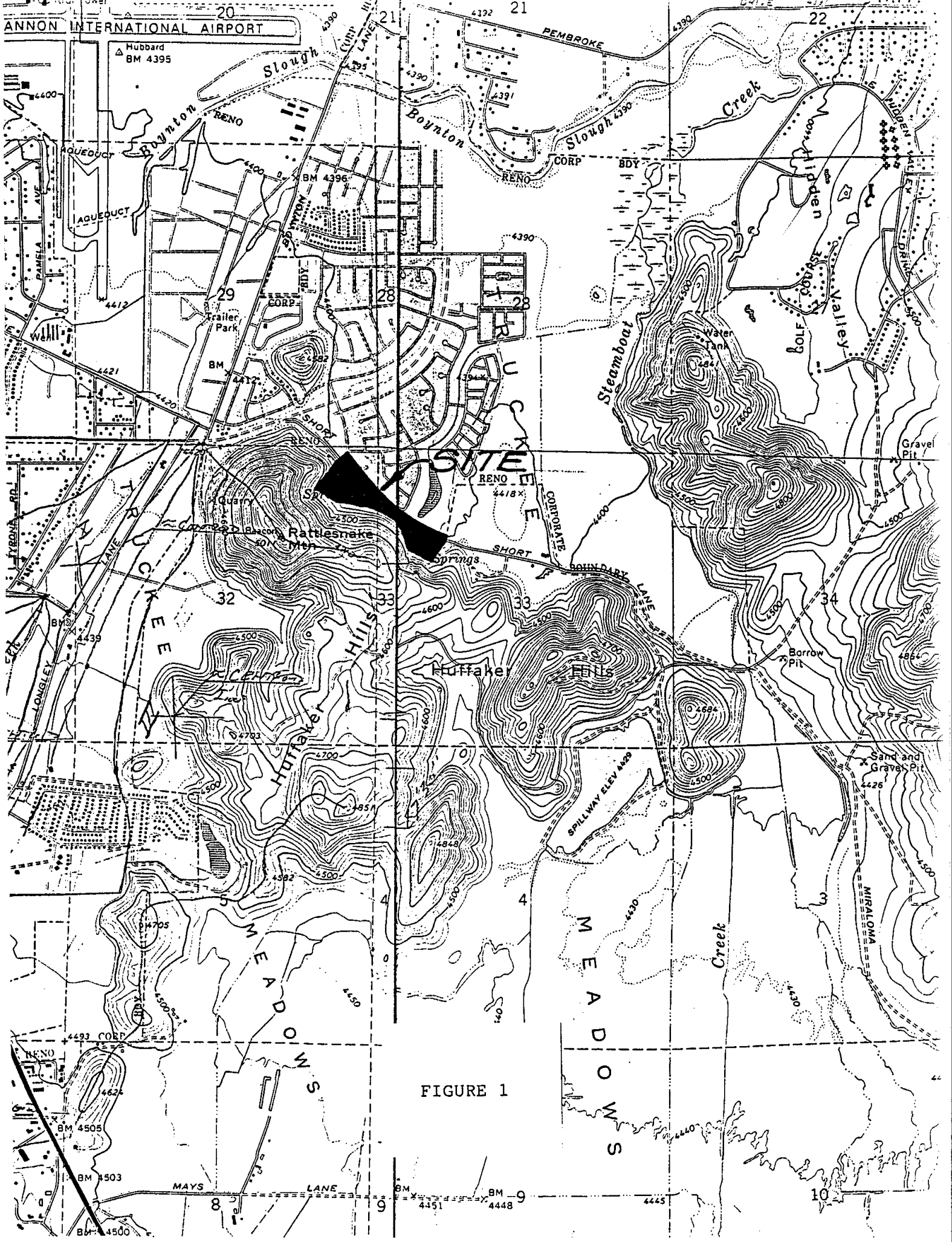


FIGURE 1

channel exits the site through 4 30-inch RCP's under Rio POCO Road. There are 2 existing catch basins on Rio POCO Road that will collect runoff from The Villages Units 2 and 3. The Villages Unit 2 and 3 are not shown to be in a Flood Hazard Zone on any FEMA map. The channel that runs parallel to Rio POCO Road is used to convey water to the pond in the Donner Creek Village Condominiums.

The Villages Units 2 and 3 will consist of 128 duplex dwelling units. A ditch to collect surface runoff from Rattlesnake Mountain will be constructed along the south side of the project. A french sub-drain will be constructed there also. The hydrology of nearby developments was studied in the various hydrology reports for those developments.

#### HYDROLOGIC ANALYSIS METHODS

Two methods of hydrologic analysis were employed in this report. SCS methods were used to study the existing state hydrology and the overall proposed state hydrology. The ditches on the south side of the project were also analyzed using SCS methods. The individual catch basins located on the streets within the project were analyzed using the Rational Method.

#### SCS METHODOLOGY

The SCS method for analyzing urban hydrology, uses the "unit hydrograph concept". This concept uses two major assumptions: (1)

For a given basin similar types of storms will produce runoff hydrographs of similar shapes, and (2) that the hydrologic system described by the unit hydrograph is a linear system. These assumptions imply that by knowing the ordinates for a unit hydrograph, (a storm which produces one inch of runoff), a hydrograph for a storm which produces two inches can be determined by multiplying all the known ordinates by two. The definition of the unit hydrograph, is a hydrograph representing one unit (one inch) of direct runoff from a rainfall excess of some unit duration and specific area distribution. The SCS has developed a typical unit hydrograph for use with a 3-hour, 6-hour, and 24-hour duration storm. This SCS unit hydrograph also pertains to a rainfall that falls over the entire watershed; not parts of it, but over the whole area.

Also, to be able to attenuate the flows from one subarea to and through another subarea, a flood routing process is performed with the hydrograph. The Muskingum routing method was used for channel routing and the Modified Puls routing method was used for the storage or detention routing. These flood routing procedures define a process of tracing, by calculation, the course and character of a flood wave as it progresses through a channel reach or storage pond. This attenuation of the flood wave actually produces a longer and lower flood wave as it moves downstream.

The SCS method requires three calculated items for analyzing each subarea: (1) The total area of the subarea; (2) the weighted

curve number of the subarea, and (3) the lag time derived from the channel lengths velocity.

The subarea weighted curve numbers were derived from combining the various improved and unimproved areas within each subarea pertaining to the different soil types as established by the SCS Soil Survey of Washoe County, Nevada, South Part, and calculating the average of the different condition curve numbers.

The subarea lag time was calculated using channel lengths and velocity charts. The SCS velocity chart was utilized. The precipitation values were taken from National Oceanic and Atmospheric Administration (NOAA) Atlas II Isopluvials, dated 1973.

The channel routing process and the reservoir routing process were calculated by using the Muskingum method and the Modified Puls method, respectively. The Muskingum method requires a storage constant (k), and an inflow, outflow constant (x) for each channel reach. The Modified Puls method requires the storage-discharge curve data for each reservoir (detention pond).

#### THE RATIONAL METHOD

The Rational Method has been in widespread use for smaller areas (i.e. less than 20 acres) for many years. The parameters for this method are:

1. Drainage Area - A
2. Time of Concentration - Tc
3. Runoff Coefficient - C
4. Rainfall Intensity - I

A weighted runoff coefficient (c) was developed using C values for different areas given in the City of Reno Policy and Procedures. This was calculated using the following equation:

$$C_{\text{weighted}} = \frac{A^1 C^1 + A^2 C^2 + A^3 C^3}{A^1 + A^2 + A^3}$$

where:

A = Area in acres

C = Runoff coefficient corresponding to that area

Average velocities for estimating travel time for overland flow were used to develop a time of concentration (reference Section 3.2 of Urban Hydrology for Small Watersheds, Technical Release No. 55). The following are the parameters used to calculate the velocity over a given watershed.

1. Watercourse slope in percent
2. Length of watercourse in feet
3. Type of watercourse

Once the velocities have been calculated, the following equation is used to determine the appropriate time of concentration (Tc).

$$Tc = L_1/V_1 + L_2/V_2 + L_3/V_3 + \dots$$

Where:

L = Length of a given section of a watercourse

V = Velocity over that given section

The time of concentration for a given area was then added to a ten-minute minimum buildup time to achieve the final time of concentration. The ten-minute buildup time was based on the City of Reno Policy and Procedures.

Using this time of concentration, an average rainfall intensity is calculated using the rainfall intensity-duration-frequency curves for the general Reno area.

The flow for each Subarea is then calculated using the rational formula:

$$Q = CIA$$

Where:

Q = Flow in CFS

C = Weighted Runoff Coefficient

I = Rainfall Intensity

A = Area in Acres

#### EXISTING STATE HYDROLOGY

In its existing state The Villages Unit 2 drains into the channel that runs parallel to Rio Poco Road. The peak flow including the contributing runoff from Rattlesnake Mountain and The Villages Unit 1 is 232 cfs during a 100-year storm and 33 cfs during a 5-year storm.

In its existing state The Villages Unit 3 drains onto Rio Poco Road. The peak flow including the contributing runoff from Rattlesnake Mountain is 39.6 cfs during a 100-year storm and 8.7 cfs during a 5-year storm.

The runoff from The Villages Units 2 and 3 passes over and under Rio Poco Road and all ends up in the Donner Creek Village Condominium Pond. During a 5-year storm the peak flow to this pond



is 35.6 cfs. The 100-year flow is 247 cfs. The 5-year flow is contained in the culverts under Rio POCO Road. The 100-year overflow of 47 cfs flows over the low point in Rio POCO Road.

The computer runs for the Existing State Hydrology can be found in Appendix A.

#### PROPOSED STATE HYDROLOGY

In the developed state the off-site runoff from Rattlesnake Mountain and the on-site runoff from the common area on the south side of project will be collected in v-ditches. These ditches were sized to carry the 100-year storm flow. These ditches flow into pipes designed for the 100-year storm. These pipes carry the flow underground to the channel which runs parallel to Rio POCO Road. A french drain will be provided under the v-ditches to collect groundwater flow from Rattlesnake Mountain.

Three catch basins will be constructed in the interior streets of the project. These catch basins will have the capacity to carry the 5-year storm flow generated within the project.

Catch Basin No. 1 (Reference Appendix B for a map showing the location of all catch basins and drainage facilities) will have a 5-year flow of 1.94 cfs. The 5-year capacity will be 2.34 cfs so there will be no 5-year overflow. The 100-year flow will be 5.53 cfs. This includes 0.26 cfs of overflow from Catch Basin No. 2. The 100-year capacity will be 3.79 cfs. The overflow of 1.74 cfs will flow onto Rio POCO Road toward existing Catch Basin No. 6.

Catch Basin No. 2 will have a 5-year flow of 1.32 cfs. The 5-year capacity will be 2.03 cfs so there will be no overflow. The 100-year flow will be 3.37 cfs. The 100-year capacity will be 3.11 cfs. The overflow of 0.26 cfs will flow toward Catch Basin No. 1.

Catch Basin No. 3 will have a 5-year flow of 1.21 cfs. The 5-year

Existing Catch Basin No. 9 will have a 5-year flow of 0.33 cfs. This Type I catch basin in a sump condition will have a 5-year capacity of 0.33 cfs with a water depth of 0.2 feet. The 100-year flow will be 0.87 cfs. The 100-year capacity will be 0.87 cfs with a water depth of 0.4 cfs.

The 5-year flow to the 4 30-inch diameter RCP culverts under Rio Poco Road is 41 cfs. The culverts have a combined capacity of 200 cfs. The 100-year flow will be 265 cfs. The 65 cfs overflow will flow over the low point in Rio Poco Road and into the pond in the Donner Creek Village Condominiums.

The hydraulic and hydrologic computations for the proposed state can be found in Appendix A.

#### CONCLUSIONS

The construction of The Villages Units 2 and 3 will have a minimal effect on the hydrology in the area. The development of The Villages Units 2 and 3 will reduce the amount of flow reaching Rio Poco Road during a 5-year storm. This is due to the fact that ditch section HC-HC and HD-HD diverts the flow from Rattlesnake Mountain away from Rio Poco Road and into the channel that runs parallel to Rio Poco Road. The 5-year flow will be reduced from 8.7 cfs to 5.8 cfs.

The flow to the 4 existing 30-inch O RCP culverts will be increased by the development of The Villages Units 2 and 3. The 5-year flow will be increased from 33 cfs to 41 cfs. The 100-year flow will be increased from 232 cfs to 265 cfs. The culverts have a combined capacity of 200 cfs so there will be no overflow during a 5-year storm. The sag vertical curve in Rio Poco Road was designed to handle an overflow of 500 cfs. Since the overflow will only be 65 cfs, therefore, no mitigating measures will be necessary.

The development of The Villages Units 2 and 3 will increase the flow to the pond in Donner Creek Village Condominiums. The 5-year contribution will be increased from 36 cfs to 45 cfs. The 100-year contribution will be increased from 247 cfs to 279 cfs. The pond was designed to handle flows in excess of 700 cfs. Therefore, no mitigating measures are necessary. Furthermore, the detention effects of the pond will serve to decrease flows downstream.

# APPENDIX A

**5-YEAR HYDROLOGY**

**EXISTING AND PROPOSED STATE**

**SCS METHODS**

-----  
TIME INCREMENT, MIN, = 5.00  
-----

DISCHARGE DIMENSION = 500.00  
-----

COMPUTE RAINFALL 5 YR  
STORM DURATION 24 HOURS WITH 1.34 " RAINFALL - TYPE II DISTRIBUTION  
-----

STATION	WEIGHT
1	1.00

AVERAGE RAINFALL, IN = 1.34  
-----

STATION	WEIGHT
1	1.00

-----  
\*\*\*\*\* ----- \*\*\*\*\*  
-----

\*\*\*\*\* ----- \*\*\*\*\*  
-----

\*\*\*\*\* EXISTING STATE HYDROLOGY \*\*\*\*\*  
-----

\*\*\*\*\* EXISTING FLOW FROM THE VILLAGES UNIT 1 \*\*\*\*\*  
-----

CATCHMENT AREA 1 , SQ. MI. = .1  
-----

SCS CURVE NUMBER = 85.00  
-----

SCS LAG, HRS = .27  
-----

COMPUTE RUNOFF @ 1

MAXIMUM FLOW = 17.73 CFS  
TIME @ MAX FLOW = 730.00 MINUTES  
-----

VOLUME IN AC. FT. @ CP # 1 = 1.89027986807  
-----

CATCHMENT AREA 2 , SQ. MI. = .0156  
-----

SCS CURVE NUMBER = 85.00  
-----

-----  
SCS LAG, HRS = .10  
-----

COMPUTE RUNOFF @ 2

MAXIMUM FLOW = 4.13 CFS  
TIME @ MAX FLOW = 720.00 MINUTES  
-----

VOLUME IN AC. FT. @ CP # 2 = .292731576277  
-----

MUSKINGUM K, HRS. = 0.00  
-----

MUSKINGUM X = .25  
-----

MUSKINGUM ROUTE FROM 1 TO 2

MAXIMUM CONTRIBUTION = 17.73  
MAXIMUM FLOW = 19.88  
TIME @ MAX FLOW = 730.00 MINUTES  
-----

\*\*\*\*\* EXISTING FLOW FROM THE VILLAGES \*\*\*\*\*  
-----

\*\*\*\*\* UNIT 2 INCLUDING RATTLESNAKE \*\*\*\*\*  
-----

\*\*\*\*\* MTN. TO THE CHANNEL RUNNING \*\*\*\*\*  
-----

\*\*\*\*\* PARALLEL TO RIO POCO ROAD \*\*\*\*\*  
-----

CATCHMENT AREA 3 , SQ. MI. = .1  
-----

SCS CURVE NUMBER = 85.00  
-----

SCS LAG, HRS = .39  
-----

COMPUTE RUNOFF @ 3

MAXIMUM FLOW = 14.18 CFS  
TIME @ MAX FLOW = 740.00 MINUTES  
-----

VOLUME IN AC. FT. @ CP # 3 = 1.89042143355

---

\*\*\*\*\* ROUTE UNIT 1 TO UNIT 2 \*\*\*\*\*

---

\*\*\*\*\* TOTAL EXISTING STATE FLOW TO EXISTING \*\*\*\*\*

---

\*\*\*\*\* 4-30 INCH RCP CULVERTS UNDER RIO POCO ROAD \*\*\*\*\*

---

MUSKINGUM K, HRS. = .13

---

MUSKINGUM X = .25

---

MUSKINGUM ROUTE FROM 2 TO 3

MAXIMUM CONTRIBUTION = 18.59  
MAXIMUM FLOW = 32.77  
TIME @ MAX FLOW = 740.00 MINUTES

---

\*\*\*\*\* EXISTING STATE FLOW FROM THE VILLAGES \*\*\*\*\*

---

\*\*\*\*\* UNIT 2 AND 3 TO RIO POCO ROAD \*\*\*\*\*

---

CATCHMENT AREA 4 , SQ. MI. = .0356

---

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .12

---

COMPUTE RUNOFF @ 4

MAXIMUM FLOW = 8.71 CFS  
TIME @ MAX FLOW = 725.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 4 = .66735800492

---

\*\*\*\*\* TOTAL EXISTING STATE FLOW TO THE \*\*\*\*\*

---

\*\*\*\*\* POND IN DONNER CREEK VILLAGE CONDOMINIUMS \*\*\*\*\*

---



MUSKINGUM K, HRS. = 0.00

MUSKINGUM X = .25

MUSKINGUM ROUTE FROM 3 TO 4

MAXIMUM CONTRIBUTION = 32.77  
MAXIMUM FLOW = 35.57  
TIME @ MAX FLOW = 740.00 MINUTES

\*\*\*\*\* ----- \*\*\*\*\*

\*\*\*\*\* ----- \*\*\*\*\*

\*\*\*\*\* PROPOSED STATE HYDROLOGY \*\*\*\*\*

\*\*\*\*\* FLOW TO DITCH SECTION HA-HA \*\*\*\*\*

\*\*\*\*\* TOTAL FLOW TO 30 INCH RCP INLET \*\*\*\*\*

CATCHMENT AREA 5, SQ. MI. = .0382

SCS CURVE NUMBER = 85.00

SCS LAG, HRS = .07

COMPUTE RUNOFF @ 5

MAXIMUM FLOW = 11.91 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

VOLUME IN AC. FT. @ CP # 5 = .737787354258

\*\*\*\*\* FLOW TO DITCH SECTION HB-HB \*\*\*\*\*

CATCHMENT AREA 6, SQ. MI. = .0447

SCS CURVE NUMBER = 85.00

SCS LAG, HRS = .08

---

COMPUTE RUNOFF @ 6

MAXIMUM FLOW = 13.30 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 6 = .860149860669

---

\*\*\*\*\* FLOW TO DITCH SECTION HC-HC AND HD-HD \*\*\*\*\*

---

CATCHMENT AREA 7 , SQ. MI. = .0279

---

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .14

---

COMPUTE RUNOFF @ 7

MAXIMUM FLOW = 6.75 CFS  
TIME @ MAX FLOW = 725.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 7 = .52466926409

---

\*\*\*\*\* PROPOSED STATE FLOW FROM THE VILLAGES \*\*\*\*\*

---

\*\*\*\*\* UNIT 1 AND 2 AND RIO POCO ROAD TO THE \*\*\*\*\*

---

\*\*\*\*\* EXISTING CHANNEL RUNNING PARALLEL TO RIO POCO ROAD \*\*\*\*\*

---

CATCHMENT AREA 8 , SQ. MI. = .0225

---

SCS CURVE NUMBER = 92.00

---

SCS LAG, HRS = .31

---

COMPUTE RUNOFF @ 8

MAXIMUM FLOW = 7.69 CFS  
TIME @ MAX FLOW = 730.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 8 = .802316131595

---

\*\*\*\*\* PROPOSED STATE FLOW FROM THE VILLAGES \*\*\*\*\*

---

\*\*\*\*\* UNIT 2 AND 3 TO RIO POCO ROAD \*\*\*\*\*

---

CATCHMENT AREA 9 , SQ. MI. = .0108

---

SCS CURVE NUMBER = 92.00

---

SCS LAG, HRS = .10

---

COMPUTE RUNOFF @ 9

MAXIMUM FLOW = 5.78 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 9 = .382342218658

---

\*\*\*\*\* ROUTE FLOW FROM THE VILLAGES UNIT 1 \*\*\*\*\*

---

\*\*\*\*\* TO THE 4 EXISTING 30 INCH RCP CULVERTS \*\*\*\*\*

---

\*\*\*\*\* UNDER RIO POCO ROAD \*\*\*\*\*

---

MUSKINGUM K, HRS. = .13

---

MUSKINGUM X = .25

---

MUSKINGUM ROUTE FROM 2 TO 8

MAXIMUM CONTRIBUTION = 18.59  
MAXIMUM FLOW = 25.29  
TIME @ MAX FLOW = 740.00 MINUTES

---

\*\*\*\*\* ROUTE FLOW FROM DITCH SECTION HA-HA \*\*\*\*\*

---

\*\*\*\*\* TO THE 4 EXISTING 30 INCH RCP \*\*\*\*\*

\*\*\*\*\* CULVERTS UNDER RIO POCO ROAD \*\*\*\*\*

MUSKINGUM K, HRS. = .13

MUSKINGUM X = .25

MUSKINGUM ROUTE FROM 5 TO 8

MAXIMUM CONTRIBUTION = 9.47  
MAXIMUM FLOW = 32.38  
TIME @ MAX FLOW = 735.00 MINUTES

\*\*\*\*\* ROUTE FLOW FROM DITCH SECTION HB-HB, \*\*\*\*\*

\*\*\*\*\* HC-HC AND HD-HD TO 36 INCH RCP INLET \*\*\*\*\*

\*\*\*\*\* TOTAL FLOW TO PROPOSED 36 INCH RCP INLET \*\*\*\*\*

MUSKINGUM K, HRS. = 0.00

MUSKINGUM X = .25

MUSKINGUM ROUTE FROM 6 TO 7

MAXIMUM CONTRIBUTION = 13.30  
MAXIMUM FLOW = 19.28  
TIME @ MAX FLOW = 720.00 MINUTES

\*\*\*\*\* ROUTE FLOW FROM 36 INCH RCP INLET \*\*\*\*\*

\*\*\*\*\* TO THE 4 EXISTING 30 INCH \*\*\*\*\*

\*\*\*\*\* RCP CULVERTS UNDER RIO POCO ROAD \*\*\*\*\*

\*\*\*\*\* TOTAL FLOW TO 4 EXISTING 30 INCH CULVERTS \*\*\*\*\*

MUSKINGUM K, HRS. = 0.00

MUSKINGUM X = .25

-----  
MUSKINGUM ROUTE FROM 7 TO 8

MAXIMUM CONTRIBUTION = 19.28  
MAXIMUM FLOW = 41.11  
TIME @ MAX FLOW = 730.00 MINUTES  
-----

\*\*\*\*\* TOTAL PROPOSED STATE CONTRIBUTION \*\*\*\*\*  
-----

\*\*\*\*\* TO THE POND IN DONNER CREEK \*\*\*\*\*  
-----

\*\*\*\*\* VILLAGE CONDOMINIUMS FROM THE VILLAGES 1,2 AND 3 \*\*\*\*\*  
-----

MUSKINGUM K, HRS. = 0.00  
-----

MUSKINGUM X = .25  
-----

MUSKINGUM ROUTE FROM 8 TO 9

MAXIMUM CONTRIBUTION = 41.11  
MAXIMUM FLOW = 45.23  
TIME @ MAX FLOW = 725.00 MINUTES  
-----

NORMAL TERMINATION  
TIME FOR THIS RUN 00:03:53

**100-YEAR HYDROLOGY**

**EXISTING AND PROPOSED STATE**

**SCS METHODS**

-----  
TIME INCREMENT, MIN, = 5.00  
-----

DISCHARGE DIMENSION = 500.00  
-----

COMPUTE RAINFALL 100 YR  
STORM DURATION 24 HOURS WITH 2.88 " RAINFALL - TYPE II DISTRIBUTION  
-----

STATION	WEIGHT
1	1.00

AVERAGE RAINFALL, IN = 2.88  
-----

STATION	WEIGHT
1	1.00

-----  
\*\*\*\*\* ----- \*\*\*\*\*  
-----

\*\*\*\*\* ----- \*\*\*\*\*  
-----

\*\*\*\*\* EXISTING STATE HYDROLOGY \*\*\*\*\*  
-----

\*\*\*\*\* EXISTING FLOW FROM THE VILLAGES UNIT 1 \*\*\*\*\*  
-----

CATCHMENT AREA 1 , SQ. MI. = .1  
-----

SCS CURVE NUMBER = 85.00  
-----

SCS LAG, HRS = .27  
-----

COMPUTE RUNOFF @ 1

MAXIMUM FLOW = 83.47 CFS  
TIME @ MAX FLOW = 730.00 MINUTES  
-----

VOLUME IN AC. FT. @ CP # 1 = 7.9441261789  
-----

CONTROL POINT = 1.00  
BASEFLOW, CFS = 79.00  
-----

CATCHMENT AREA 2 , SQ. MI. = .0156

---

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .10

---

COMPUTE RUNOFF @ 2

MAXIMUM FLOW = 18.60 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 2 = 1.23023929831

---

MUSKINGUM K, HRS. = 0.00

---

MUSKINGUM X = .25

---

MUSKINGUM ROUTE FROM 1 TO 2

MAXIMUM CONTRIBUTION = 162.47  
MAXIMUM FLOW = 171.13  
TIME @ MAX FLOW = 730.00 MINUTES

---

\*\*\*\*\* EXISTING FLOW FROM THE VILLAGES \*\*\*\*\*

---

\*\*\*\*\* UNIT 2 INCLUDING RATTLESNAKE \*\*\*\*\*

---

\*\*\*\*\* MTN. TO THE CHANNEL RUNNING \*\*\*\*\*

---

\*\*\*\*\* PARALLEL TO RIO POCO ROAD \*\*\*\*\*

---

CATCHMENT AREA 3 , SQ. MI. = .1

---

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .39

---

COMPUTE RUNOFF @ 3



MAXIMUM FLOW = 67.21 CFS  
TIME @ MAX FLOW = 735.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 3 = 7.94472112468

---

\*\*\*\*\* ROUTE UNIT 1 TO UNIT 2 \*\*\*\*\*

---

\*\*\*\*\* TOTAL EXISTING STATE FLOW TO EXISTING \*\*\*\*\*

---

\*\*\*\*\* 4-30 INCH RCP CULVERTS UNDER RIO POCO ROAD \*\*\*\*\*

---

MUSKINGUM K, HRS. = .13

---

MUSKINGUM X = .25

---

MUSKINGUM ROUTE FROM 2 TO 3

MAXIMUM CONTRIBUTION = 165.73  
MAXIMUM FLOW = 232.06  
TIME @ MAX FLOW = 740.00 MINUTES

---

\*\*\*\*\* EXISTING STATE FLOW FROM THE VILLAGES \*\*\*\*\*

---

\*\*\*\*\* UNIT 2 AND 3 TO RIO POCO ROAD \*\*\*\*\*

---

CATCHMENT AREA 4 , SQ. MI. = .0356

---

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .12

---

COMPUTE RUNOFF @ 4

MAXIMUM FLOW = 39.61 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 4 = 2.80465146307

---

\*\*\*\*\* TOTAL EXISTING STATE FLOW TO THE \*\*\*\*\*

---

\*\*\*\*\* POND IN DONNER CREEK VILLAGE CONDOMINIUMS \*\*\*\*\*

MUSKINGUM K, HRS. = 0.00

MUSKINGUM X = .25

MUSKINGUM ROUTE FROM 3 TO 4

MAXIMUM CONTRIBUTION = 232.06  
MAXIMUM FLOW = 246.81  
TIME @ MAX FLOW = 735.00 MINUTES

\*\*\*\*\* ----- \*\*\*\*\*

\*\*\*\*\* ----- \*\*\*\*\*

\*\*\*\*\* PROPOSED STATE HYDROLOGY \*\*\*\*\*

\*\*\*\*\* FLOW TO DITCH SECTION HA-HA \*\*\*\*\*

\*\*\*\*\* TOTAL FLOW TO 30 INCH RCP INLET \*\*\*\*\*

CATCHMENT AREA 5 , SQ. MI. = .0382

SCS CURVE NUMBER = 85.00

SCS LAG, HRS = .07

COMPUTE RUNOFF @ 5

MAXIMUM FLOW = 51.01 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

VOLUME IN AC. FT. @ CP # 5 = 3.10063918811

\*\*\*\*\* FLOW TO DITCH SECTION HB-HB \*\*\*\*\*

CATCHMENT AREA 6 , SQ. MI. = .0447

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .08

---

COMPUTE RUNOFF @ 6

MAXIMUM FLOW = 57.93 CFS  
TIME @ MAX FLOW = 720.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 6 = 3.61488218827

---

\*\*\*\*\* FLOW TO DITCH SECTION HC-HC AND HD-HD \*\*\*\*\*

---

CATCHMENT AREA 7 , SQ. MI. = .0279

---

SCS CURVE NUMBER = 85.00

---

SCS LAG, HRS = .14

---

COMPUTE RUNOFF @ 7

MAXIMUM FLOW = 29.57 CFS  
TIME @ MAX FLOW = 725.00 MINUTES

---

VOLUME IN AC. FT. @ CP # 7 = 2.20498504297

---

\*\*\*\*\* PROPOSED STATE FLOW FROM THE VILLAGES \*\*\*\*\*

---

\*\*\*\*\* UNIT 1 AND 2 AND RIO POCO ROAD TO THE \*\*\*\*\*

---

\*\*\*\*\* EXISTING CHANNEL RUNNING PARALLEL TO RIO POCO ROAD \*\*\*\*\*

---

CATCHMENT AREA 8 , SQ. MI. = .0225

---

SCS CURVE NUMBER = 92.00

---

SCS LAG, HRS = .31

-----  
COMPUTE RUNOFF @ 8

MAXIMUM FLOW = 23.61 CFS  
TIME @ MAX FLOW = 730.00 MINUTES  
-----

VOLUME IN AC. FT. @ CP # 8 = 2.4598886745  
-----

\*\*\*\*\* PROPOSED STATE FLOW FROM THE VILLAGES \*\*\*\*\*  
-----

\*\*\*\*\* UNIT 2 AND 3 TO RIO POCO ROAD \*\*\*\*\*  
-----

CATCHMENT AREA 9 , SQ. MI. = .0108  
-----

SCS CURVE NUMBER = 92.00  
-----

SCS LAG, HRS = .10  
-----

COMPUTE RUNOFF @ 9

MAXIMUM FLOW = 17.17 CFS  
TIME @ MAX FLOW = 720.00 MINUTES  
-----

VOLUME IN AC. FT. @ CP # 9 = 1.17225524506  
-----

\*\*\*\*\* ROUTE FLOW FROM THE VILLAGES UNIT 1 \*\*\*\*\*  
-----

\*\*\*\*\* TO THE 4 EXISTING 30 INCH RCP CULVERTS \*\*\*\*\*  
-----

\*\*\*\*\* UNDER RIO POCO ROAD \*\*\*\*\*  
-----

MUSKINGUM K, HRS. = .13  
-----

MUSKINGUM X = .25  
-----

MUSKINGUM ROUTE FROM 2 TO 8

MAXIMUM CONTRIBUTION = 165.73  
MAXIMUM FLOW = 187.58  
TIME @ MAX FLOW = 735.00 MINUTES

-----  
\*\*\*\*\* ROUTE FLOW FROM DITCH SECTION HA-HA \*\*\*\*\*  
-----

\*\*\*\*\* TO THE 4 EXISTING 30 INCH RCP \*\*\*\*\*  
-----

\*\*\*\*\* CULVERTS UNDER RIO POCO ROAD \*\*\*\*\*  
-----

MUSKINGUM K, HRS. = .13  
-----

MUSKINGUM X = .25  
-----

MUSKINGUM ROUTE FROM 5 TO 8

MAXIMUM CONTRIBUTION = 41.62  
MAXIMUM FLOW = 218.49  
TIME @ MAX FLOW = 735.00 MINUTES  
-----

\*\*\*\*\* ROUTE FLOW FROM DITCH SECTION HB-HB, \*\*\*\*\*  
-----

\*\*\*\*\* HC-HC AND HD-HD TO 36 INCH RCP INLET \*\*\*\*\*  
-----

\*\*\*\*\* TOTAL FLOW TO PROPOSED 36 INCH RCP INLET \*\*\*\*\*  
-----

MUSKINGUM K, HRS. = 0.00  
-----

MUSKINGUM X = .25  
-----

MUSKINGUM ROUTE FROM 6 TO 7

MAXIMUM CONTRIBUTION = 57.93  
MAXIMUM FLOW = 86.87  
TIME @ MAX FLOW = 720.00 MINUTES  
-----

\*\*\*\*\* ROUTE FLOW FROM 36 INCH RCP INLET \*\*\*\*\*  
-----

\*\*\*\*\* TO THE 4 EXISTING 30 INCH \*\*\*\*\*  
-----

\*\*\*\*\* RCP CULVERTS UNDER RIO POCO ROAD \*\*\*\*\*  
-----

\*\*\*\*\* TOTAL FLOW TO 4 EXISTING 30 INCH CULVERTS \*\*\*\*\*  
-----

MUSKINGUM K, HRS. = 0.00

---

MUSKINGUM X = .25

---

MUSKINGUM ROUTE FROM 7 TO 8

MAXIMUM CONTRIBUTION = 86.87  
MAXIMUM FLOW = 264.87  
TIME @ MAX FLOW = 725.00 MINUTES

---

\*\*\*\*\* TOTAL PROPOSED STATE CONTRIBUTION \*\*\*\*\*

---

\*\*\*\*\* TO THE POND IN DONNER CREEK \*\*\*\*\*

---

\*\*\*\*\* VILLAGE CONDOMINIUMS FROM THE VILLAGES 1,2 AND 3 \*\*\*\*\*

---

MUSKINGUM K, HRS. = 0.00

---

MUSKINGUM X = .25

---

MUSKINGUM ROUTE FROM 8 TO 9

MAXIMUM CONTRIBUTION = 264.87  
MAXIMUM FLOW = 278.78  
TIME @ MAX FLOW = 725.00 MINUTES

---

NORMAL TERMINATION  
TIME FOR THIS RUN 00:03:54

**RATIONAL METHOD CALCULATION**

**CATCH BASINS NO.'S 1, 2, 3, 6, 7, AND 8**

<u>Catch Basin No.</u>	<u>A</u> <u>Acres</u>	<u>TC</u> <u>Minute</u>	<u>I5</u>	<u>I100</u>	<u>C</u>	<u>O5</u>	<u>O100</u>
1	3.8	18.9	0.93	2.52	.55	1.94	5.27
2	1.97	12.7	1.22	3.11	.55	1.32	3.37
3	1.77	12.5	1.24	3.3	.55	1.21	3.21
6	0.70	14.0	1.14	3.0	.55	0.44	1.16
7	6.89	20.5	0.895	2.45	.55	3.39	9.28
8	3.8	20.0	0.90	2.48	.55	1.88	5.18
9	0.53	14.0	1.14	3.0	.55	0.33	0.87



HYDRAULIC CALCULATIONS

Analysis Points 4 and 5

Storm Drain Pipes

Ditch Sections HA-HA, HB-HB, HC-HC, and HD-HD

Channel Running Parallel to Rio POCO Road

Inlet Capacity of 4 30-inch  $\varnothing$  RCP Culverts

Depth of Flow in Streets

Capacity of Catch Basins 1, 2, 4, 6, 7, 8, and 9

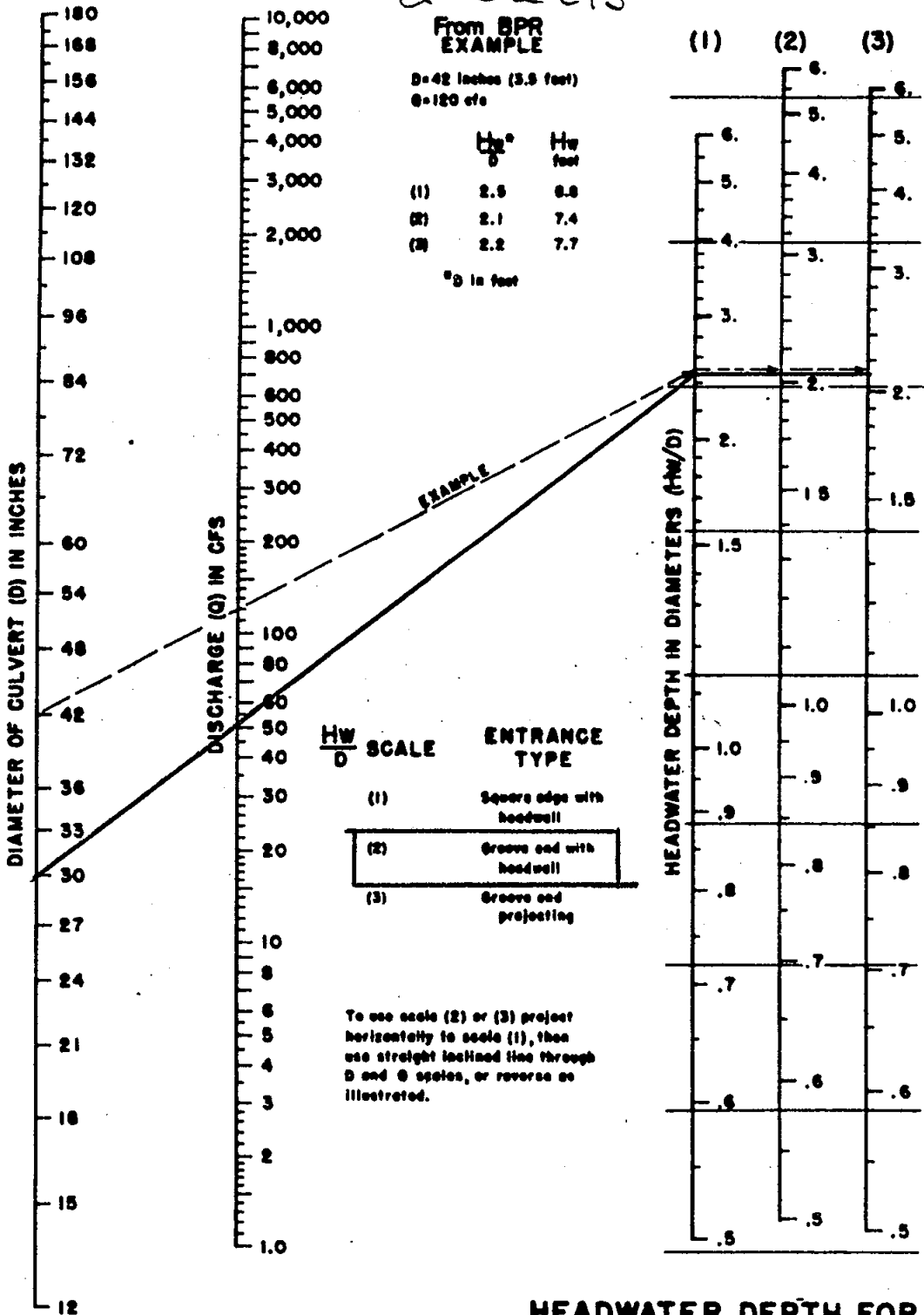
# Analysis Point #4

DRAINAGE CRITERIA MANUAL

INLETS & CULVERTS

$$HW = (2.1)(2.5) = 5.25'$$

$$Q = 52 \text{ cfs}$$



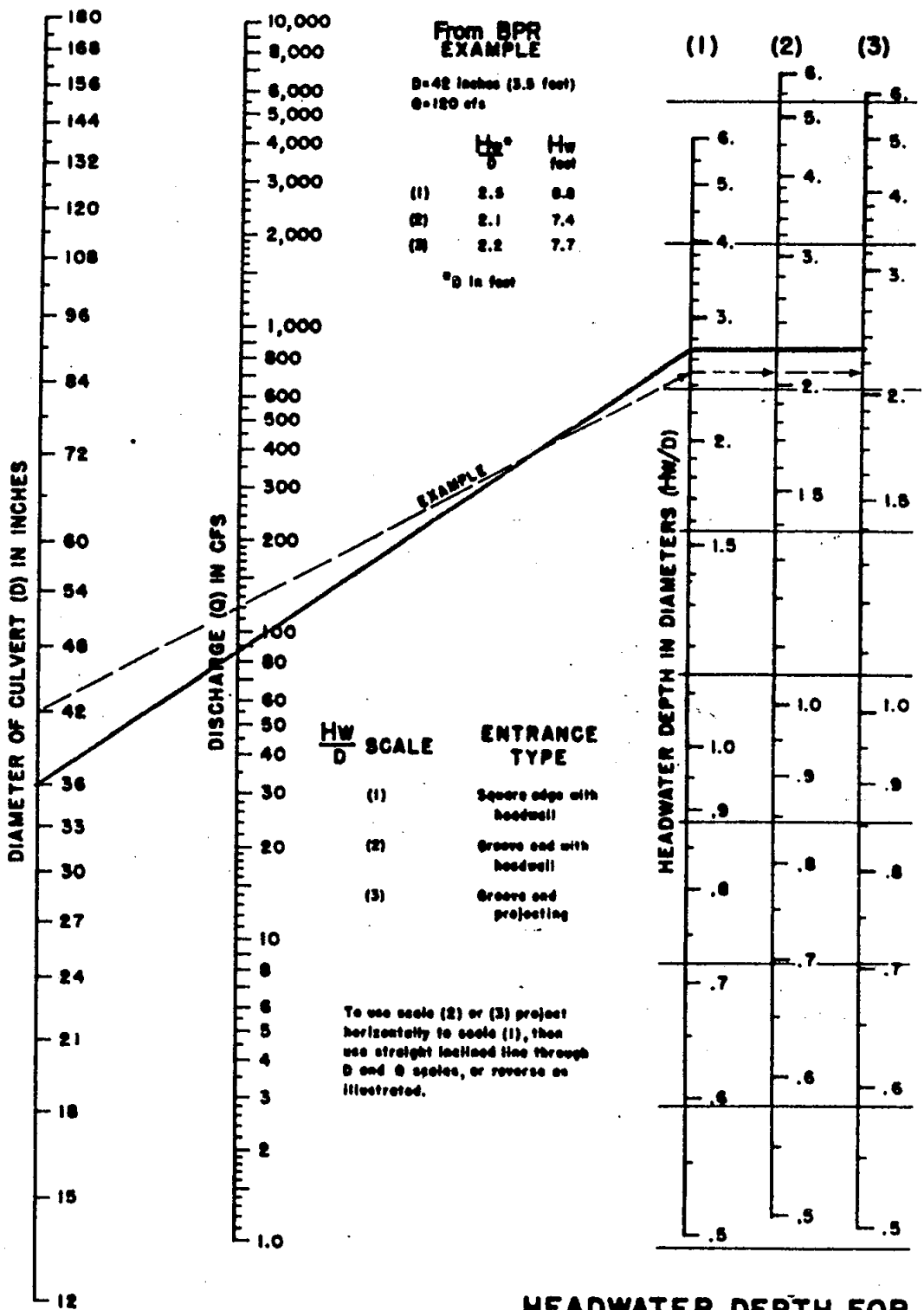
## HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL

FIGURE 10-10.

11-15-68

Denver Regional Council of Governments

Analysis Point #5  
 $Q = 87 \text{ cfs}$      $HW = (2.2)(3') = 6.6'$



HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL

FIGURE 10-10.

STORM DRAIN PIPE ANALYSIS

<u>Pipe Reach Description</u>	<u>Pipe Size</u>	<u>Pipe Slope</u>	<u>.05</u>	<u>5-Year Depth of Flow</u>	<u>Q100</u>	<u>100-Year Depth of Flow</u>
Analysis Point #4 to SDMH #1	30"	2.52%	11.9	8.7"	51.0	20.0"
Catch Basin #1 to SDMH #1	12"	1.2 %	1.94	6.0"	3.79	9.6"
Catch Basin #2 to SDMH #1	10"	12.6 %	1.32	2.8"	3.11	4.4"
SDMH #1 to SDMH #2	36"	0.8 %	15.16	12.6"	57.9	28.8"
SDMH #2 TO Outlet	36"	1.33%	15.16	11.2"	57.9	23.4"
Catch Basin to SDMH #3	10"	9.42%	1.21	2.9"	3.08	4.8"
SDMH #3 to SDMH #4	12"	2.3 %	1.21	4.0"	3.08	6.5"
SDMH #4 to SDMH #5	15"	0.25%	1.21	6.5"	3.08	11.7"
Analysis Point #5 to SDMH #5	36"	5.22%	19.3	8.6"	86.9	19.8"
SDMH #5 to Outlet	36"	1.56%	20.51	12.2"	89.98	33.8"

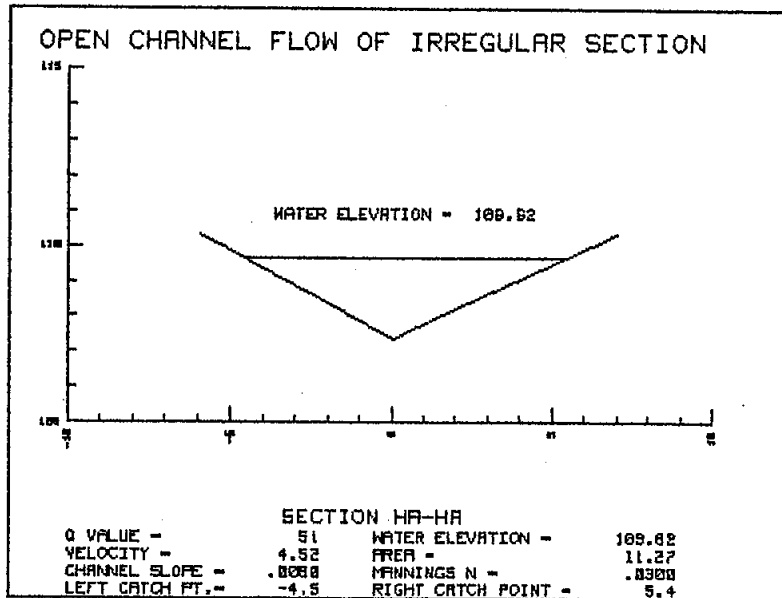
All pipes will be concrete with N = 0.013

Q VALUE = 51.0082898964  
 WATER ELEVATION = 109.620771232  
 VELOCITY = 4.52435107897  
 AREA = 11.2741670587  
 WETTED PERIMETER = 10.9248087126  
 CHANNEL SLOPE IN Ft/Ft = .008  
 MANNINGS N = .03  
 CATCH POINT ON LEFT SIDE = -4.541542464  
 CATCH POINT ON RIGHT SIDE = 5.38827072

CHANNEL COORDINATES

ELEVATION	DISTANCE
110.30	-5.90
107.35	0.00
110.30	7.00

\*\*\*\*\*

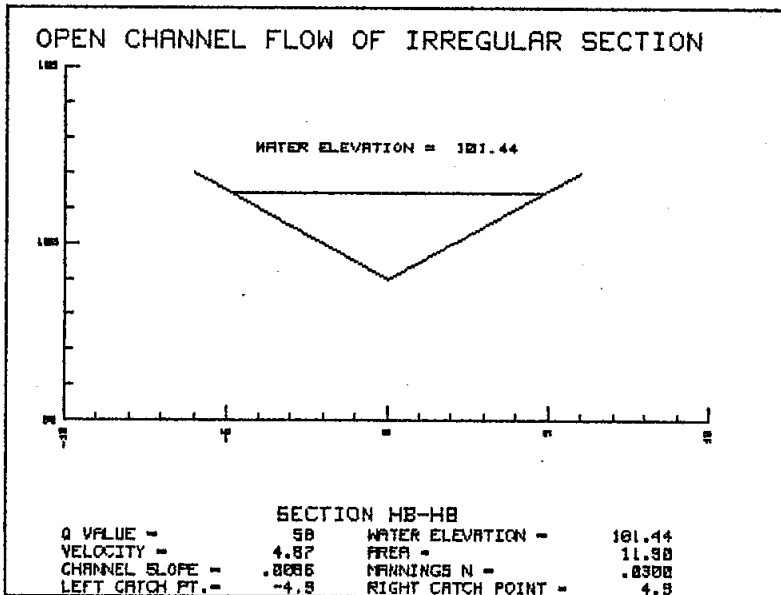


Q VALUE = 57.9256106139  
 WATER ELEVATION = 101.439250722  
 VELOCITY = 4.86774411481  
 AREA = 11.8998881715  
 WETTED PERIMETER = 10.908660858  
 CHANNEL SLOPE IN Ft/Ft = .0086  
 MANNINGS N = .03  
 CATCH POINT ON LEFT SIDE = -4.8785014444  
 CATCH POINT ON RIGHT SIDE = 4.8785014444

CHANNEL COORDINATES

ELEVATION	DISTANCE
102.00	-6.00
99.00	0.00
102.00	6.00

\*\*\*\*\*

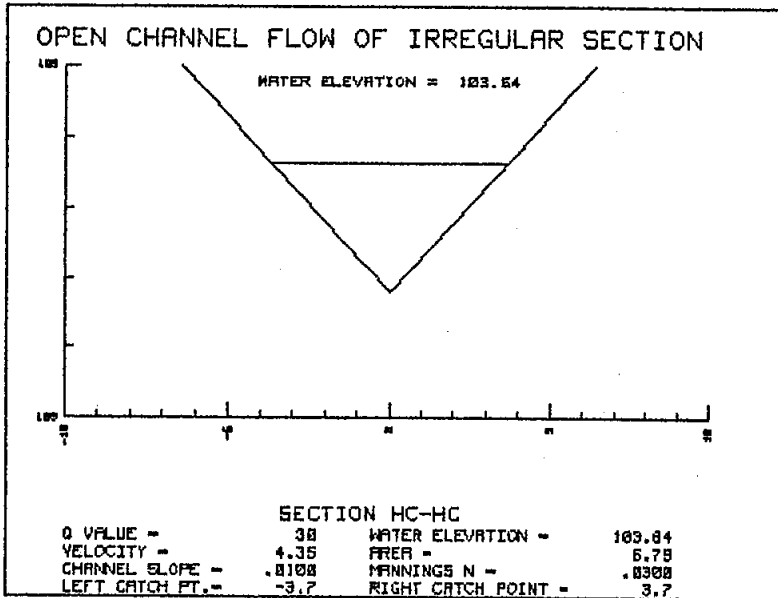


Q VALUE = 29.5758246998  
 WATER ELEVATION = 103.642891398  
 VELOCITY = 4.35419005857  
 AREA = 6.79249741101  
 WETTED PERIMETER = 8.24166088298  
 CHANNEL SLOPE IN Ft/Ft = .01  
 MANNINGS N = .03  
 CATCH POINT ON LEFT SIDE = -3.68578279637  
 CATCH POINT ON RIGHT SIDE = 3.68578279637

CHANNEL COORDINATES

ELEVATION	DISTANCE
105.00	-6.40
101.80	0.00
105.00	6.40

\*\*\*\*\*

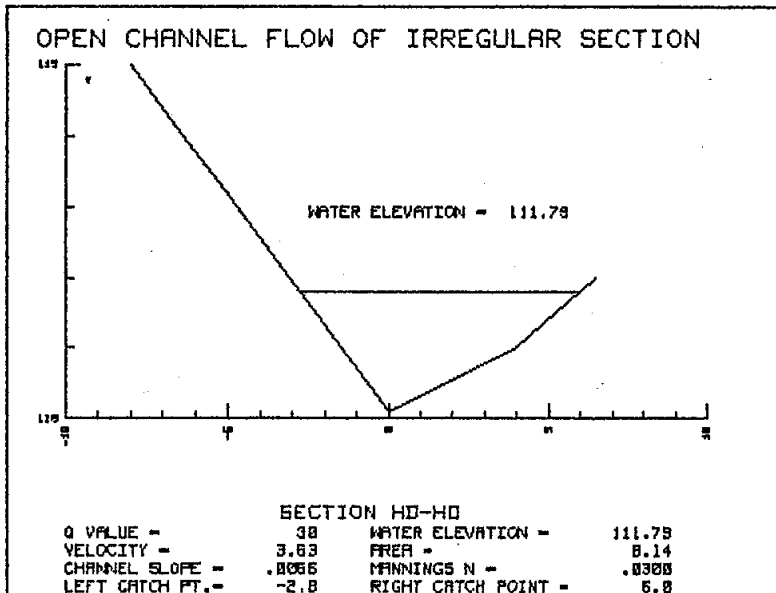


Q VALUE = 29.5760787973  
 WATER ELEVATION = 111.787962923  
 VELOCITY = 3.63359675881  
 AREA = 8.13961503175  
 WETTED PERIMETER = 9.48643542174  
 CHANNEL SLOPE IN Ft/Ft = .0066  
 MANNINGS N = .03  
 CATCH POINT ON LEFT SIDE = -2.77717548466  
 CATCH POINT ON RIGHT SIDE = 5.96990730766

CHANNEL COORDINATES

ELEVATION	DISTANCE
115.00	-8.00
110.08	0.00
111.00	4.00
112.00	6.50

\*\*\*\*\*



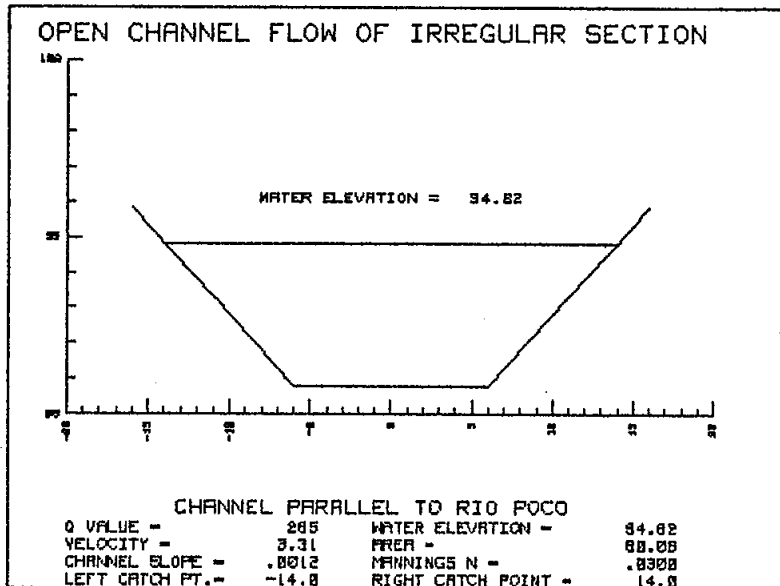


Q VALUE = 264.993334206  
 WATER ELEVATION = 94.8228576372  
 VELOCITY = 3.30910632313  
 AREA = 80.0800301744  
 WETTED PERIMETER = 29.9013235622  
 CHANNEL SLOPE IN Ft/Ft = .0012  
 MANNINGS N = .03  
 CATCH POINT ON LEFT SIDE = -14.0057152744  
 CATCH POINT ON RIGHT SIDE = 14.0057152744

CHANNEL COORDINATES

ELEVATION	DISTANCE
95.82	-16.00
90.82	-6.00
90.82	0.00
90.82	6.00
95.82	16.00

\*\*\*\*\*

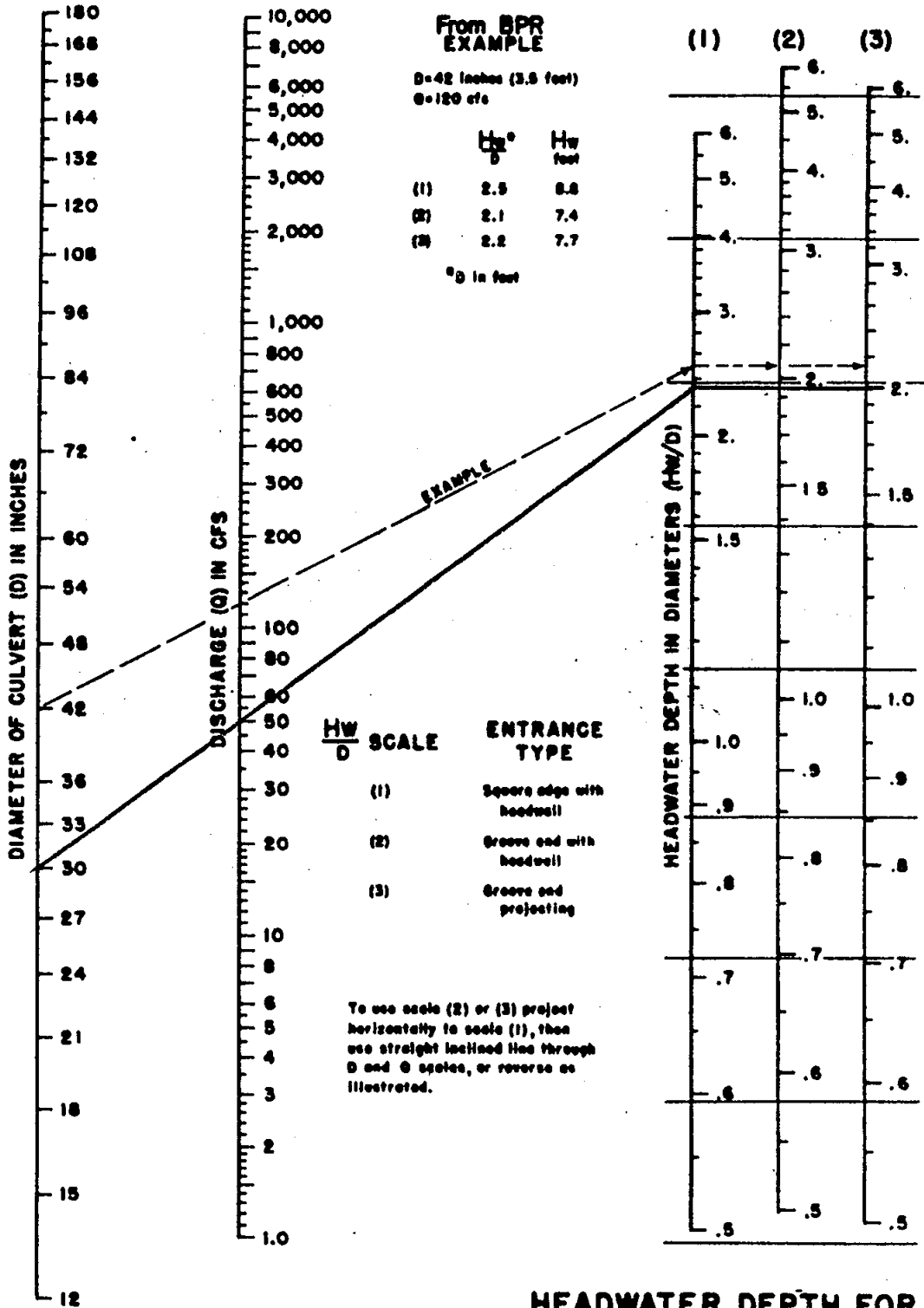


4-30 of RCP CULVERTS  
 $Q=200 \text{ cfs} \Rightarrow 50 \text{ cfs each}$

DRAINAGE CRITERIA MANUAL

INLETS & CULVERTS

$HW = (2)(2.5') = 5'$



HEADWATER DEPTH FOR  
 CONCRETE PIPE CULVERTS  
 WITH INLET CONTROL

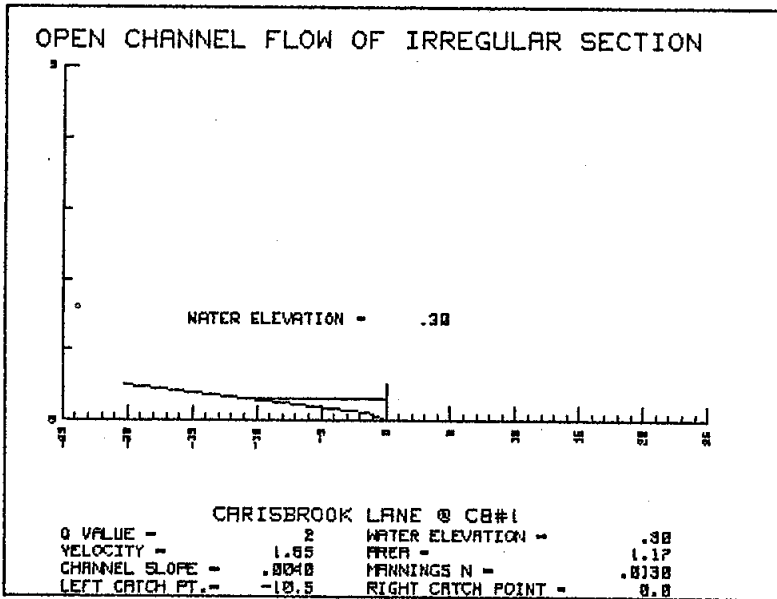
FIGURE 10-10.

Q VALUE = 1.93412341998  
 WATER ELEVATION = .30425952  
 VELOCITY = 1.64831460721  
 AREA = 1.17339457621  
 WETTED PERIMETER = 10.7780971693  
 CHANNEL SLOPE IN Ft/Ft= .004  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -10.462976  
 CATCH POINT ON RIGHT SIDE = .0486815232

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*

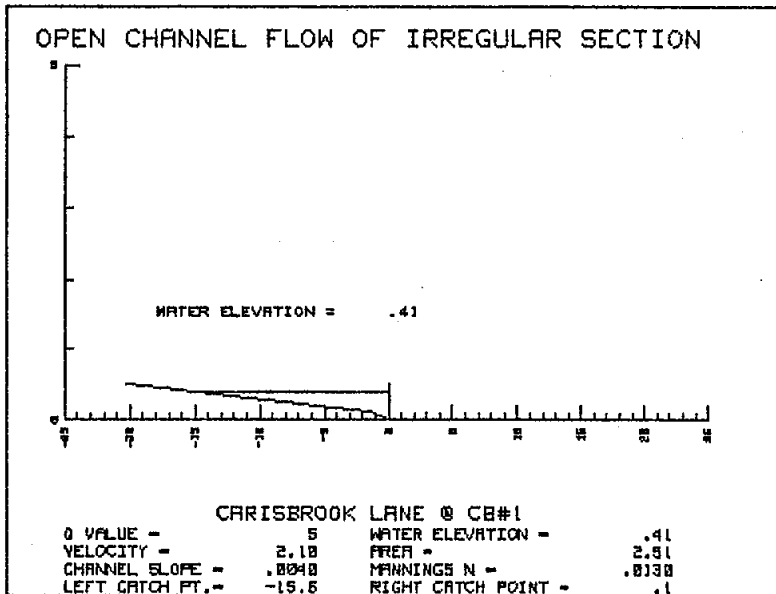


Q VALUE = 5.27508600565  
 WATER ELEVATION = .40638072576  
 VELOCITY = 2.1029595979  
 AREA = 2.50841053291  
 WETTED PERIMETER = 15.988598664  
 CHANNEL SLOPE IN Ft/Ft= .004  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -15.569036288  
 CATCH POINT ON RIGHT SIDE = .0650209161216

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*



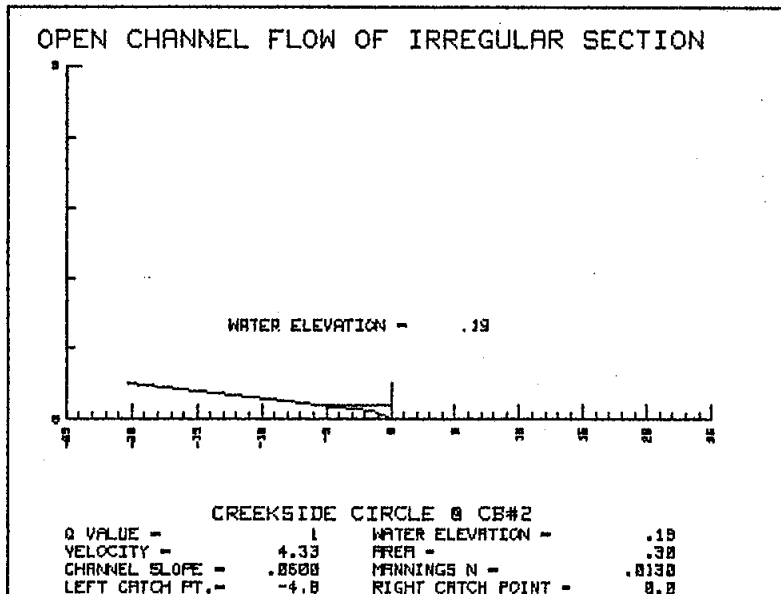
±

Q VALUE = 1.31880239545  
WATER ELEVATION = .19094048  
VELOCITY = 4.33415876035  
AREA = .304281053918  
WETTED PERIMETER = 4.99625173459  
CHANNEL SLOPE IN Ft/Ft = .06  
MANNINGS N = .013  
CATCH POINT ON LEFT SIDE = -4.797024  
CATCH POINT ON RIGHT SIDE = .0305504768

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*

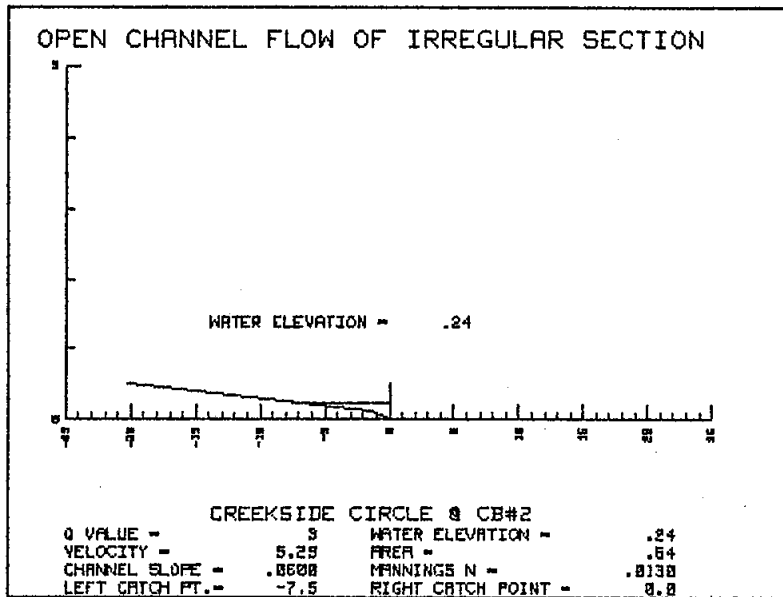


Q VALUE = 3.36980260144  
 WATER ELEVATION = .24472352  
 VELOCITY = 5.29452347983  
 AREA = .636469479129  
 WETTED PERIMETER = 7.74040862373  
 CHANNEL SLOPE IN Ft/Ft= .06  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -7.486176  
 CATCH POINT ON RIGHT SIDE = .0391557632

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*

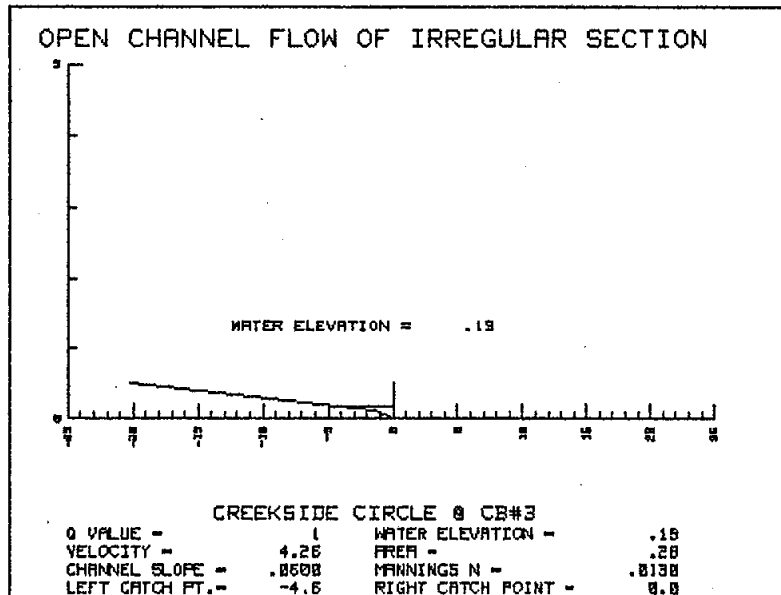


Q VALUE = 1.21100258749  
 WATER ELEVATION = .186632  
 VELOCITY = 4.26488794016  
 AREA = .283947105874  
 WETTED PERIMETER = 4.77642137406  
 CHANNEL SLOPE IN Ft/Ft = .06  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -4.5816  
 CATCH POINT ON RIGHT SIDE = .02986112

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*

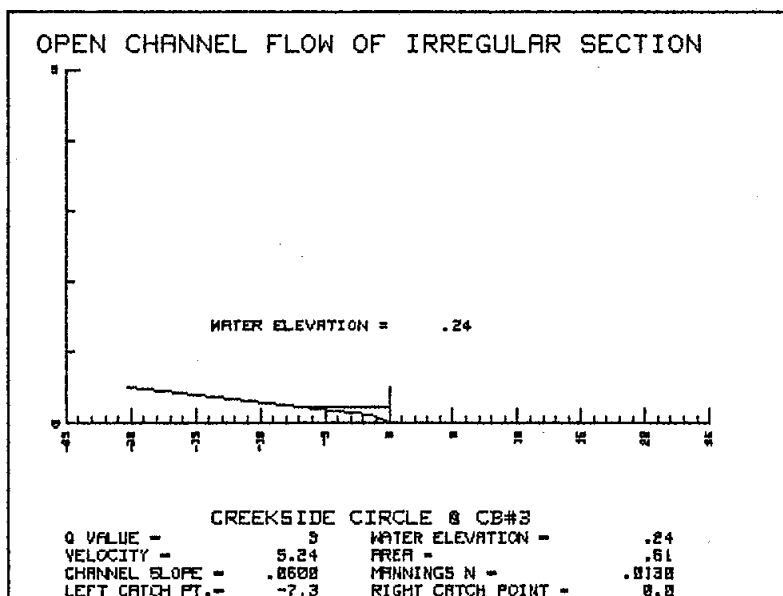


Q VALUE = 3.21999839653  
 WATER ELEVATION = .2417744  
 VELOCITY = 5.24007682758  
 AREA = .614494501224  
 WETTED PERIMETER = 7.58993650529  
 CHANNEL SLOPE IN Ft/Ft= .06  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -7.33872  
 CATCH POINT ON RIGHT SIDE = .038683904

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*



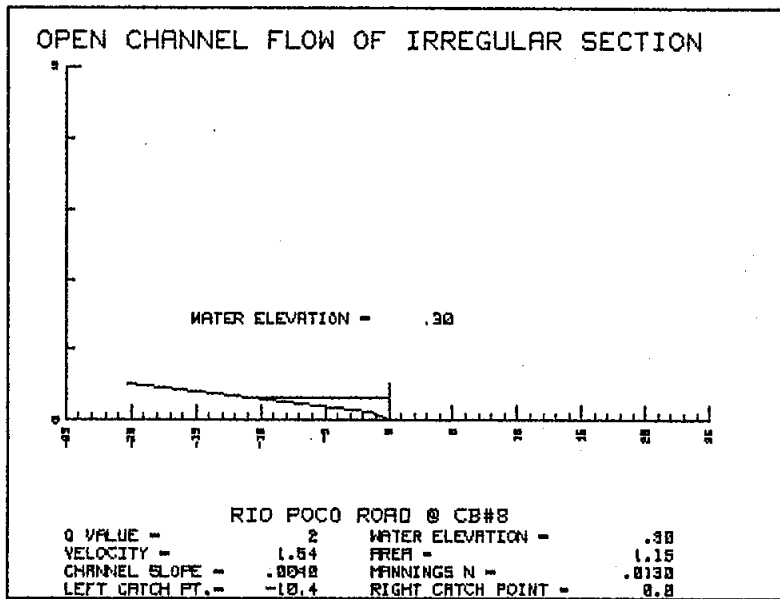


Q VALUE = 1.88400995802  
 WATER ELEVATION = .30204  
 VELOCITY = 1.63800275799  
 AREA = 1.15018729293  
 WETTED PERIMETER = 10.664851226  
 CHANNEL SLOPE IN Ft/Ft = .004  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -10.352  
 CATCH POINT ON RIGHT SIDE = .0483264

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*

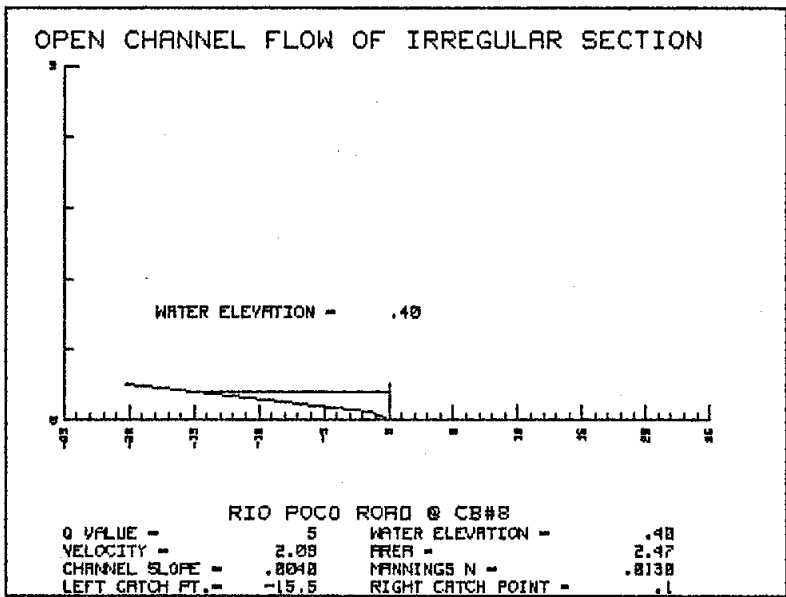


Q VALUE = 5.17529098916  
 WATER ELEVATION = .40407648  
 VELOCITY = 2.09312487293  
 AREA = 2.47251898636  
 WETTED PERIMETER = 15.8710297822  
 CHANNEL SLOPE IN Ft/Ft = .004  
 MANNINGS N = .013  
 CATCH POINT ON LEFT SIDE = -15.453824  
 CATCH POINT ON RIGHT SIDE = .0646522368

CHANNEL COORDINATES

ELEVATION	DISTANCE
.50	-20.25
.13	-1.50
0.00	0.00
.50	.08

\*\*\*\*\*



### CATCH BASIN CAPACITIES

From Neenah  $Q = K' D^{5/3}$  (non-sump condition)

$K'$  is dependent on grate size and type, slope of street and cross slope of street.  $K'$  is taken from charts provided by Neenah.

$D$  is depth of flow in gutter (determined using Manning's equation)

For sump condition low flow is determined from weir flow equation:

$$Q = \frac{2}{3} C b \sqrt{2g} (H)^{3/2}$$

Where:  $C = 0.5$   
 $b$  = effective width of opening  
 $g = 32.2 \text{ ft/sec}^2$   
 $H$  = water depth at catch basin

For sump condition high flow is determined from orifice flow equation:

$$Q = C A \sqrt{2g H}$$

Where:  $C = 0.6$   
 $A$  = Open area of grate and curb inlet  
 $g = 32.2 \text{ ft/sec}^2$   
 $H$  = Depth of water over catch basin

Catch Basin No. 1 Type 4-R

$$Q = K' D^{5/3}$$

$K' = 17$   
 $D_{5\text{-Year}} = .304 \text{ ft}$   
 $D_{100\text{-Year}} = .406 \text{ ft}$

$$Q_5 \text{ Capacity} = (17) (.304)^{5/3} = 2.34 \text{ cfs}$$

$$Q_{100} \text{ Capacity} = (17) (.406)^{5/3} = 3.79 \text{ cfs}$$

Catch Basin No. 2 Type 4-R

$$Q = K' D^{5/3}$$

$K' = 32$   
 $D_{5\text{-Year}} = .191 \text{ ft}$   
 $D_{100\text{-Year}} = .245 \text{ ft}$

$$Q_5 \text{ Capacity} = (32) (.191)^{5/3} = 2.03 \text{ cfs}$$

$$Q_{100} \text{ Capacity} = (32) (.242)^{5/3} = 3.11 \text{ cfs}$$

Catch Basin No. 3 Type 4-R

$$Q = K' D^{5/3}$$
$$K' = 32$$
$$D_{5\text{-Year}} = .19 \text{ ft}$$
$$D_{100\text{-Year}} = .242 \text{ ft}$$

$$Q_5 \text{ Capacity} = (32) (.19)^{5/3} = 2.01 \text{ cfs}$$
$$Q_{100} \text{ Capacity} = (32) (.242)^{5/3} = 3.08 \text{ cfs}$$

Catch Basin No. 6 Type I

$$Q_5 \text{ Capacity} = \frac{2}{3} C b \sqrt{2g} (H)^{3/2}$$

$$.44 = \frac{2}{3} (0.5) (1.71) \sqrt{(2) (32.2)} (H)^{3/2}$$

$$H = .21$$

$$Q_{100} \text{ Capacity} = C A \sqrt{2gh}$$
$$Q_{100} \text{ Capacity} = (0.6) (.875) \sqrt{(2) (3.2) (.42)}$$
$$Q_{100} \text{ Capacity} = 2.72 \text{ cfs}$$

Catch Basin No. 7 Type 3

$$Q_5 \text{ Capacity} = C A \sqrt{2gh}$$
$$Q_5 \text{ Capacity} = (0.6) (1.1) \sqrt{(2) (32.2) (0.41)}$$
$$Q_5 \text{ Capacity} = 3.39$$

$$Q_{100} \text{ Capacity} = C A \sqrt{2gh}$$
$$Q_{100} \text{ Capacity} = (0.6) (1.1) \sqrt{(2) (32.2) (0.65)}$$
$$Q_{100} \text{ Capacity} = 4.27$$

Catch Basin No. 8 Type 3

$$Q = K' D^{5/3}$$
$$K' = 16$$
$$D_{5\text{-Year}} = .31 \text{ ft}$$
$$D_{100\text{-Year}} = .4 \text{ ft}$$

$$Q_5 \text{ Capacity} = (16) (.3)^{5/3} = 2.12$$
$$Q_{100} \text{ Capacity} = (16) (.4)^{5/3} = 3.48$$

Catch Basin No. 9 Type I

$$Q_5 \text{ Capacity} = \frac{2}{3} C b \sqrt{2g} (H)^{3/2}$$

$$0.33 = \frac{(2)}{3} (0.5) (1.71) \sqrt{(2)(32.2)} H^{3/2}$$

$$H = .17 \text{ ft}$$

$$Q_{100} \text{ Capacity} = \frac{2}{3} C b \sqrt{2g} H^{3/2}$$

$$0.87 = \frac{2}{3} (0.5) (1.67) \sqrt{2(32.2)} H^{3/2}$$

$$H = .34 \text{ ft}$$

APPENDIX B

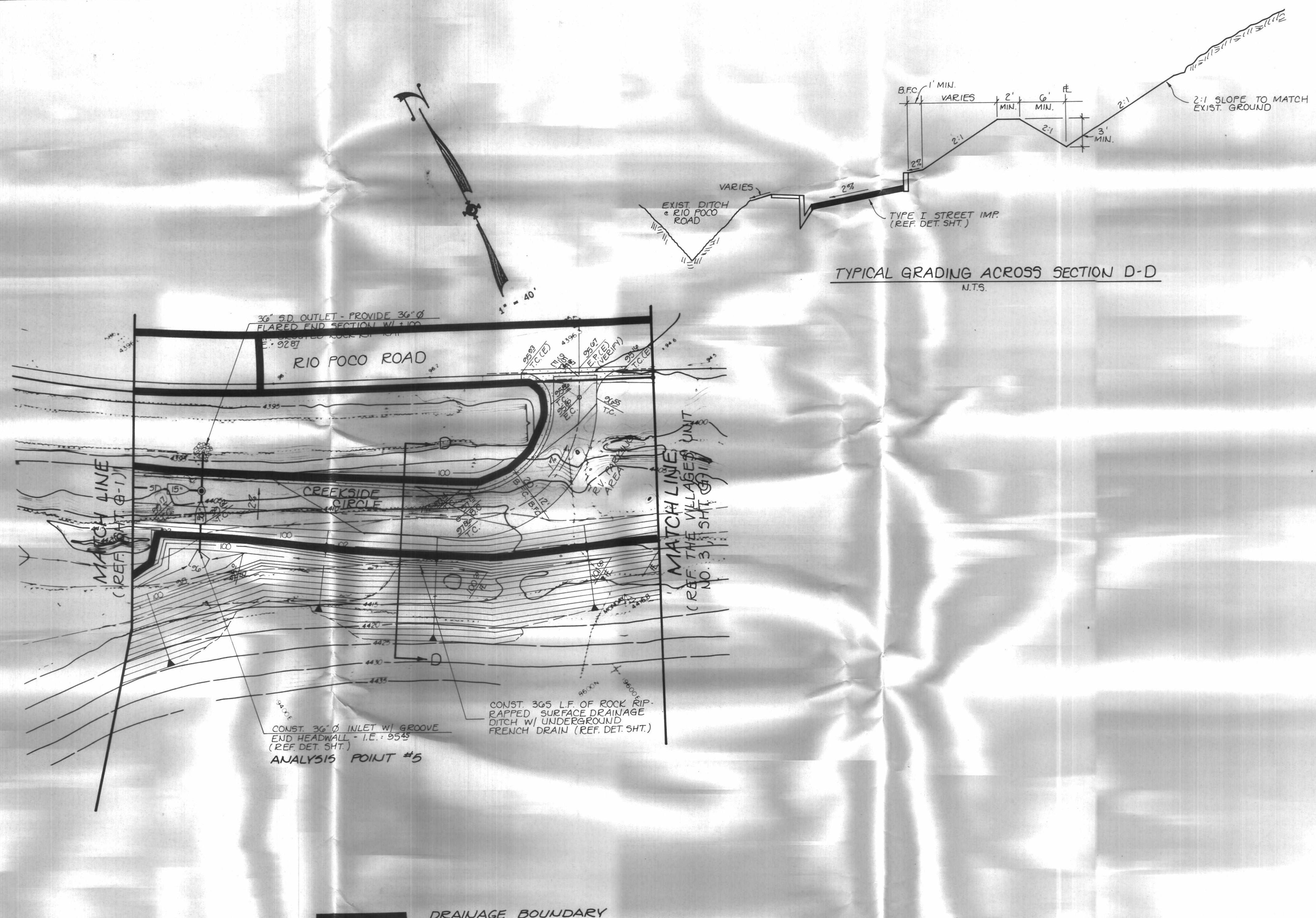


**NOTES:**

- 1) THE CONTRACTOR SHALL MAINTAIN A DUST CONTROL PROGRAM, INCLUDING WATERING OF OPEN AREAS. THE CONTRACTOR SHALL ALSO MAINTAIN CONFORMITY WITH SECTION 040.030 OF THE WASHOE COUNTY AIR POLLUTION REGULATIONS.
- 2) THE CONTRACTOR SHALL MAINTAIN AN ON-GOING PROCESS OF REMOVAL OF ALL SPILLAGE OF EXCAVATION MATERIAL ON ALL PAVED STREETS.
- 3) THE INSPECTION AND TESTING OF SOILS SHALL BE TO THE CITY OF RENO STANDARDS.
- 4) ALL AREAS DISTURBED AND LEFT UNDEVELOPED FOR A PERIOD OF MORE THAN 90 DAYS SHALL BE STABILIZED BY THE APPLICATION OF A DUST PALLIATIVE.
- 5) LAND GRADING SHALL BE DONE IN A METHOD TO PREVENT DUST FROM TRAVERSING THE PROPERTY LINE.
- 6) THE CONTRACTOR SHALL OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND FEES REQUIRED FOR CONSTRUCTION.
- 7) THE CONTRACTOR SHALL NOTIFY ALL AFFECTED PUBLIC ENTITIES 48 HOURS PRIOR TO BEGINNING CONSTRUCTION.
- 8) THE CONTRACTOR SHALL VERIFY IN FIELD, ALL ELEVATIONS, DIMENSIONS, FLOW LINES, EXISTING CONDITIONS, AND POINTS OF CONNECTIONS WITH ADJOINING PROPERTY (PUBLIC OR PRIVATE). ANY DISCREPANCIES SHALL BE CALLED TO THE ATTENTION OF THE ENGINEER BEFORE PROCEEDING WITH THE WORK.
- 9) THE CONTRACTOR SHALL NOTIFY THE PROJECT ENGINEER, THE SOILS ENGINEER, THE CITY OF RENO, AND SIERRA PACIFIC POWER COMPANY 48 HOURS PRIOR TO COMMENCEMENT OF WORK.
- 10) THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL DAMAGE TO EXISTING UTILITIES ENCOUNTERED DURING CONSTRUCTION. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT THE UTILITY COMPANIES FOR LOCATIONS OR POT HOLE PRIOR TO CONSTRUCTION.
- 11) PRIOR TO ACCEPTANCE OF FINAL IMPROVEMENTS BY THE CITY OF RENO, ALL SLOPES STEEPER THAN 3:1 WITHIN PRIVATE YARDS SHALL BE STABILIZED ACCORDING TO THE SLOPE STABILIZATION PROCEDURES NOTED ON THIS SHEET. AFTER PLANTING, THE INDIVIDUAL LOT OWNERS WILL BE RESPONSIBLE TO IRRIGATE AND MAINTAIN THEIR SLOPES.
- 12) ALL SLOPES STEEPER THAN 3:1 AND GREATER THAN 3 FEET VERTICAL SHALL BE MECHANICALLY STABILIZED WITH ROCK RIP-RAP.
- 13) ALL DISTURBED AREAS LEFT UNDEVELOPED SHALL BE HYDRO-SEEDING PRIOR TO ISSUANCE OF LAST C. OF O.
- 14) ADD 4300 FEET TO ALL SPOT ELEVATIONS.
- 15) BASIS OF ELEVATIONS - U.S.C. & G.S. SEA-LEVEL DATUM OF 1929, WITH SUPPLEMENTAL ADJUSTMENT OF 1956.

**LEGEND:**

- EXISTING CONTOUR LINE
- - - PROPOSED CONTOUR LINE
- ▭ A.C. PAVEMENT AREA
- ▭ CONCRETE AREA
- ▭ EXISTING A.C. OR CONCRETE AREA
- PROPOSED TOP OF CURB ELEV.
- PROPOSED FLOWLINE ELEV.
- PROPOSED ELEV. @ GRADE BREAK
- PROPOSED ELEV. @ FINISHED GRADE
- PROPOSED PAD ELEV.
- EXISTING GRADE ELEV.
- GRADE BREAK
- MANHOLE (DASHED IF EXISTING)
- CATCH BASIN (DASHED IF EXISTING)
- SS-8 SANITARY SEWER W/ SIZE AND DIRECTION INDICATOR (DASHED IF EXISTING)
- SD-30 STORM DRAIN W/ SIZE AND DIRECTION INDICATOR (DASHED IF EXISTING)
- FLOW LINE
- ▲ CUT OR FILL SLOPE



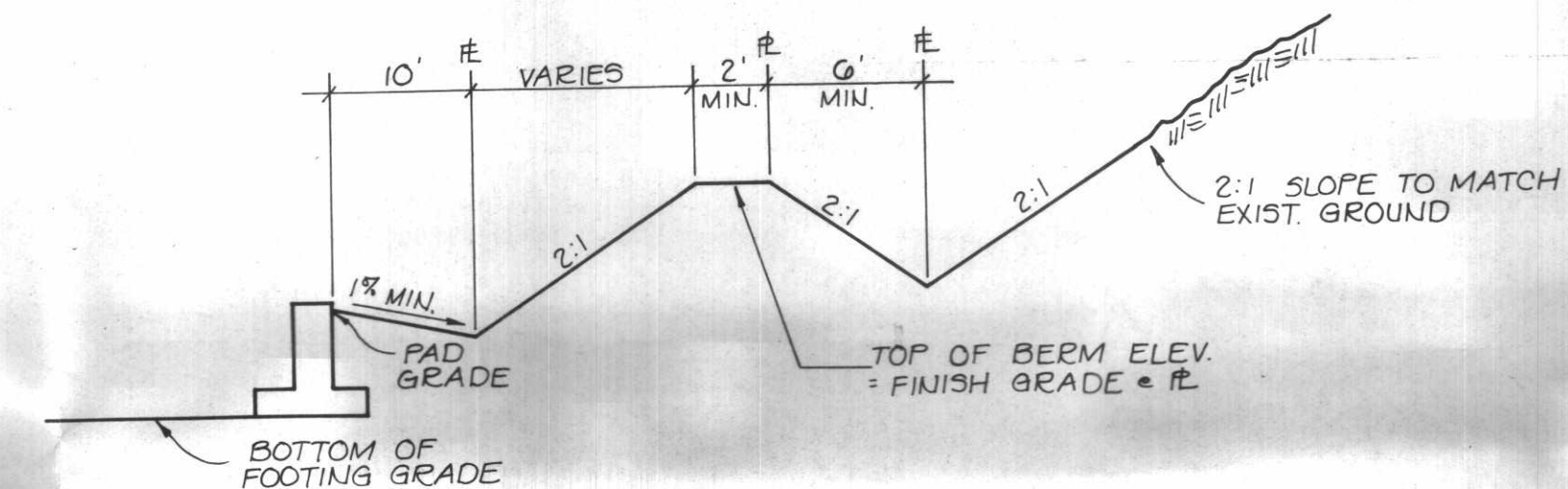
**TYPICAL GRADING ACROSS SECTION D-D**  
N.T.S.

SHEET 2 OF 3	SUMMIT CONSULTING ENGINEERS AND SURVEYORS 5405 MARKING AVENUE, SUITE 200 RENO, NEVADA 89501 PHONE: (775) 782-7477 FAX: (775) 784-8098	THE VILLAGES UNIT NO. 2 DRAINAGE PLAN	WASHINGTON COUNTY, NEVADA	RENC.
SCALE 1" = 40'	HORIZ VERT JOB NO. 3274 DRAWING NO.	DESIGNED BY JNM DRAWN BY CHECKED BY DATE: JULY 1988	DESCRIPTION DATE BY APP'D	DATE BY APP'D

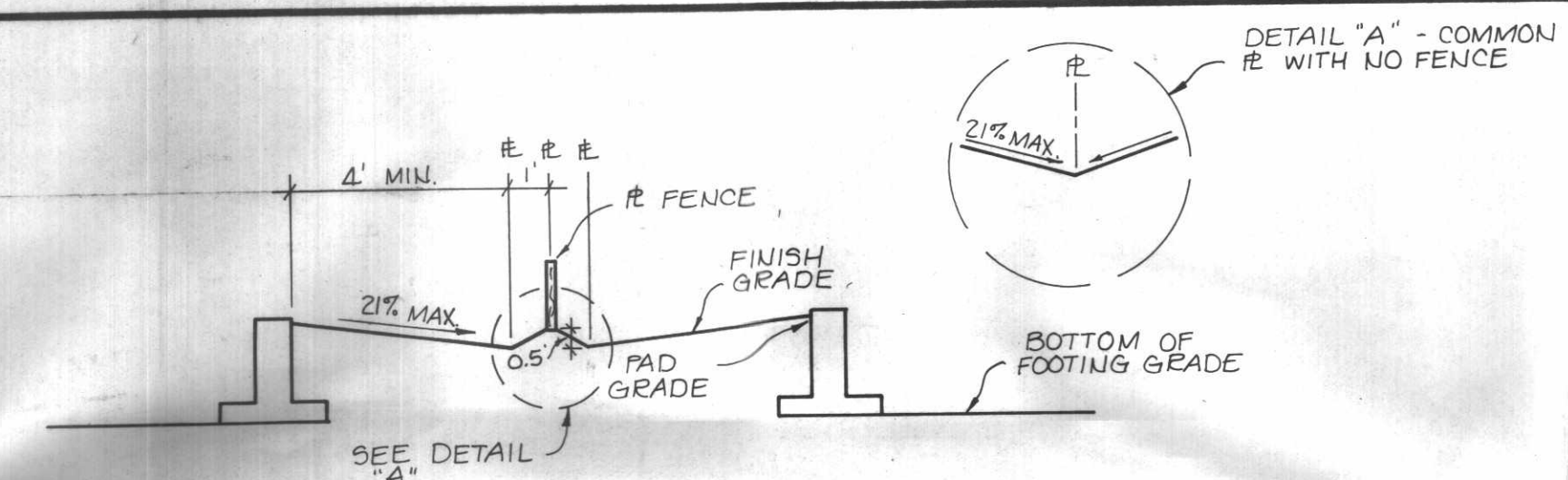


**NOTES:**

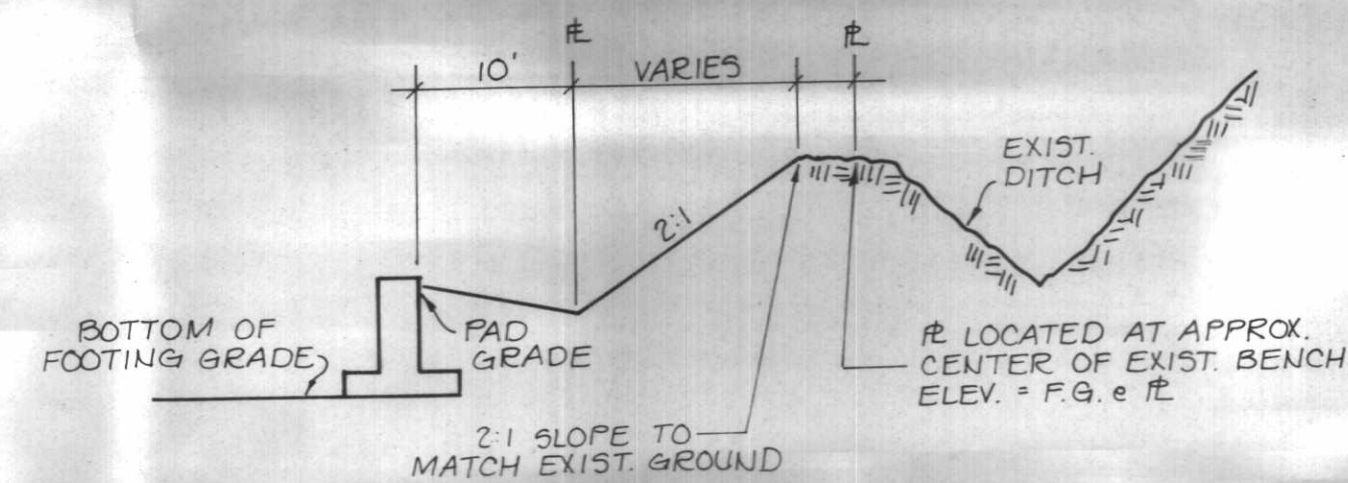
- 1) THE CONTRACTOR SHALL MAINTAIN A DUST CONTROL PROGRAM, INCLUDING WATERING OF OPEN AREAS. THE CONTRACTOR SHALL ALSO MAINTAIN CONFORMITY WITH SECTION 040.030 OF THE WASHOE COUNTY AIR POLLUTION REGULATIONS.
- 2) THE CONTRACTOR SHALL MAINTAIN AN ON-GOING PROCESS OF REMOVAL OF ALL SPILLAGE OF EXCAVATION MATERIAL ON ALL PAVED STREETS.
- 3) THE INSPECTION AND TESTING OF SOILS SHALL BE TO THE CITY OF RENO STANDARDS.
- 4) ALL AREAS DISTURBED AND LEFT UNDEVELOPED FOR A PERIOD OF MORE THAN 30 DAYS SHALL BE STABILIZED BY THE APPLICATION OF A DUST PALLIATIVE.
- 5) LAND GRADING SHALL BE DONE IN A METHOD TO PREVENT DUST FROM TRAVERSING THE PROPERTY LINE.
- 6) THE CONTRACTOR SHALL OBTAIN AND PAY FOR ALL NECESSARY PERMITS AND FEES REQUIRED FOR CONSTRUCTION.
- 7) THE CONTRACTOR SHALL NOTIFY ALL AFFECTED PUBLIC ENTITIES 48 HOURS PRIOR TO BEGINNING CONSTRUCTION.
- 8) THE CONTRACTOR SHALL VERIFY IN FIELD, ALL ELEVATIONS, DIMENSIONS, FLOW LINES, EXISTING CONDITIONS, AND POINTS OF CONNECTIONS WITH ADJOINING PROPERTY (PUBLIC OR PRIVATE). ANY DISCREPANCIES SHALL BE CALLED TO THE ATTENTION OF THE ENGINEER BEFORE PROCEEDING WITH THE WORK.
- 9) THE CONTRACTOR SHALL NOTIFY THE PROJECT ENGINEER, THE SOILS ENGINEER, THE CITY OF RENO, AND SIERRA PACIFIC POWER COMPANY 48 HOURS PRIOR TO COMMENCEMENT OF WORK.
- 10) THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL DAMAGE TO EXISTING UTILITIES ENCOUNTERED DURING CONSTRUCTION. IT SHALL BE THE CONTRACTORS RESPONSIBILITY TO CONTACT THE UTILITY COMPANIES FOR LOCATIONS OR POTHOLES PRIOR TO CONSTRUCTION.
- 11) PRIOR TO ACCEPTANCE OF FINAL IMPROVEMENTS BY THE CITY OF RENO, ALL SLOPES STEEPER THAN 3:1 WITHIN PRIVATE YARDS SHALL BE STABILIZED ACCORDING TO THE SLOPE STABILIZATION PROCEDURES NOTED ON THIS SHEET. AFTER PLANTING, THE INDIVIDUAL LOT OWNERS WILL BE RESPONSIBLE TO IRRIGATE AND MAINTAIN THEIR SLOPES.
- 12) ALL SLOPES STEEPER THAN 3:1 AND GREATER THAN 3 FEET VERTICAL SHALL BE MECHANICALLY STABILIZED WITH ROCK RIP-RAP.
- 13) ALL DISTURBED AREAS LEFT UNDEVELOPED SHALL BE HYDRO-SEEDED PRIOR TO ISSUANCE OF LAST C. OF D.
- 14) ADD 4300 FEET TO ALL SPOT ELEVATIONS.
- 15) BASIS OF ELEVATIONS - U.S.C. & G.S.S. SEA-LEVEL DATUM OF 1929, WITH SUPPLEMENTAL ADJUSTMENT OF 1956.



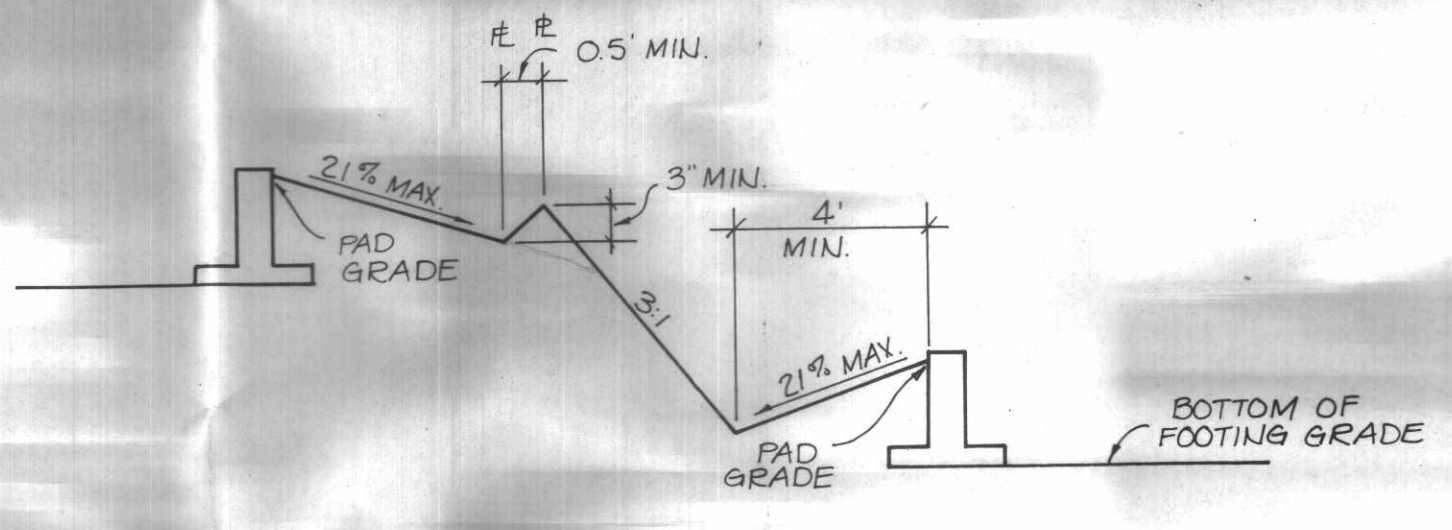
TYPICAL GRADING ACROSS SECTION A-A  
N.T.S.



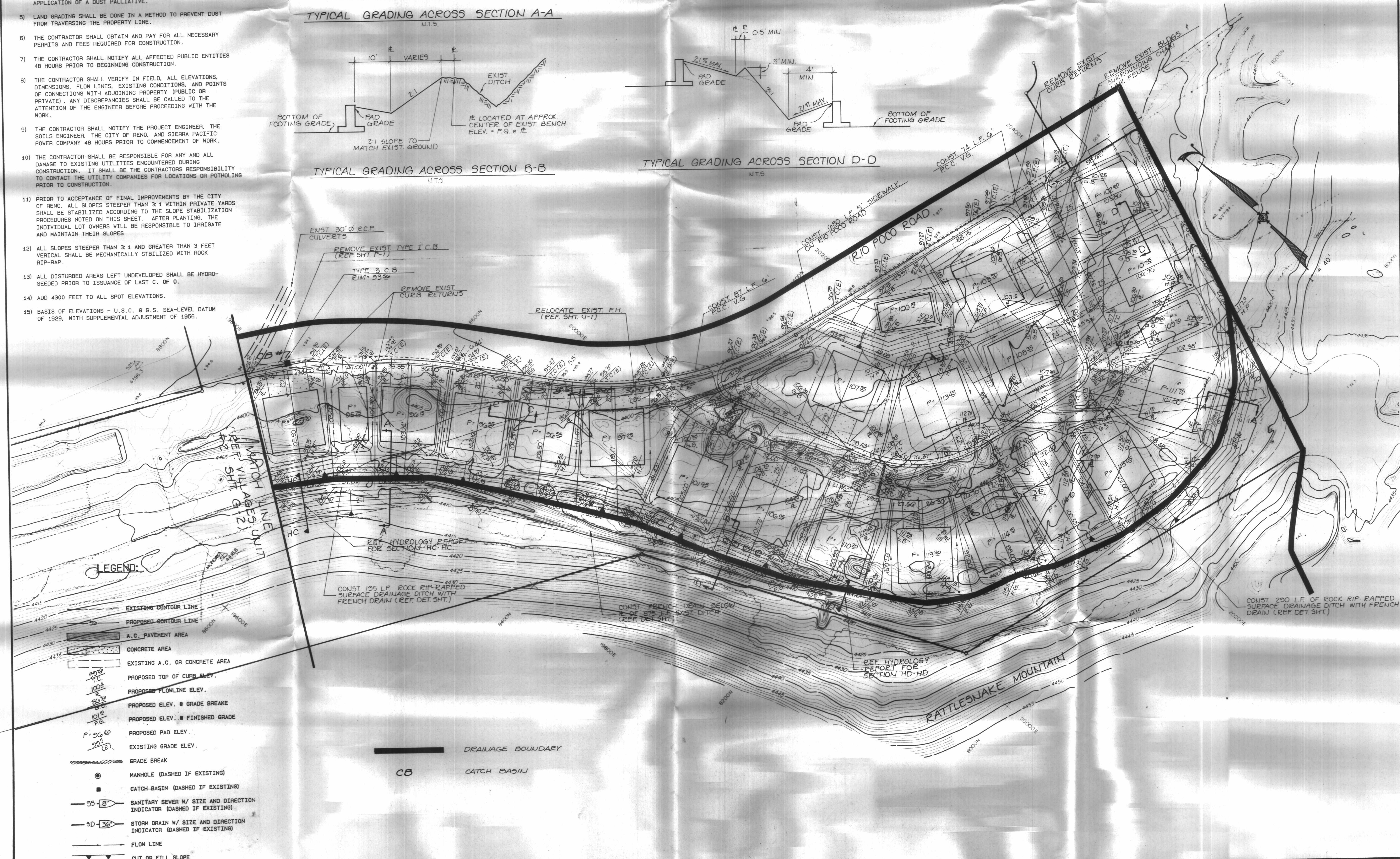
TYPICAL GRADING ACROSS SECTION C-C  
N.T.S.



TYPICAL GRADING ACROSS SECTION B-B  
N.T.S.



TYPICAL GRADING ACROSS SECTION D-D  
N.T.S.



SHEET	3	OF	3
	<b>SUMMIT</b> ENGINEERING CORPORATION CONSULTING ENGINEERS AND SURVEYORS 5405 MAXWELL AVENUE, RENO, NEVADA 89503 278 E. 17TH STREET, ELI, NEVADA 89801 PHONE: (702) 747-8500 FAX: (702) 746-8086		
SCALE	1" = 40'	JOB NO.	3274
HORIZ.		DRAWING NO.	
VERT.			
THE VILLAGES UNIT NO. 3		RENO, NEVADA	
DRAINAGE PLAN		WASHOE COUNTY, NEVADA	
DESIGNED BY	JNM	CHECKED BY	JJM
DRAWN BY	HP7580A	DATE	JULY 1988