

MASTER HYDROLOGY REPORT

Golden Hills at Damonte Foothills

Prepared for:

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C.D. ENG.

OCT 18 2005

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TABLE OF CONTENTS

Introduction.....	2
Appendix Information.....	3
Areas Within Flood Hazard Zone.....	3
Previous Studies.....	3
Background and Existing Drainage.....	4
Developed Site Hydrology.....	4
Storm Drainage System.....	4
Culverts and Channels.....	5
Conclusions.....	5
References.....	5

Drainage Report Appendices

Appendix A

Vicinity Map
Site Location Map
Assessors Parcel Map
NOAA ATLAS 14
Proposed Conditions Map

Appendix B

5-Year
Modified Form 2 (Tc Calculations)
Basin Schematic-StormCAD plan view
Hydraulic Grade Lines
Pipe Analysis Table
Detailed Inlet Table
Junction Analysis Table

Appendix C

100-Year
Modified Form 2 (Tc Calculations)
Basin Schematic-StormCAD plan view
Hydraulic Grade Lines
Pipe Analysis Table
Detailed Inlet Table
Junction Analysis Table

Appendix D

Channel Design Information

Appendix E

Culvert Design Calculations

Appendix F

Storm Drainage Master Plan (Wood Rodgers, Inc. March 05)

INTRODUCTION

This report has been updated to reflect the final design of Golden Hills Phases 2A and 2B. The major revision has been to the 5 and 100 year StormCAD models in Appendices B and C to reflect a reduction in the number of storm drain manholes.

The following report presents the storm water management plan for the Golden Hills at Damonte Foothills (tentative map LDC04-00381) single family residential development, (referred to as Golden Hills for the remainder of this report). Golden Hills is located within Section 14, Township 18 North, Range 20 East and lies adjacent to and east of the Damonte Ranch development currently under construction. Reference the vicinity map in Appendix A of this report.

Golden Hills consists of 317 single family residential lots on 133.28 acres. The project is bounded to the east by the Palisades (tentative map LDC05-00252), to the west by existing homes, the north by undeveloped land, and to the South by McCauley Ranch Estates (tentative map LDC04-00272) and Damonte Ranch High School. A Vicinity Map, project site map, and Assessor Parcel map have been included within Appendix A of this report for reference.

The existing site consists of shallow slopes with substantial range land vegetation. The soil type for the site was derived from the USCS soil survey Washoe County, Nevada, South Part. Please reference the Storm Drainage Master Plan prepared by Wood Rodgers in Appendix F for a breakdown of the soil conditions.

This report contains the design and sizing for the storm water management system for the build out of the entire development, and conformance to the Storm Drainage Master Plan. These calculations include the design of all inlets, pipes, manholes, ditches, culverts and rock rip associated with this development.

FLOOD HAZARD AREAS

The proposed Golden Hills site, per the FEMA Flood Insurance Rate Map (FIRM) 32031C3187E, dated September 30, 1994, is located within the flood zone X. This indicates areas located outside of the 500 year floodplain.

PREVIOUS STUDIES

A master hydrology report was prepared by Wood Rodgers, Inc. entitled "Storm Drainage Master Plan Golden Hills Subdivision / Damonte Foothills" and dated March 2005. This report included an analysis of the existing and proposed basins for the entire development and the existing drainage channels for the entire development. The development plan for this portion of the Damonte Foothills project is in conformance with the master hydrology report. Please reference Appendix F for a copy of the master drainage report.

BACKGROUND AND EXISTING DRAINAGE

The criteria used for this analysis was the *City of Reno Design Manual*. All storm runoff calculations, overland flows, and pipe system flows were designed in accordance with the design criteria as outlined in the above mentioned manual. The Intensity Duration Frequency (IDF) Curve used for the calculations was the Point Precipitation Frequency Estimates from NOAA Atlas 14 (reference Appendix A for a copy of the NOAA information). This IDF curves gives a more accurate rainfall event located at the site rather than using the IDF curve that was established for areas within the City of Reno. Similarly the five (5) and 100 year design events have been modeled in conformance with previous investigations.

Since the base for all design within this development is the *Storm Drainage Master Plan Golden Hills Subdivision / Damonte Foothills, March 2005* prepared by Wood Rodgers, Inc., it was first determined that the final design and drainage patterns of Golden Hills project were in conformance with this investigation. This hydrology and hydraulics report was referenced to determine the extent of offsite flows impacting the site as well as for the sizing of the culverts and channels associated with the Damonte Foothills project.

DEVELOPED SITE HYDROLOGY

For each individual developed basin, areas were determined, runoff coefficients were established and times of concentrations were calculated as outlined in *City of Reno Design Manual*. The runoff coefficients were selected per the City of Reno Design Manual, Chapter 2, Section 3. The time of concentration calculations were performed in accordance with City of Reno Design Manual and the Washoe County Drainage Design and Hydrologic Criteria Manual. The time of concentration and developed flow calculations are located within the modified form 2 located in the Appendix B and C of this report.

The master hydrology report prepared by Wood Rodgers, Inc. indicates that there will not be a need for any on or off site detention areas relevant to this site. In fact the master study indicates an overall reduction in the discharged flows associated with the development of the Golden Hills/Damonte Foothills project. Please reference Appendix F for a copy of the master drainage report.

STORM DRAINAGE SYSTEM

As stated above, the criteria used for the design of the proposed storm drainage system was Chapter 2 of the *City of Reno Design Manual*. The system designed is a standard urbanized system with Type 4R catch basins connected to piped storm sewer systems. These systems have several outfalls which discharge either to the proposed north or central channel. From the point of discharge the developed flows are conveyed to the downstream drainage facilities located to the west of the project.

The proposed storm sewer system has been designed to convey flows in accordance with the master drainage study, Referenced above, and City of Reno requirements. The storm sewer system designed for this project has been sized to convey the 100 year event in entirety. Reference Appendix B and C for the 5 and 100-year storm drainage system analysis.

CULVERTS AND CHANNELS

The Storm Drainage Master Plan by Wood Rodgers, Inc. was used to determine the developed flows carried by the channels and culverts. Please reference Appendix F for a copy of the master drainage report.

This report covers the design analysis of the culverts associated with the Golden Hills portion of the Damonte Foothills project. These culverts were preliminarily sized in the Storm Drainage Master Plan. The design analysis for the culverts can be found in Appendix E of this report.

This report also includes the design analysis for the channels associated with the Damonte Foothills development and preliminarily modeled in the Storm Drainage Master Plan. The design analysis for the channels can be found in Appendix D of this report.

CONCLUSIONS

The proposed storm sewer system has capacity for the developed flows from the Golden Hills site in both the minor (5-year) and major (100 year) storm events in accordance with the *City of Reno Design Manual*. Additionally, The final drainage design is in accordance with the referenced Wood Rodgers, Inc. Storm Drainage Master Plan..

All supporting exhibits and calculations are included within the Appendices of this report.

REFERENCES

City of Reno, 2000. City of Reno Design Manual, Chapter II Storm Drainage. March, 2004.

Washoe County, 1996. Washoe County Hydrologic Criteria and Drainage Design Manual. Prepared by WRC Nevada, December 1996.

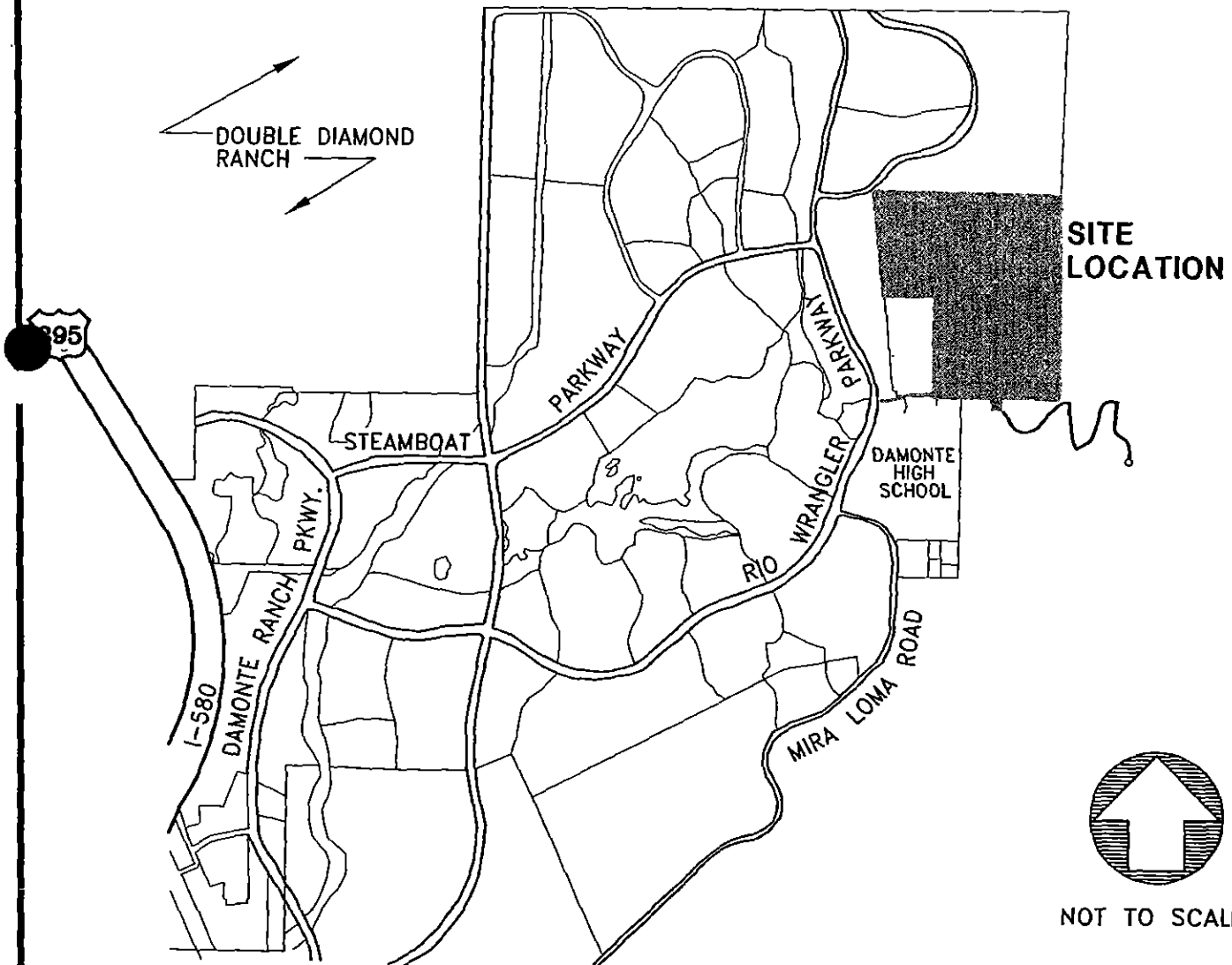
Wood Rodgers, Inc., 2005. Storm Drainage Master Plan – Golden Hills / Damonte Foothills, March, 2005.

VICINITY MAP
GOLDEN HILLS AT DAMONTE FOOTHILLS
REYNEN AND BARDIS

CITY OF RENO

NEVADA

JULY 2005



NOT TO SCALE

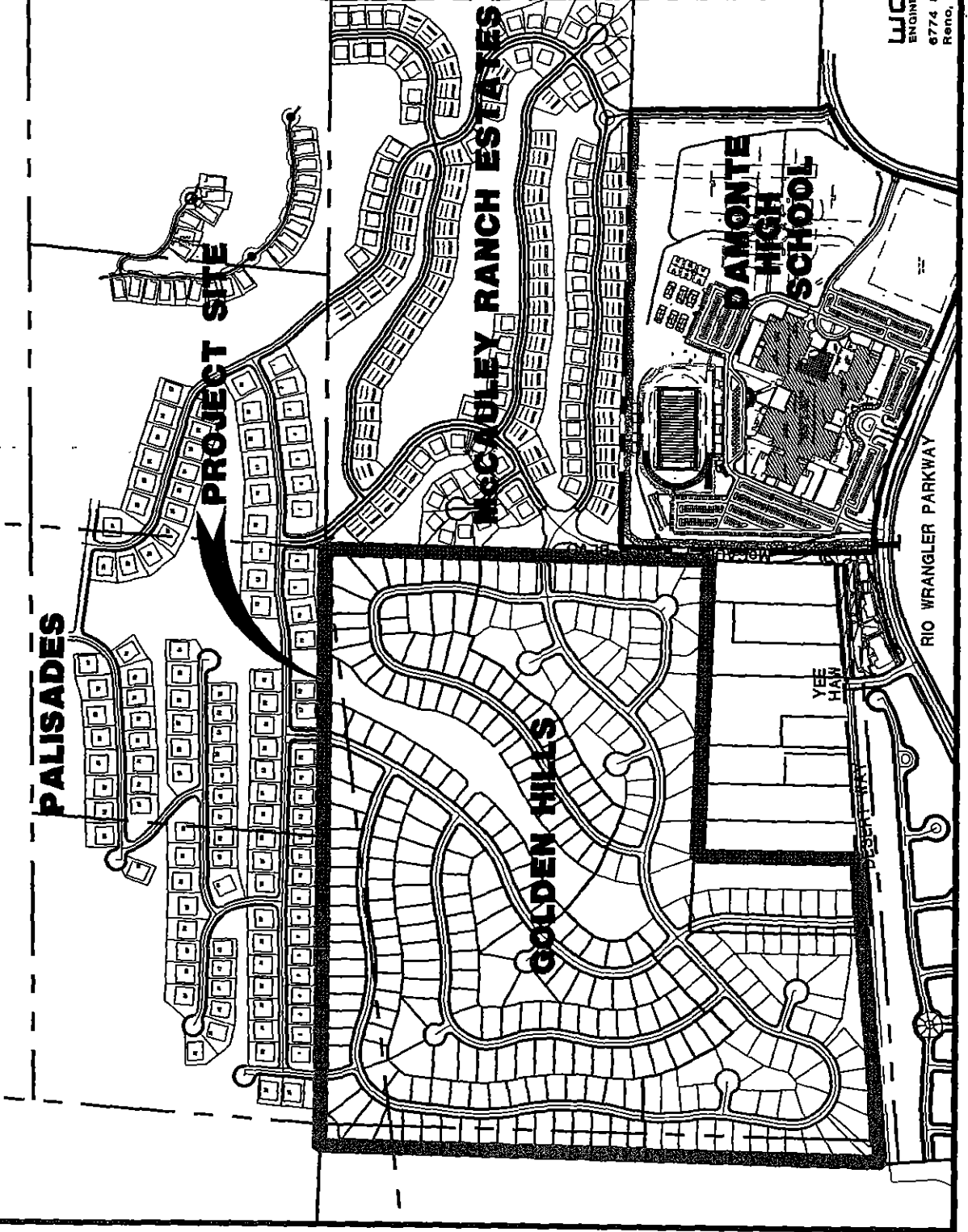
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J:\Jobs\1452_GOLDEN HILLS\GoldenHills_OA\Civil\Studies\Drain\VIC.DWG 7/16/05 10:23am dkitchen

GOLDEN HILLS AT DAMONTE FOOTHILLS

SITE PLAN

JULY 2005



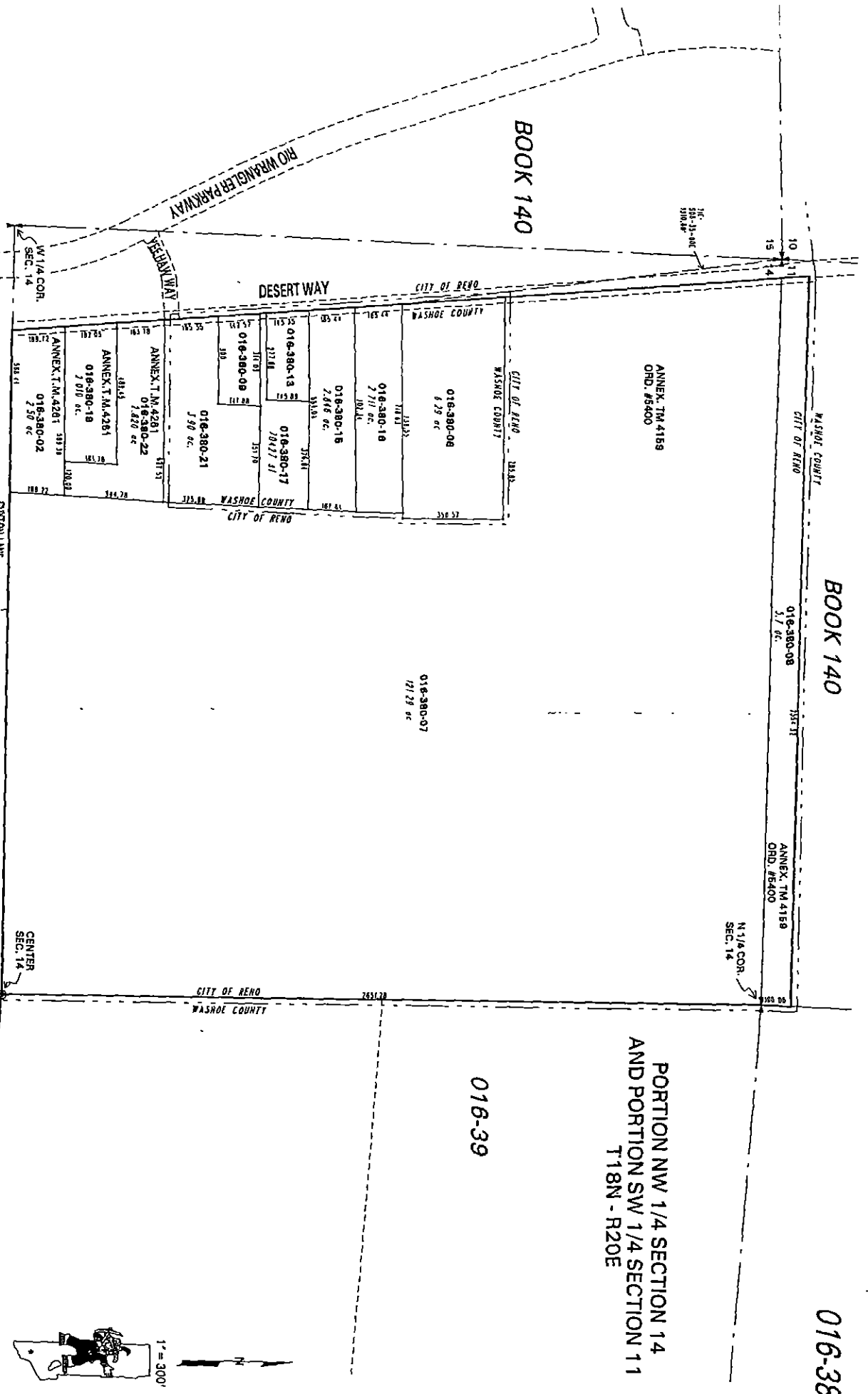
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NOTE: This map is prepared for the use of the Washoe County Assessor for assessment and illustrative purposes only. It does not represent a survey of the premises. No liability is assumed as to the sufficiency or the accuracy of the data delineated hereon.

BOOK 140
016-39
 Office of Washoe County Assessor, Nevada - Robert W. McGowan

This area previously shown on
 NOTE: Areas of parcels which are less than 2 acres are shown in squarfeet.

Drawn by HCS 01/27/03
 Revised: HCS 8/28/03, CFB 10/29/2003
 ASCE 92.11 SURVEY 1208-13



PORTION NW 1/4 SECTION 14
 AND PORTION SW 1/4 SECTION 11
 T18N - R20E

016-39

016-38



POINT PRECIPITATION FREQUENCY ESTIMATES FROM NOAA ATLAS 14



Nevada 39.4408 N 119.7298 W 4566 feet
 from "Precipitation-Frequency Atlas of the United States" NOAA Atlas 14, Volume 1, Version 3
 G.M. Bonnin, D. Todd, B. Lin, T. Parzybok, M. Yekta, and D. Ruley
 NOAA, National Weather Service, Silver Spring, Maryland, 2003

Extracted: Wed Jun 22 2005

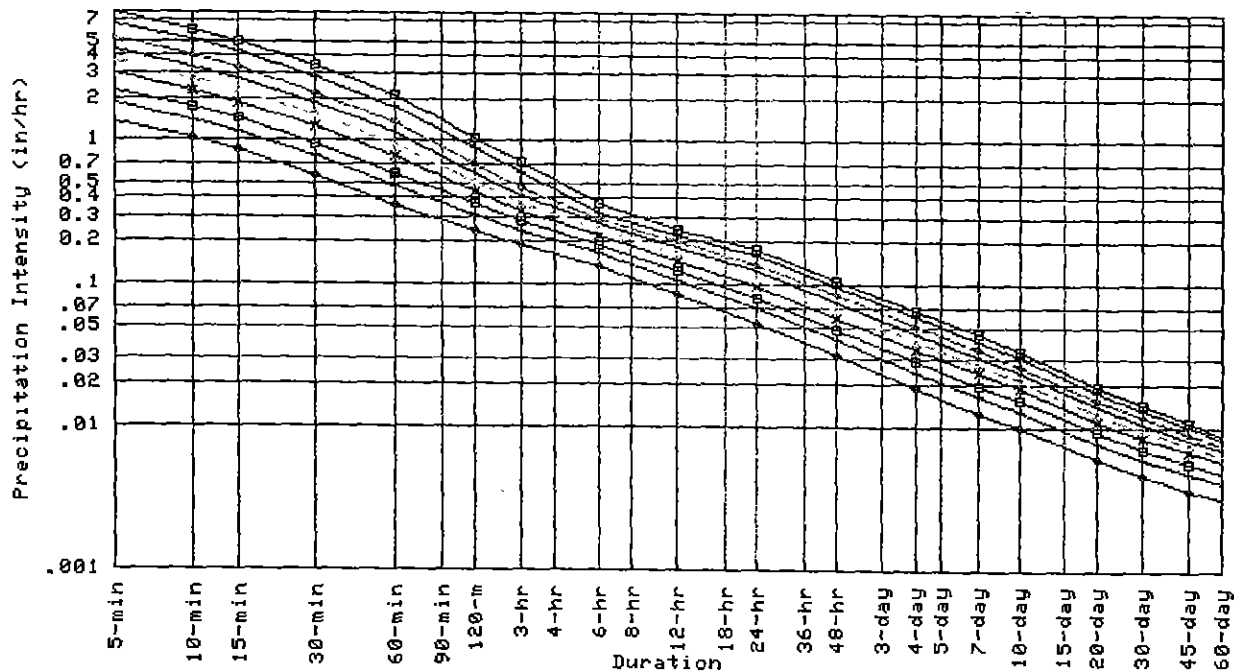
[Confidence Limits](#) | [Seasonality](#) | [Location Maps](#) | [Other Info](#) | [Grids](#) | [Maps](#) | [Help](#) | [Docs](#) | [U.S. Map](#)

Precipitation Intensity Estimates (in/hr)																		
ARI* (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
2	1.36	1.03	0.86	0.58	0.36	0.24	0.19	0.13	0.09	0.05	0.03	0.02	0.01	0.01	0.01	0.00	0.00	0.00
5	1.85	1.40	1.16	0.78	0.48	0.31	0.24	0.16	0.11	0.07	0.04	0.02	0.02	0.01	0.01	0.01	0.00	0.00
10	2.27	1.72	1.42	0.96	0.59	0.36	0.28	0.19	0.13	0.08	0.05	0.03	0.02	0.02	0.01	0.01	0.01	0.01
25	2.96	2.26	1.86	1.25	0.78	0.45	0.33	0.22	0.15	0.10	0.06	0.04	0.02	0.02	0.01	0.01	0.01	0.01
50	3.59	2.73	2.26	1.52	0.94	0.52	0.37	0.24	0.17	0.11	0.07	0.04	0.03	0.02	0.01	0.01	0.01	0.01
100	4.33	3.29	2.72	1.83	1.13	0.60	0.42	0.27	0.18	0.12	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01
200	5.20	3.95	3.27	2.20	1.36	0.69	0.48	0.29	0.20	0.14	0.09	0.05	0.04	0.03	0.02	0.01	0.01	0.01
500	6.61	5.03	4.16	2.80	1.73	0.88	0.60	0.32	0.22	0.16	0.10	0.06	0.04	0.03	0.02	0.01	0.01	0.01
1000	7.92	6.02	4.98	3.35	2.07	1.05	0.71	0.36	0.24	0.18	0.11	0.07	0.05	0.03	0.02	0.01	0.01	0.01

Text version of table

* These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval. Please refer to the documentation for more information. NOTE: Formatting forces estimates near zero to appear as zero.

Partial duration based Point IDF Curves
 39.4408 N 119.7298 W 4566 ft



Wed Jun 22 18:10:59 2005

Average Recurrence Interval (years)	
2-year	+
5-year	+
10-year	#
25-year	*
50-year	+
100-year	—
200-year	+
500-year	+
1000-year	—

Confidence Limits -

*** Upper bound of the 90% confidence interval**

Precipitation Intensity Estimates (in/hr)

ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
2	1.61	1.22	1.01	0.68	0.42	0.28	0.21	0.15	0.09	0.06	0.04	0.02	0.01	0.01	0.01	0.01	0.00	0.00
5	2.17	1.65	1.36	0.92	0.57	0.36	0.27	0.18	0.12	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.00
10	2.68	2.03	1.68	1.13	0.70	0.42	0.31	0.21	0.14	0.09	0.05	0.03	0.02	0.02	0.01	0.01	0.01	0.01
25	3.54	2.69	2.23	1.50	0.93	0.53	0.37	0.25	0.17	0.11	0.07	0.04	0.03	0.02	0.01	0.01	0.01	0.01
50	4.36	3.31	2.74	1.84	1.14	0.62	0.43	0.28	0.19	0.12	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01
100	5.32	4.04	3.34	2.25	1.39	0.74	0.51	0.31	0.21	0.14	0.09	0.05	0.04	0.03	0.02	0.01	0.01	0.01
200	6.55	4.99	4.12	2.77	1.72	0.87	0.60	0.34	0.24	0.16	0.10	0.06	0.04	0.03	0.02	0.01	0.01	0.01
500	8.70	6.62	5.48	3.69	2.28	1.16	0.78	0.42	0.27	0.19	0.11	0.07	0.05	0.04	0.02	0.02	0.01	0.01
1000	10.73	8.16	6.74	4.54	2.81	1.42	0.96	0.51	0.30	0.21	0.13	0.08	0.05	0.04	0.02	0.02	0.01	0.01

* The upper bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are greater than

** These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval.

Please refer to the [documentation](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

*** Lower bound of the 90% confidence interval**

Precipitation Intensity Estimates (in/hr)

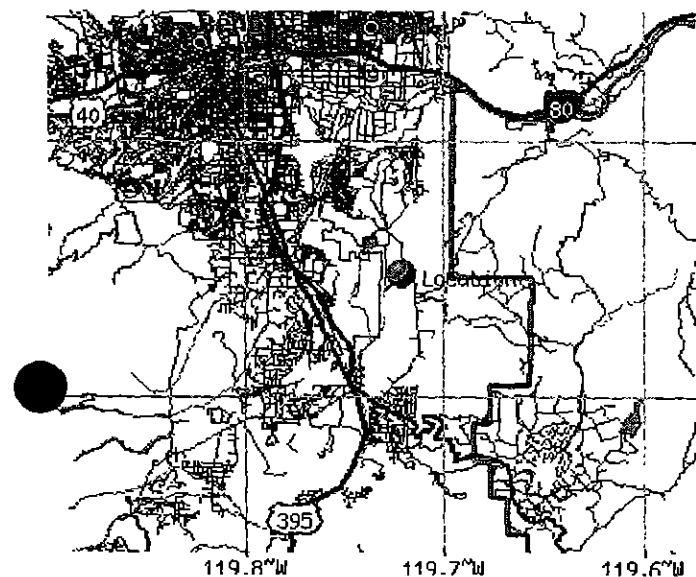
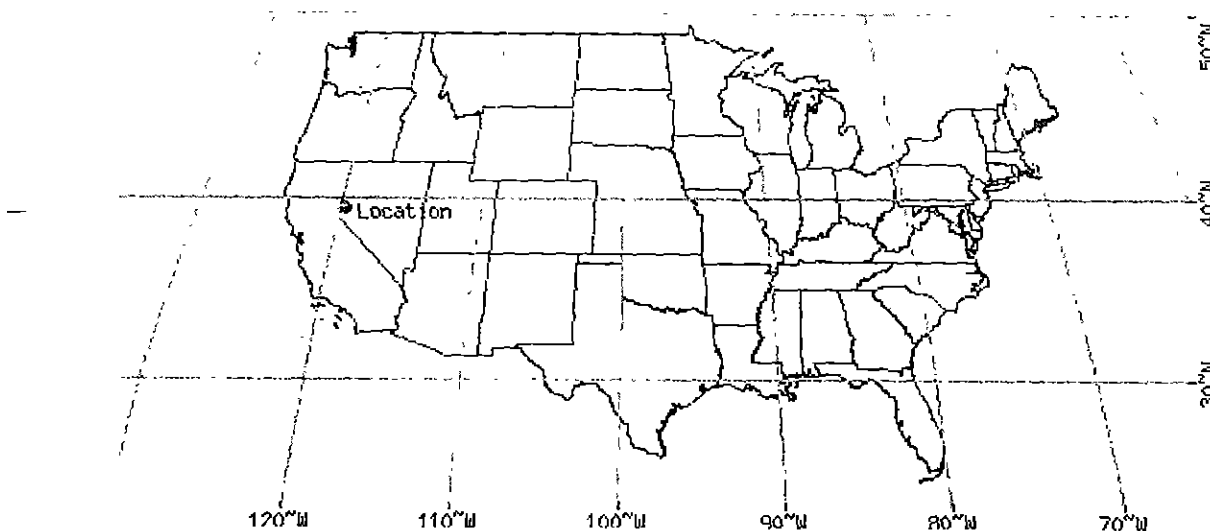
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
2	1.18	0.89	0.74	0.50	0.31	0.21	0.17	0.12	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.00	0.00	0.00
5	1.57	1.20	0.99	0.67	0.41	0.27	0.22	0.15	0.10	0.06	0.04	0.02	0.01	0.01	0.01	0.01	0.00	0.00
10	1.92	1.46	1.20	0.81	0.50	0.32	0.24	0.17	0.11	0.07	0.04	0.03	0.02	0.01	0.01	0.01	0.01	0.00
25	2.44	1.85	1.53	1.03	0.64	0.37	0.28	0.19	0.13	0.09	0.05	0.03	0.02	0.02	0.01	0.01	0.01	0.01
50	2.81	2.14	1.77	1.19	0.74	0.42	0.31	0.21	0.14	0.10	0.06	0.04	0.02	0.02	0.01	0.01	0.01	0.01
100	3.28	2.49	2.06	1.39	0.86	0.47	0.35	0.22	0.16	0.11	0.07	0.04	0.03	0.02	0.01	0.01	0.01	0.01
200	3.76	2.86	2.36	1.59	0.98	0.53	0.39	0.24	0.17	0.12	0.07	0.05	0.03	0.02	0.01	0.01	0.01	0.01
500	4.43	3.37	2.78	1.87	1.16	0.63	0.48	0.25	0.18	0.13	0.08	0.05	0.03	0.03	0.02	0.01	0.01	0.01
1000	5.03	3.83	3.16	2.13	1.32	0.73	0.55	0.29	0.19	0.14	0.09	0.06	0.04	0.03	0.02	0.01	0.01	0.01

* The lower bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are less than.

** These precipitation frequency estimates are based on a partial duration maxima series. ARI is the Average Recurrence Interval.

Please refer to the [documentation](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

Maps -



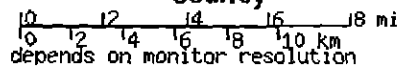
These maps were produced using a direct map request from the U.S. Census Bureau Mapping and Cartographic Resources Tiger Map Server

Please read [disclaimer](#) for more information.

LEGEND

- State
- County
- Indian Resv
- Lake/Pond/Ocean
- Street
- Expressway
- Highway
- Connector
- Stream
- Military Area
- National Park
- Other Park
- City
- County

Scale 1:228583
 *average—true scale depends on monitor resolution



Other Maps/Photographs -

View [USGS digital orthophoto quadrangle \(DOQ\)](#) covering this location from TerraServer; [USGS Aerial Photograph](#) may also be available from this site. A DOQ is a computer-generated image of an aerial photograph in which image displacement caused by terrain relief and camera tilts has been removed. It combines the image characteristics of a photograph with the geometric qualities of a map. Visit the [USGS](#) for more information.

Watershed/Stream Flow Information -

Find the [Watershed](#) for this location using the U.S. Environmental Protection Agency's site.

Climate Data Sources -

Precipitation frequency results are based on data from a variety of sources, but largely [NCDC](#). The following links provide general information

about observing sites in the area, regardless of if their data was used in this study. For detailed information about the stations used in this study, please refer to our documentation.

Using the [National Climatic Data Center's \(NCDC\)](#) station search engine, locate other climate stations within:

+/-30 minutes | ...OR... | +/-1 degree | of this location (39.4408/-119.7298). Digital ASCII data can be obtained directly from [NCDC](#).

and [Natural Resources Conservation Service \(NRCS\) SNOTEL \(SNOWpack TELEmetry\) stations](#) by visiting the [Western Regional Climate Center's state-specific SNOTEL station maps](#).

Hydrometeorological Design Studies Center
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Silver Spring, MD 20910
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Questions? HDSC.Questions@noaa.gov

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Project: GOLDEN HIGHLANDS
MODIFIED FORM 2

5-YEAR STORM EVENT

Sub-Basin	Initial Overland						Channelized Flow						Tc	Tc Urbanized Basin	Final Tc	Region 2		Final Intensity (in/hr)	O=CIA (cfs)	Check Flow		Check Flow	Check Flow	BYPASS TARGET
	Basin	R10	Area (ac)	L1 (ft)	Slope (%)	T1 (min)	L1 (ft)	Slope (%)	Vel (fps)	T1 (min)	(T1+T1) (min)	Check Total Length				Tc (check)	Min			INTENSITIES (min)	10			
B1	0.53	3.17	200.00	3.50	9.60	625.00	0.64	1.60	6.51	16.11	825.00	14.58	14.58	14.00	1.16	1.18	1.98	1.31	1.31	0.69	CB 1-12			
B2	0.53	2.91	142.00	1.65	10.36	717.00	5.00	4.47	2.67	13.04	859.00	14.77	13.04	14.00	1.16	1.25	1.93	2.43	2.43	0	CB 1-12			
B3	0.53	4.40	151.00	4.90	7.46	800.00	5.00	4.47	2.98	10.44	951.00	15.28	10.44	14.00	1.16	1.38	3.22	3.64	3.64	0	CB 1-12			
B4	0.53	3.66	166.00	6.10	7.28	736.00	4.70	4.34	2.83	10.11	902.00	15.01	10.11	14.00	1.16	1.39	2.71	2.73	2.73	0	CB 1-12			
B5	0.53	6.01	165.00	1.94	10.59	799.00	4.09	4.04	3.29	13.88	964.00	15.36	13.88	14.00	1.16	1.21	3.87	3.9	3.9	0	CB 1-12			
B6	0.53	4.45	124.00	2.10	8.94	577.00	5.10	4.52	2.13	11.07	701.00	13.69	11.07	14.00	1.16	1.35	3.18	3.21	3.21	0	CB 1-12			
B7	0.53	1.81	216.00	5.50	8.59	179.00	4.03	4.01	0.74	9.33	395.00	12.19	10.00	14.00	1.16	1.40	1.82	1.69	1.69	0	CB 1-12			
B8	0.53	2.64	134.00	1.98	9.48	825.00	6.78	5.21	2.64	12.12	959.00	15.33	12.12	14.00	1.16	1.30	3.55	1.52	1.52	0.31	CB 1-19			
B9	0.53	4.88	200.00	6.90	7.67	883.00	6.39	5.06	2.91	10.58	1083.00	16.02	10.58	14.00	1.16	1.37	3.55	2.29	2.29	1.29	CB 1-19			
B10	0.53	0.35	2.00	2.00	1.15	369.00	0.60	1.55	3.97	5.12	371.00	12.06	10.00	14.00	1.16	1.40	0.26	1.57	1.57	0	CB 1-22			
B11	0.53	3.23	137.00	1.75	9.98	812.00	5.82	4.82	2.80	12.79	949.00	15.27	12.79	14.00	1.16	1.27	2.17	1.82	1.82	0.36	CB 1-15			
B12	0.53	3.48	198.00	7.11	7.56	830.00	5.55	4.75	2.91	10.47	1028.00	15.71	10.47	14.00	1.16	1.38	2.54	2.03	2.03	0.53	CB 1-14			
B13	0.53	0.06	4.00	2.00	1.63	106.00	2.00	2.83	0.62	2.26	110.00	10.61	10.00	14.00	1.16	1.40	0.04	0.86	0.86	0	CB 1-14			
B14	0.53	0.35	20.00	20.00	1.71	269.00	0.54	1.47	3.05	4.76	289.00	11.61	10.00	14.00	1.16	1.40	0.26	0.74	0.74	0	CB 1-11			
B15	0.53	2.59	66.00	1.30	7.64	1300.00	3.89	3.94	5.49	13.14	1366.00	17.59	13.14	14.00	1.16	1.25	1.72	1.31	1.31	0.43	CB 1-11			
B16	0.53	3.14	156.00	9.20	6.16	372.00	5.07	4.50	1.38	7.54	528.00	12.93	10.00	14.00	1.16	1.40	2.33	2.35	2.35	0	CB 1-10			
B17	0.53	1.45	77.00	1.16	8.57	642.00	7.41	5.44	1.97	10.54	719.00	13.99	10.54	14.00	1.16	1.37	1.06	1.05	1.05	0.01	CB 1-10			
B18	0.53	0.17	4.00	2.00	1.63	280.00	7.96	5.64	0.83	2.46	284.00	11.58	10.00	14.00	1.16	1.40	0.13	0.13	0.13	0	CB 1-10			
B19	0.53	3.42	77.00	1.17	8.55	852.00	1.24	2.23	6.38	14.92	929.00	15.16	14.92	14.00	1.16	1.16	2.11	2.48	2.48	0	CB 1-10			
B20	0.53	4.59	124.00	1.13	10.97	936.00	1.26	2.24	6.95	17.92	1060.00	15.89	15.89	14.00	1.16	1.12	2.72	2.79	2.79	0	CB 1-10			
B21	0.53	2.99	116.00	1.06	10.84	543.00	1.63	2.55	3.54	14.38	659.00	13.66	13.66	14.00	1.16	1.22	1.94	1.96	1.96	0	CB 1-10			
B22	0.53	2.90	148.00	1.41	11.14	723.00	2.12	2.91	4.14	15.28	871.00	14.84	14.84	14.00	1.16	1.17	1.79	2.43	2.43	0	CB 1-10			
B23	0.53	2.87	151.00	1.78	10.42	657.00	2.16	2.94	3.73	14.15	808.00	14.49	14.15	14.00	1.16	1.20	1.83	2.99	2.99	0	CB 1-10			
B24	0.53	2.01	152.00	2.79	9.02	560.00	2.53	3.18	2.93	11.95	712.00	13.96	11.95	14.00	1.16	1.31	1.39	1.44	1.44	0.43	CB 1-08			
B25	0.53	3.42	222.00	7.36	8.00	738.00	2.96	3.07	4.00	12.00	965.00	15.36	12.00	14.00	1.16	1.30	2.36	1.68	1.68	0.7	CB 1-07			
B26	0.53	5.74	225.00	10.75	7.03	917.00	2.67	3.27	4.68	11.71	1142.00	16.34	11.71	14.00	1.16	1.32	4.01	4.04	4.04	0	CB 1-07			
B27	0.53	2.96	119.00	1.05	11.01	830.00	2.75	3.32	4.17	15.18	949.00	15.27	15.18	14.00	1.16	1.15	1.81	1.41	1.41	0.41	CB 1-08			
B28	0.53	1.49	62.00	1.10	7.83	728.00	2.25	3.00	4.04	11.87	790.00	14.39	11.87	14.00	1.16	1.31	1.03	1.32	1.32	0.4	CB 1-04			
B29	0.53	1.40	153.00	1.42	11.30	199.00	1.00	2.00	1.66	12.96	352.00	11.96	11.96	14.00	1.16	1.31	0.97	1.72	1.72	0	CB 1-02			
B30	0.53	3.72	247.00	2.02	12.79	958.00	2.97	3.45	4.63	17.42	1205.00	16.69	16.69	14.00	1.16	1.08	2.13	1.64	1.64	0.58	CB 1-02			
B31	0.53	2.80	145.00	1.94	9.93	839.00	3.08	3.51	3.98	13.91	984.00	15.47	13.91	14.00	1.16	1.21	1.80	1.48	1.48	0.41	CB 1-01			
B32	0.53	0.07	107.00	1.11	10.25	300.00	1.32	2.30	2.18	12.43	407.00	12.26	12.26	14.00	1.16	1.29	0.05	0.75	0.75	0.08	CB 2-02			
B33	0.53	1.47	192.00	3.10	9.79	307.00	1.32	2.30	2.23	12.01	499.00	12.77	12.01	14.00	1.16	1.30	1.02	2.02	2.02	0	CB 2-02			
B34	0.53	3.60	255.00	4.60	9.90	891.00	1.98	2.81	5.28	15.18	1146.00	16.37	15.18	14.00	1.16	1.15	2.20	1.5	1.5	0.72	CB 1-08			
B35	0.53	5.12	110.00	1.00	10.76	2435.00	2.42	10.17	3.99	14.75	2545.00	24.14	14.75	14.00	1.16	1.17	3.18	0	0	0	to channel			
B36	0.53	1.71	76.00	1.17	8.49	780.00	1.21	2.20	5.91	14.40	856.00	14.76	14.40	14.00	1.16	1.19	1.08	1.09	1.09	0	to channel			
B37	0.53	2.24	147.00	1.00	12.44	581.00	1.20	2.19	4.42	16.86	728.00	14.04	14.04	14.00	1.16	1.21	1.43	1.44	1.44	0	CB 1-01			
B38	0.53	2.29	107.00	1.07	10.38	620.00	2.30	3.03	3.41	13.79	727.00	14.04	13.79	14.00	1.16	1.22	1.48	1.21	1.21	0.28	CB 1-01			
B39	0.53	5.16	310.00	8.24	9.01	985.00	2.64	3.25	5.05	14.06	1295.00	17.19	14.06	14.00	1.16	1.21	3.30	2.4	2.4	0.92	CB 2-04			
B40	0.53	3.51	118.00	1.40	9.97	1030.00	2.64	3.25	5.28	15.26	1148.00	16.38	15.26	14.00	1.16	1.15	2.14	1.47	1.47	0.7	CB 2-03			
B41	0.53	1.67	726.00	2.04	21.85	147.00	0.50	1.41	1.73	23.58	873.00	14.65	14.85	14.00	1.16	1.17	1.03	2.35	2.35	0	CB 2-03			
B42	0.53	5.94	687.00	2.04	21.25	350.00	0.50	1.41	4.12	25.38	1037.00	15.76	15.76	14.00	1.16	1.12	3.54	3.36	3.36	1.29	CB 1-25			
B43	0.53	6.56	647.00	2.04	20.63	350.00	0.50	1.41	4.12	24.75	997.00	15.54	15.54	14.00	1.16	1.13	3.94	2.98	2.98	1.04	CB 1-26			
B44	0.53	10.55	145.00	1.00	12.35	1950.00	5.64	4.75	6.84	19.20	2095.00	21.64	19.20	14.00	1.16	0.96	5.36	0	0	0	to channel			
B45	0.53	4.33	131.00	1.00	11.74	1050.00	1.14	2.14	8.20	19.94	1181.00	16.56	16.56	14.00	1.16	1.09	2.49	0	0	0	to channel			

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Inlet Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Mannings n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
P-163	SDMH 2-2	SDMH 2-20	N/A	2.26	156.00	0.016859	15 inch	0.014	7.79	4,473.60	4,470.97	4,479.70	4,477.07	4,474.20	4,471.68
P-162	SDMH 2-23	SDMH 2-24	N/A	0.13	351.00	0.078205	12 inch	0.014	9.25	4,548.59	4,521.14	4,554.59	4,527.24	4,548.74	4,521.48
P-161	SDMH 2-15	SDMH 2-18	N/A	4.95	119.00	0.021765	18 inch	0.014	14.39	4,492.49	4,489.90	4,498.59	4,496.00	4,493.35	4,490.93
P-160	SDMH 2-17	SDMH 2-16	N/A	4.89	215.00	0.023674	18 inch	0.014	15.01	4,487.44	4,482.35	4,493.54	4,488.45	4,488.29	4,483.37
P-159	SDMH 2-14	SDMH 2-13	N/A	7.43	151.00	0.020000	24 inch	0.014	29.71	4,475.65	4,472.63	4,481.75	4,478.73	4,476.52	4,473.78
P-158	SDMH 2-12	SDMH 2-11	N/A	7.32	162.00	0.016914	24 inch	0.014	27.32	4,469.42	4,466.68	4,475.52	4,472.78	4,470.38	4,467.52
P-156	CB 1-27 A	SDMH 1-31	0.53	2.98	22.00	0.095455	12 inch	0.014	10.22	4,462.18	4,460.08	4,465.18	4,465.30	4,462.92	4,461.16
P-155	SDMH 2-08	BT: 2-03	N/A	5.43	8.00	0.028750	18 inch	0.014	16.54	4,511.21	4,510.98	4,517.31	4,517.22	4,512.11	4,511.93
P-154	BT: 2-03	SDMH 2-07	N/A	6.09	88.00	0.028068	18 inch	0.014	16.34	4,510.98	4,508.51	4,517.22	4,514.61	4,511.93	4,509.67
P-153	BT 1-25	O-10	N/A	12.87	18.00	0.015556	24 inch	0.014	26.20	4,455.76	4,455.48	4,463.07	4,463.31	4,457.05	4,456.55
P-152	SDMH 1-30	BT 1-25	N/A	10.68	145.00	0.016345	24 inch	0.014	26.85	4,458.13	4,455.76	4,463.73	4,463.07	4,459.30	4,457.33
P-151	CB 1-23	BT 1-23	0.53	1.44	61.00	0.067705	12 inch	0.014	8.61	4,460.95	4,456.82	4,463.95	4,460.00	4,461.46	4,457.64
P-150	SDMH 2-01	SDMH 2-06	N/A	6.06	100.00	0.037000	18 inch	0.014	18.76	4,508.51	4,504.81	4,514.61	4,510.91	4,509.46	4,505.96
P-149	BT 1-24	BT 1-23	N/A	1.08	41.00	0.005122	12 inch	0.014	2.37	4,457.03	4,456.82	4,460.00	4,460.00	4,457.68	4,457.64
P-148	SDMH 2-01	SDMH 2-04	N/A	6.01	336.00	0.030030	18 inch	0.014	16.90	4,501.10	4,491.01	4,507.20	4,497.11	4,502.05	4,492.15
P-147	BT 1-23	O-9	N/A	2.47	28.00	0.076429	12 inch	0.014	9.15	4,456.82	4,454.68	4,460.00	4,460.26	4,457.49	4,455.04
P-146	SDMH 2-01	BT:CB 2-02	N/A	5.88	185.00	0.025081	24 inch	0.014	33.27	4,488.10	4,483.46	4,494.20	4,489.46	4,488.96	4,484.59
P-145	SDMH 2-01	SDMH 2-01	N/A	8.73	153.00	0.028758	24 inch	0.014	35.62	4,482.59	4,478.19	4,488.69	4,484.29	4,483.64	4,479.45
P-144	SDMH 1-31	SDMH 1-30	N/A	7.48	350.00	0.005000	24 inch	0.014	14.85	4,459.98	4,458.23	4,465.30	4,463.73	4,460.98	4,459.54
P-143	SDMH 1-31	SDMH 1-31	N/A	4.50	350.00	0.005000	18 inch	0.014	6.90	4,461.83	4,460.08	4,466.88	4,465.30	4,462.71	4,461.16
P-142	I-43	SDMH 1-32	0.00	4.50	116.00	0.027328	12 inch	0.010	7.66	4,465.00	4,461.83	4,468.00	4,466.88	4,465.89	4,462.85
P-140	BT 2-04	SDMH 2-08	N/A	5.45	55.00	0.018000	15 inch	0.014	8.05	4,512.20	4,511.21	4,518.20	4,517.31	4,513.15	4,512.30
P-139	SDMH 2-08	BT 2-04	N/A	3.71	54.00	0.009444	15 inch	0.014	5.83	4,512.71	4,512.20	4,518.81	4,518.20	4,513.49	4,513.38
P-138	SDMH 2-11	SDMH 2-09	N/A	3.76	210.00	0.013762	15 inch	0.014	7.04	4,515.60	4,512.71	4,521.60	4,518.81	4,516.38	4,513.36
P-135	BT:CB 1-3	SDMH 1-28	N/A	9.54	144.00	0.018681	24 inch	0.014	28.71	4,469.06	4,466.37	4,475.00	4,472.37	4,470.16	4,467.59
P-134	SDMH 1-28	BT:CB 1-3	N/A	8.55	121.00	0.017190	24 inch	0.014	27.54	4,471.14	4,469.06	4,477.24	4,475.00	4,472.18	4,470.16
P-133	SDMH 1-08	SDMH 1-08	N/A	17.72	79.00	0.006835	36 inch	0.014	51.20	4,454.38	4,453.84	4,462.48	4,462.08	4,456.28	4,456.29
P-132	CB 1-05 A	SDMH 1-08	0.53	2.79	21.00	0.071429	12 inch	0.014	8.84	4,459.24	4,457.74	4,462.24	4,462.08	4,459.96	4,458.15
P-131	SDMH 1-28	SDMH 1-19	N/A	6.69	240.00	0.007500	30 inch	0.014	32.98	4,474.28	4,472.48	4,480.83	4,485.33	4,475.14	4,473.80
P-130	BT:CB 1-14	SDMH 1-13	N/A	17.07	52.00	0.004038	36 inch	0.014	39.36	4,468.30	4,468.09	4,475.69	4,475.29	4,471.02	4,471.00
P-129	SDMH 2-11	BT:CB 1-08	N/A	7.26	152.00	0.022763	24 inch	0.014	31.69	4,466.68	4,463.22	4,472.78	4,469.00	4,467.64	4,464.97
P-127	BT:CB 1-01	SDMH 1-27	N/A	11.89	267.00	0.040974	24 inch	0.014	42.52	4,465.35	4,454.41	4,471.84	4,466.78	4,466.59	4,455.73
P-125	BT 1-06	SDMH 1-06	N/A	17.88	155.00	0.007935	36 inch	0.014	55.17	4,455.71	4,454.48	4,464.00	4,462.48	4,457.06	4,456.39
P-124	SDMH 1-08	SDMH 1-01	N/A	21.97	60.00	0.002000	36 inch	0.014	27.70	4,453.00	4,452.88	4,464.02	4,464.54	4,455.67	4,455.61
P-123	SDMH 1-01	O-5	N/A	33.13	391.00	0.001995	48 inch	0.014	59.57	4,452.78	4,452.00	4,464.54	4,456.00	4,455.50	4,455.27

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Manning's n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
P-118	SDMH 2-06	SDMH 2-08	N/A	6.04	100.00	0.035300	18 inch	0.014	18.33	4,504.81	4,501.28	4,510.91	4,507.20	4,505.76	4,502.25
P-115	SDMH 2-04	SDMH 2-03	N/A	5.93	144.00	0.018194	18 inch	0.014	13.16	4,491.01	4,488.39	4,497.11	4,494.20	4,491.95	4,489.10
P-111	BT:CB 2-02	SDMH 2-02	N/A	7.15	29.00	0.030000	24 inch	0.014	36.38	4,483.46	4,482.59	4,489.46	4,488.69	4,484.41	4,483.85
P-107	SDMH 2-0	SDMH 1-23	N/A	8.67	313.00	0.022204	24 inch	0.014	31.30	4,478.19	4,471.24	4,484.29	4,477.24	4,479.24	4,472.39
P-103	SDMH 1-28	BT:CB 1-02	N/A	9.47	6.00	0.044333	24 inch	0.014	44.23	4,466.27	4,466.00	4,472.37	4,472.14	4,467.37	4,467.41
P-102	BT:CB 1-02	BT:CB 1-01	N/A	10.52	16.00	0.040875	24 inch	0.014	42.47	4,466.00	4,465.35	4,472.14	4,471.84	4,467.17	4,466.85
P-99	SDMH 1-21	SDMH 1-26	N/A	11.78	142.00	0.001972	36 inch	0.014	27.50	4,453.41	4,453.13	4,466.78	4,465.25	4,455.70	4,455.65
P-98	SDMH 1-28	SDMH 1-01	N/A	11.59	77.00	0.001948	36 inch	0.014	27.33	4,453.03	4,452.88	4,465.25	4,464.54	4,455.63	4,455.61
P-95	SDMH 1-01	SDMH 1-02	N/A	22.13	76.00	0.001974	36 inch	0.014	27.51	4,453.25	4,453.10	4,463.33	4,464.02	4,455.83	4,455.75
P-94	SDMH 1-04	SDMH 1-03	N/A	22.26	65.00	0.002000	36 inch	0.014	27.70	4,453.48	4,453.35	4,462.74	4,463.33	4,456.00	4,455.92
P-93	SDMH 2-18	SDMH 1-04	N/A	22.42	78.00	0.002051	36 inch	0.014	28.05	4,453.74	4,453.58	4,462.08	4,462.74	4,456.18	4,456.09
P-83	SDMH 2-18	SDMH 2-17	N/A	4.92	108.00	0.022778	18 inch	0.014	14.72	4,489.90	4,487.44	4,496.00	4,493.54	4,490.75	4,488.46
P-78	SDMH 2-16	SDMH 2-19	N/A	4.84	128.00	0.022500	18 inch	0.014	14.63	4,482.35	4,479.47	4,488.45	4,485.35	4,483.20	4,480.06
P-77	SDMH 2-19	BT:CB 2-07	N/A	4.81	52.00	0.024808	24 inch	0.014	33.08	4,479.35	4,478.06	4,485.35	4,484.06	4,480.12	4,479.11
P-76	BT:CB 2-01	BT:CB 2-08	N/A	6.24	13.00	0.023077	24 inch	0.014	31.91	4,478.06	4,477.76	4,484.06	4,483.76	4,478.94	4,478.92
P-75	BT:CB 2-08	SDMH 2-14	N/A	7.46	95.00	0.022211	24 inch	0.014	31.30	4,477.76	4,475.65	4,483.76	4,481.75	4,478.73	4,476.81
P-72	SDMH 2-11	SDMH 2-12	N/A	7.38	160.00	0.020063	24 inch	0.014	29.75	4,472.63	4,469.42	4,478.73	4,475.52	4,473.60	4,470.57
P-67	BT:CB 1-01	SDMH 1-09	N/A	12.14	34.00	0.000588	24 inch	0.014	5.09	4,463.22	4,463.20	4,469.00	4,468.80	4,464.82	4,464.45
P-66	SDMH 1-11	BT:CB 1-08	N/A	3.39	33.00	0.010909	18 inch	0.014	10.19	4,467.15	4,466.79	4,473.25	4,473.00	4,467.85	4,467.79
P-65	BT:CB 1-01	SDMH 1-09	N/A	4.65	284.00	0.010880	18 inch	0.014	10.17	4,466.79	4,463.70	4,473.00	4,468.80	4,467.62	4,464.41
P-64	SDMH 1-08	SDMH 1-08	N/A	16.43	189.00	0.029947	30 inch	0.014	65.91	4,462.70	4,457.04	4,468.80	4,466.14	4,464.07	4,457.89
P-63	SDMH 1-01	SDMH 1-07	N/A	16.32	63.00	0.003651	36 inch	0.014	37.42	4,456.54	4,456.31	4,466.14	4,465.31	4,457.93	4,457.74
P-62	SDMH 1-01	BT 1-06	N/A	16.24	54.00	0.009259	36 inch	0.014	59.59	4,456.21	4,455.71	4,465.31	4,464.00	4,457.50	4,457.32
P-49	SDMH 2-24	BT 2-10	N/A	0.12	27.00	0.008519	12 inch	0.014	3.05	4,521.14	4,520.91	4,527.24	4,526.00	4,521.48	4,521.48
P-48	BT 2-10	O-3	N/A	1.13	202.00	0.004505	12 inch	0.014	2.22	4,520.91	4,520.00	4,526.00	4,522.00	4,521.41	4,520.45
P-45	SDMH 2-21	SDMH 2-22	N/A	2.34	186.00	0.025161	15 inch	0.014	9.51	4,480.95	4,476.27	4,487.05	4,482.15	4,481.56	4,476.69
P-44	SDMH 2-21	SDMH 2-21	N/A	2.30	144.00	0.011528	15 inch	0.014	6.44	4,476.05	4,474.39	4,482.15	4,479.70	4,476.66	4,474.91
P-41	SDMH 2-28	BT:CB 1-09	N/A	2.22	160.00	0.016750	15 inch	0.014	7.76	4,470.97	4,468.29	4,477.07	4,474.29	4,471.57	4,469.19
P-40	BT:CB 1-01	SDMH 1-10	N/A	3.40	38.00	0.027368	15 inch	0.014	9.92	4,468.29	4,467.25	4,474.29	4,473.25	4,469.03	4,467.76
P-38	SDMH 1-11	BT:CB 1-11	N/A	0.74	29.00	0.010690	12 inch	0.014	3.42	4,467.91	4,467.60	4,474.01	4,473.00	4,470.82	4,470.81
P-37	BT:CB 1-11	O-1	N/A	1.57	42.00	0.011905	12 inch	0.014	3.61	4,467.60	4,467.10	4,473.00	4,475.00	4,470.77	4,470.68
P-27	SDMH 2-26	SDMH 2-27	N/A	3.68	142.00	0.012676	18 inch	0.014	10.98	4,516.68	4,514.88	4,521.68	4,520.00	4,517.41	4,515.75
P-26	SDMH 2-21	O-4	N/A	3.62	111.00	0.007928	18 inch	0.014	8.68	4,514.88	4,514.00	4,520.00	4,516.00	4,515.61	4,514.68
P-22	SDMH 1-21	SDMH 1-24	N/A	5.14	100.00	0.023200	18 inch	0.014	14.86	4,507.76	4,505.44	4,513.76	4,511.34	4,508.63	4,506.39
P-21	SDMH 1-24	BT:CB 1-18	N/A	5.10	113.00	0.047257	18 inch	0.014	21.20	4,505.34	4,500.00	4,511.34	4,505.74	4,506.21	4,501.21

Pipe Report

Label	Upstream Node	Downstream Node	Upsream Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Mannings n	Full Capacity (cfs)	Upsream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upsream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
P-20	BT:CB 1-11	SDMH 1-23	N/A	6.60	40.00	0.040250	18 inch	0.014	19.57	4,500.00	4,498.39	4,505.74	4,504.28	4,500.99	4,499.39
P-19	SDMH 1-22	SDMH 1-22	N/A	6.58	153.00	0.045621	18 inch	0.014	20.83	4,498.18	4,491.20	4,504.28	4,497.09	4,499.17	4,492.19
P-18	SDMH 1-22	SDMH 1-19	N/A	6.52	246.00	0.071585	18 inch	0.014	26.10	4,490.99	4,473.38	4,497.09	4,485.33	4,491.98	4,473.99
P-15	SDMH 1-2	SDMH 1-20	N/A	6.74	58.00	0.004828	30 inch	0.014	26.46	4,474.66	4,474.38	4,479.72	4,480.83	4,475.52	4,475.29
P-12	SDMH 1-11	SDMH 1-11	N/A	12.48	87.00	0.005057	30 inch	0.014	27.08	4,472.38	4,471.94	4,485.33	4,481.52	4,473.57	4,473.28
P-11	SDMH 1-11	BT:CB 1-15	N/A	12.41	71.00	0.005070	30 inch	0.014	27.12	4,471.84	4,471.48	4,481.52	4,479.48	4,473.08	4,473.03
P-10	BT:CB 1-11	SDMH 1-17	N/A	14.59	28.00	0.005000	30 inch	0.014	26.93	4,471.48	4,471.34	4,479.48	4,478.90	4,472.79	4,472.68
P-9	SDMH 1-11	SDMH 1-16	N/A	14.57	112.00	0.005893	36 inch	0.014	47.54	4,471.24	4,470.58	4,478.90	4,478.09	4,472.46	4,472.02
P-8	SDMH 1-11	SDMH 1-12	N/A	14.47	132.00	0.005000	36 inch	0.014	43.79	4,470.58	4,469.92	4,478.09	4,477.22	4,471.79	4,471.25
P-7	SDMH 1-11	SDMH 1-12	N/A	14.34	102.00	0.009314	36 inch	0.014	59.77	4,469.82	4,468.87	4,477.22	4,476.48	4,471.03	4,471.16
P-6	SDMH 1-11	BT:CB 1-14	N/A	14.26	118.00	0.003983	36 inch	0.014	39.09	4,468.77	4,468.30	4,476.48	4,475.69	4,471.11	4,471.07
P-3	SDMH 1-11	BT:CB 1-12	N/A	19.15	97.00	0.003505	36 inch	0.014	36.67	4,467.99	4,467.65	4,475.29	4,474.84	4,470.94	4,470.85
P-2	BT:CB 1-11	SDMH 1-12	N/A	20.24	43.00	0.003953	36 inch	0.014	38.94	4,467.65	4,467.48	4,474.84	4,474.63	4,470.79	4,470.74
P-1	SDMH 1-11	O-2	N/A	20.12	58.00	0.005690	42 inch	0.014	70.47	4,467.33	4,467.00	4,474.63	4,475.00	4,470.70	4,470.68
LAT:1-35	DITCH 2-1	O-8	0.00	0.00	57.00	0.020000	12 inch	0.014	4.68	4,530.00	4,528.86	4,533.00	4,531.86	4,530.00	4,528.86
LAT:CB 2-15	CB 2-15 A	SDMH 2-26	0.53	1.82	35.00	0.100000	12 inch	0.014	10.46	4,520.28	4,516.78	4,523.28	4,521.68	4,520.85	4,517.56
LAT:CB 2-14	CB 2-14 A	SDMH 2-26	0.53	2.03	26.00	0.145385	12 inch	0.014	12.61	4,520.56	4,516.78	4,523.56	4,521.68	4,521.17	4,517.56
LAT:CB 2-13	CB 2-13	SDMH 2-25	0.53	0.13	40.00	0.065750	12 inch	0.014	8.48	4,551.22	4,548.59	4,554.22	4,554.59	4,551.37	4,548.76
LAT:CB 2-12	CB 2-12	BT 2-10	0.53	1.05	25.00	0.161200	12 inch	0.014	13.28	4,525.94	4,521.91	4,528.94	4,526.00	4,526.37	4,522.10
LAT:CB 2-10	CB 2-10 A	SDMH 2-19	0.53	4.04	31.00	0.135484	12 inch	0.014	12.18	4,496.69	4,492.49	4,499.69	4,498.59	4,497.54	4,493.52
LAT:CB 2-09	CB 2-09	SDMH 2-19	0.53	1.41	49.00	0.089367	12 inch	0.014	9.83	4,496.82	4,492.49	4,499.82	4,498.59	4,497.32	4,493.52
LAT:CB 2-08	CB 2-08 A	BT:CB 2-08	0.53	1.44	24.00	0.112917	12 inch	0.014	11.12	4,480.97	4,478.26	4,483.97	4,483.76	4,481.48	4,478.92
LAT:CB 2-07	CB 2-07 A	BT:CB 2-07	0.53	1.68	7.00	0.384286	12 inch	0.014	20.51	4,481.25	4,478.56	4,484.25	4,484.06	4,481.80	4,479.11
LAT:CB 1-21	CB 1-22 A	SDMH 1-25	0.53	1.57	57.00	0.063684	12 inch	0.014	8.35	4,511.49	4,507.86	4,514.49	4,513.76	4,512.02	4,508.81
LAT:CB 1-20	CB 1-21 A	SDMH 1-25	0.53	2.29	40.00	0.096000	12 inch	0.014	10.25	4,511.70	4,507.86	4,514.70	4,513.76	4,512.35	4,508.81
LAT:CB 1-19	CB 1-20	SDMH 1-25	0.53	1.52	33.00	0.123030	12 inch	0.014	11.60	4,511.92	4,507.86	4,514.92	4,513.76	4,512.44	4,508.81
LAT:CB 1-18	CB 1-19 A	BT:CB 1-18	0.53	1.69	36.00	0.066111	12 inch	0.014	9.71	4,503.60	4,500.50	4,506.60	4,505.74	4,504.15	4,501.21
LAT:CB 1-17	CB 1-18 A	SDMH 1-21	0.53	3.21	50.00	0.024200	15 inch	0.014	9.33	4,476.62	4,475.41	4,479.62	4,479.72	4,477.34	4,475.92
LAT:CB 1-16	CB 1-17 A	SDMH 1-21	0.53	3.90	58.00	0.020862	15 inch	0.014	8.66	4,476.62	4,475.41	4,479.62	4,479.72	4,477.42	4,476.00
LAT:CB 1-15	CB 1-16	BT:CB 1-15	0.53	2.73	5.00	0.732000	12 inch	0.014	28.30	4,476.64	4,472.98	4,479.64	4,479.48	4,477.35	4,473.25
LAT:CB 1-14	CB 1-15 A	BT:CB 1-14	0.53	3.64	7.00	0.397143	12 inch	0.014	20.85	4,472.97	4,470.19	4,475.97	4,475.69	4,473.78	4,471.07
LAT:CB 1-13	CB 1-14	SDMH 1-13	0.53	2.43	26.00	0.135000	12 inch	0.014	12.15	4,473.50	4,469.99	4,476.50	4,475.29	4,474.17	4,471.00
LAT:CB 1-12	CB 1-13	BT:CB 1-12	0.53	1.31	27.00	0.128148	12 inch	0.014	11.84	4,472.06	4,468.60	4,475.06	4,474.84	4,472.54	4,470.85
LAT:CB 1-11	CB 1-12	BT:CB 1-11	0.53	0.86	12.00	0.140000	12 inch	0.014	12.38	4,471.12	4,469.44	4,474.12	4,473.00	4,471.51	4,470.81
LAT:CB 1-10	CB 1-11	SDMH 1-11	0.53	0.74	12.00	0.100833	12 inch	0.014	10.50	4,471.12	4,469.91	4,474.12	4,474.01	4,471.48	4,470.83

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Inlet Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Mannings n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
LAT: CB 1-09	CB 1-10	BT: CB 1-06	0.53	1.31	34.00	0.055882	12 inch	0.014	7.82	4,471.19	4,469.29	4,474.19	4,474.29	4,471.67	4,469.57
LAT: CB 1-08	CB 1-09 A	BT: CB 1-06	0.53	1.50	7.00	0.134286	12 inch	0.014	12.12	4,470.00	4,469.06	4,473.00	4,473.00	4,470.52	4,469.34
LAT: CB 1-06	CB 1-07 A	BT: CB 1-06	0.53	2.43	7.00	0.341429	12 inch	0.014	19.33	4,466.11	4,463.72	4,469.11	4,469.00	4,466.78	4,464.97
LAT: CB 1-05	CB 1-06	BT 1-06	0.53	1.96	54.00	0.090741	12 inch	0.014	9.97	4,461.61	4,456.71	4,464.61	4,464.00	4,462.21	4,457.32
LAT: CB 1-02	CB 1-02 A	BT: CB 1-02	0.53	1.32	6.00	0.435000	12 inch	0.014	21.82	4,469.11	4,466.50	4,472.11	4,472.14	4,469.60	4,467.41
LAT: CB 2-11	CB 2-11 A	SDMH 2-23	0.53	2.35	53.00	0.085094	12 inch	0.014	9.65	4,485.46	4,480.95	4,488.46	4,487.05	4,486.12	4,481.68
LAT: CB 1-08	CB 1-08 A	BT: CB 1-06	0.53	2.99	26.00	0.106538	12 inch	0.010	15.12	4,466.49	4,463.72	4,469.49	4,469.00	4,467.23	4,464.97
LAT: CB 1-03	CB 1-04 A	SDMH 1-06	0.53	2.48	34.00	0.073529	12 inch	0.010	12.56	4,459.24	4,456.74	4,462.35	4,462.08	4,459.91	4,457.06
LAT: 2-06	CB 2-06 A	SDMH 2-10	0.53	2.40	45.00	0.085333	12 inch	0.014	9.66	4,519.48	4,515.64	4,522.48	4,521.60	4,520.14	4,516.55
LAT: 2-05	CB 2-05	SDMH 2-10	0.53	1.47	27.00	0.117778	12 inch	0.014	11.35	4,518.82	4,515.64	4,521.82	4,521.60	4,519.33	4,516.55
LAT: 2-03	CB 2-03 A	BT: 2-03	0.53	0.75	32.00	0.115000	12 inch	0.010	15.71	4,514.66	4,510.98	4,517.66	4,517.22	4,515.02	4,511.93
LAT: 1-25	CB 1-25	BT 1-25	0.53	2.35	23.00	0.182174	12 inch	0.014	14.12	4,459.95	4,455.76	4,462.95	4,463.07	4,460.61	4,457.33
LAT 2-04	CB 2-04 A	BT 2-04	0.53	2.02	7.00	0.458571	12 inch	0.014	22.40	4,515.41	4,512.20	4,518.41	4,518.20	4,516.02	4,513.38
LAT 2-02	CB 2-02 A	BT: CB 2-02	0.53	1.48	26.00	0.087308	12 inch	0.014	9.77	4,486.73	4,484.46	4,489.73	4,489.46	4,487.25	4,484.72
LAT 2-01	CB 2-01 A	SDMH 2-02	0.53	1.64	10.00	0.233000	12 inch	0.014	15.97	4,485.92	4,483.59	4,488.92	4,488.69	4,486.46	4,483.83
LAT 1-3	CB 1-03	BT: CB 1-3	0.53	1.21	24.00	0.117083	12 inch	0.010	15.85	4,472.37	4,469.56	4,475.37	4,475.00	4,472.83	4,470.16
LAT 1-26	CB 1-26 A	SDMH 1-30	0.53	3.36	22.00	0.108182	12 inch	0.010	15.23	4,460.61	4,458.23	4,463.61	4,463.73	4,461.39	4,459.54
LAT 1-24	CB 1-24	BT 1-24	0.53	1.09	54.00	0.072593	12 inch	0.014	8.91	4,460.95	4,457.03	4,463.95	4,460.00	4,461.39	4,457.71
LAT 1-01	CB 1-01 A	BT: CB 1-01	0.53	1.72	54.00	0.053889	12 inch	0.014	7.68	4,468.80	4,465.89	4,471.80	4,471.84	4,469.36	4,466.85

Inlet Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Rim Elevation (ft)	Sump Elevation (ft)	Area (acres)	Inlet C	Inlet CA (acres)	Total Flow To Inlet (cfs)	Total Intercepted Flow (cfs)	Total Bypassed Flow (cfs)	Bypass Target	Time of Concentration (min)	Inlet Location	Known Flow (cfs)	Inlet
CB 1-01 A-E	9+31	4,471.80	4,471.80	4,468.80	1.40	0.53	0.74	1.72	1.72	0.00	CB 1-04 A-	11.96	In Sag	0.00	Combination DUAL
CB 1-02 A-E	8+99	4,472.11	4,472.11	4,469.11	1.49	0.53	0.79	1.72	1.32	0.40	CB 1-04 A-	11.87	On Grade	0.00	Combination DUAL
CB 1-03	10+67	4,475.37	4,475.37	4,472.37	2.29	0.53	1.21	1.49	1.21	0.28	CB 1-01 A-	13.79	On Grade	0.00	Combination 4R
CB 1-04 A-E	7+04	4,462.35	4,462.35	4,459.24	3.42	0.53	1.81	2.48	2.48	0.00		14.92	In Sag	0.00	Combination DUAL
CB 1-05 A-E	6+91	4,462.24	4,462.24	4,459.24	4.59	0.53	2.43	2.79	2.79	0.00		15.89	In Sag	0.00	Combination DUAL
CB 1-06	9+58	4,464.61	4,464.61	4,461.61	2.99	0.53	1.58	1.96	1.96	0.00		13.66	In Sag	0.00	Combination 4R
CB 1-07 A-E	12+51	4,469.11	4,469.11	4,466.11	2.90	0.53	1.54	2.43	2.43	0.00		14.84	In Sag	0.00	Combination DUAL
CB 1-08 A-E	12+70	4,469.49	4,469.49	4,466.49	2.87	0.53	1.52	2.99	2.99	0.00		14.15	In Sag	0.00	Combination DUAL
CB 1-09 A-E	15+01	4,473.00	4,473.00	4,470.00	3.60	0.53	1.91	2.22	1.50	0.72	CB 1-08 A-	15.18	On Grade	0.00	Combination DUAL
CB 1-10	15+99	4,474.19	4,474.19	4,471.19	2.59	0.53	1.37	1.74	1.31	0.43	CB 1-11	13.14	On Grade	0.00	Combination 4R
CB 1-11	0+83	4,474.12	4,474.12	4,471.12	0.35	0.53	0.19	0.74	0.74	0.00		10.00	In Sag	0.00	Combination 4R
CB 1-12	0+54	4,474.12	4,474.12	4,471.12	0.08	0.53	0.03	0.86	0.86	0.00		10.00	In Sag	0.00	Combination 4R
CB 1-13	1+28	4,475.06	4,475.06	4,472.06	3.17	0.53	1.68	2.00	1.31	0.69	CB 1-12	14.58	On Grade	0.00	Combination 4R
CB 1-14	2+24	4,476.50	4,476.50	4,473.50	2.91	0.53	1.54	2.43	2.43	0.00		13.04	In Sag	0.00	Combination 4R
CB 1-15 A-E	2+57	4,475.97	4,475.97	4,472.97	4.40	0.53	2.33	3.64	3.64	0.00		10.44	In Sag	0.00	Combination DUAL
CB 1-16	7+47	4,479.64	4,479.64	4,476.64	3.66	0.53	1.94	2.73	2.73	0.00		10.11	In Sag	0.00	Combination 4R
CB 1-17 A-E	12+56	4,479.62	4,479.62	4,476.62	6.01	0.53	3.19	3.90	3.90	0.00		13.88	In Sag	0.00	Combination DUAL
CB 1-18 A-E	12+48	4,479.62	4,479.62	4,476.62	4.45	0.53	2.36	3.21	3.21	0.00		11.07	In Sag	0.00	Combination DUAL
CB 1-19 A-E	13+75	4,506.60	4,506.60	4,503.60	1.81	0.53	0.96	1.69	1.69	0.00		10.00	In Sag	0.00	Combination DUAL
CB 1-20	15+85	4,514.92	4,514.92	4,511.92	2.64	0.53	1.40	1.83	1.52	0.31	CB 1-19 A-	12.12	On Grade	0.00	Combination 4R
CB 1-21 A-E	15+92	4,514.70	4,514.70	4,511.70	4.88	0.53	2.59	3.58	2.29	1.29	CB 1-22 A-	10.58	On Grade	0.00	Combination DUAL
CB 1-22 A-E	16+09	4,514.49	4,514.49	4,511.49	0.35	0.53	0.19	1.57	1.57	0.00		10.00	In Sag	0.00	Combination DUAL
CB 1-23	0+89	4,463.95	4,463.95	4,460.95	2.24	0.53	1.19	1.44	1.44	0.00		14.04	In Sag	0.00	Combination 4R
CB 1-24	1+23	4,463.95	4,463.95	4,460.95	1.71	0.53	0.91	1.09	1.09	0.00		14.40	In Sag	0.00	Combination 4R
CB 1-25	0+41	4,462.95	4,462.95	4,459.95	1.65	0.53	0.87	2.35	2.35	0.00		14.85	In Sag	0.00	Combination DUAL
CB 1-26 A-E	1+85	4,463.61	4,463.61	4,460.61	5.94	0.53	3.15	4.65	3.36	1.29	CB 1-25	15.76	On Grade	0.00	Combination DUAL
CB 1-27 A-E	5+35	4,465.18	4,465.18	4,462.18	6.56	0.53	3.48	4.02	2.98	1.04	CB 1-26 A-	15.54	On Grade	0.00	Combination DUAL
CB 2-01 A-E	16+40	4,488.92	4,488.92	4,485.92	3.72	0.53	1.97	2.22	1.64	0.58	CB 1-02 A-	16.69	On Grade	0.00	Combination DUAL
CB 2-02 A-E	16+85	4,489.73	4,489.73	4,486.73	2.80	0.53	1.48	1.89	1.48	0.41	CB 1-01 A-	13.91	On Grade	0.00	Combination DUAL
CB 2-03 A-E	26+44	4,517.66	4,517.66	4,514.66	0.07	0.53	0.04	0.83	0.75	0.08	CB 2-02 A-	12.26	On Grade	0.00	Combination DUAL
CB 2-04 A-E	26+82	4,518.41	4,518.41	4,515.41	1.47	0.53	0.78	2.02	2.02	0.00		12.01	In Sag	0.00	Combination DUAL
CB 2-05	29+66	4,521.82	4,521.82	4,518.82	3.51	0.53	1.86	2.16	1.47	0.70	CB 2-03 A-	15.26	On Grade	0.00	Combination Type4
CB 2-06 A-E	29+84	4,522.48	4,522.48	4,519.48	5.16	0.53	2.73	3.32	2.40	0.92	CB 2-04 A-	14.06	On Grade	0.00	Combination DUAL
CB 2-07 A-E	19+84	4,484.25	4,484.25	4,481.25	3.42	0.53	1.81	2.38	1.68	0.70	CB 1-07 A-	12.00	On Grade	0.00	Combination DUAL
CB 2-08 A-E	19+88	4,483.97	4,483.97	4,480.97	2.01	0.53	1.07	1.87	1.44	0.43	CB 1-08 A-	11.95	On Grade	0.00	Combination DUAL

Inlet Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Rim Elevation (ft)	Sump Elevation (ft)	Area (acres)	Inlet C	Inlet CA (acres)	Total Flow To Inlet (cfs)	Total Intercepted Flow (cfs)	Total Bypassed Flow (cfs)	Bypass Target	Time of Concentration (min)	Inlet Location	Known Flow (cfs)	Inlet
CB 2-09	26+48	4,499.82	4,499.82	4,496.82	2.96	0.53	1.57	1.83	1.41	0.41	CB 2-08 A-	15.18	On Grade	0.00	Combination 4R
CB 2-10 A-B	26+30	4,499.69	4,499.69	4,496.69	5.74	0.53	3.04	4.04	4.04	0.00		11.71	In Sag	0.00	Combination DUAL
CB 2-11 A-B	22+64	4,488.46	4,488.46	4,485.46	3.14	0.53	1.66	2.35	2.35	0.00		10.00	In Sag	0.00	Combination DUAL
CB 2-12	2+27	4,528.94	4,528.94	4,525.94	1.45	0.53	0.77	1.06	1.05	0.01	CB 1-10	10.54	On Grade	0.00	Combination 4R
CB 2-13	6+20	4,554.22	4,554.22	4,551.22	0.17	0.53	0.09	0.13	0.13	0.00	CB 2-04 A-	10.00	On Grade	0.00	Combination 4R
CB 2-14 A-B	2+79	4,523.56	4,523.56	4,520.56	3.48	0.53	1.84	2.56	2.03	0.53	CB 1-14	10.47	On Grade	0.00	Combination DUAL
CB 2-15 A-B	2+88	4,523.28	4,523.28	4,520.28	3.23	0.53	1.71	2.18	1.82	0.36	CB 1-15 A-	12.79	On Grade	0.00	Combination DUAL
DITCH 2-1	0+57	4,533.00	4,533.00	4,530.00	3.07	0.00	0.00	0.00	0.00	0.00		16.33	In Sag	0.00	Generic Default 10'
I-43	9+79	4,468.00	4,468.00	4,465.00	0.00	0.00	0.00	4.50	4.50	0.00		0.00	In Sag	0.00	Generic Default 10'

Scenario: Base

Junction Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Set Rim Equal to Ground Elevation?	Rim Elevation (ft)	Sump Elevation (ft)	Bolted Cover?	Structure Diameter (ft)	Description
BT 1-06	9+04	4,464.00	true	4,464.00	4,455.71	true	0.00	
BT 1-23	0+28	4,460.00	true	4,460.00	4,456.82	true	0.00	
BT 1-24	0+69	4,460.00	true	4,460.00	4,457.03	true	0.00	
BT 1-25	0+18	4,463.07	true	4,463.07	4,455.76	true	0.00	
BT 2-04	26+75	4,518.20	true	4,518.20	4,512.20	true	0.00	
BT 2-10	2+02	4,526.00	true	4,526.00	4,520.91	true	0.00	
BT: 2-03	26+12	4,517.22	true	4,517.22	4,510.98	true	0.00	
BT:CB 1-01	8+77	4,471.84	true	4,471.84	4,465.35	true	0.00	
BT:CB 1-02	8+93	4,472.14	true	4,472.14	4,466.00	true	0.00	
BT:CB 1-06	12+44	4,469.00	true	4,469.00	4,463.22	true	0.00	
BT:CB 1-08	14+94	4,473.00	true	4,473.00	4,466.79	true	0.00	
BT:CB 1-09	15+65	4,474.29	true	4,474.29	4,468.29	true	0.00	
BT:CB 1-11	0+42	4,473.00	true	4,473.00	4,467.60	true	0.00	
BT:CB 1-12	1+01	4,474.84	true	4,474.84	4,467.65	true	0.00	
BT:CB 1-14	2+50	4,475.69	true	4,475.69	4,468.30	true	0.00	
BT:CB 1-15	7+42	4,479.48	true	4,479.48	4,471.48	true	0.00	
BT:CB 1-18	13+39	4,505.74	true	4,505.74	4,500.00	true	0.00	
BT:CB 1-3	10+43	4,475.00	true	4,475.00	4,469.06	true	0.00	
BT:CB 2-02	16+59	4,489.46	true	4,489.46	4,483.46	true	0.00	
BT:CB 2-07	19+77	4,484.06	true	4,484.06	4,478.06	true	0.00	
BT:CB 2-08	19+64	4,483.76	true	4,483.76	4,477.76	true	0.00	
SDMH 1-01	3+91	4,464.54	true	4,464.54	4,452.78	false	4.00	
SDMH 1-02	4+51	4,464.02	true	4,464.02	4,453.00	false	4.00	
SDMH 1-03	5+27	4,463.33	true	4,463.33	4,453.25	false	4.00	
SDMH 1-04	5+92	4,462.74	true	4,462.74	4,453.48	false	4.00	
SDMH 1-05	6+70	4,462.08	true	4,462.08	4,453.74	false	4.00	
SDMH 1-06	7+49	4,462.48	true	4,462.48	4,454.38	false	4.00	
SDMH 1-07	9+58	4,465.31	true	4,465.31	4,456.21	false	4.00	
SDMH 1-08	10+21	4,466.14	true	4,466.14	4,456.54	false	4.00	
SDMH 1-09	12+10	4,468.80	true	4,468.80	4,462.70	false	4.00	
SDMH 1-10	15+27	4,473.25	true	4,473.25	4,467.15	false	4.00	
SDMH 1-11	0+71	4,474.01	true	4,474.01	4,467.91	false	4.00	
SDMH 1-12	0+58	4,474.63	true	4,474.63	4,467.33	false	4.00	
SDMH 1-13	1+98	4,475.29	true	4,475.29	4,467.99	false	4.00	
SDMH 1-14	3+68	4,476.48	true	4,476.48	4,468.77	false	4.00	
SDMH 1-15	4+70	4,477.22	true	4,477.22	4,469.82	false	4.00	
SDMH 1-16	6+02	4,478.09	true	4,478.09	4,470.58	false	4.00	
SDMH 1-17	7+14	4,478.90	true	4,478.90	4,471.24	false	4.00	
SDMH 1-18	8+13	4,481.52	true	4,481.52	4,471.84	false	4.00	
SDMH 1-19	9+00	4,485.33	true	4,485.33	4,472.38	false	4.00	
SDMH 1-20	11+40	4,480.83	true	4,480.83	4,474.28	false	4.00	
SDMH 1-21	11+98	4,479.72	true	4,479.72	4,474.66	false	4.00	
SDMH 1-22	11+46	4,497.09	true	4,497.09	4,490.99	false	4.00	
SDMH 1-23	12+99	4,504.28	true	4,504.28	4,498.18	false	4.00	
SDMH 1-24	14+52	4,511.34	true	4,511.34	4,505.34	false	4.00	
SDMH 1-25	15+52	4,513.76	true	4,513.76	4,507.76	false	4.00	
SDMH 1-26	4+68	4,465.25	true	4,465.25	4,453.03	false	4.00	
SDMH 1-27	6+10	4,466.78	true	4,466.78	4,453.41	false	4.00	
SDMH 1-28	8+99	4,472.37	true	4,472.37	4,466.27	false	4.00	
SDMH 1-29	11+64	4,477.24	true	4,477.24	4,471.14	false	4.00	
SDMH 1-30	1+63	4,463.73	true	4,463.73	4,458.13	false	4.00	

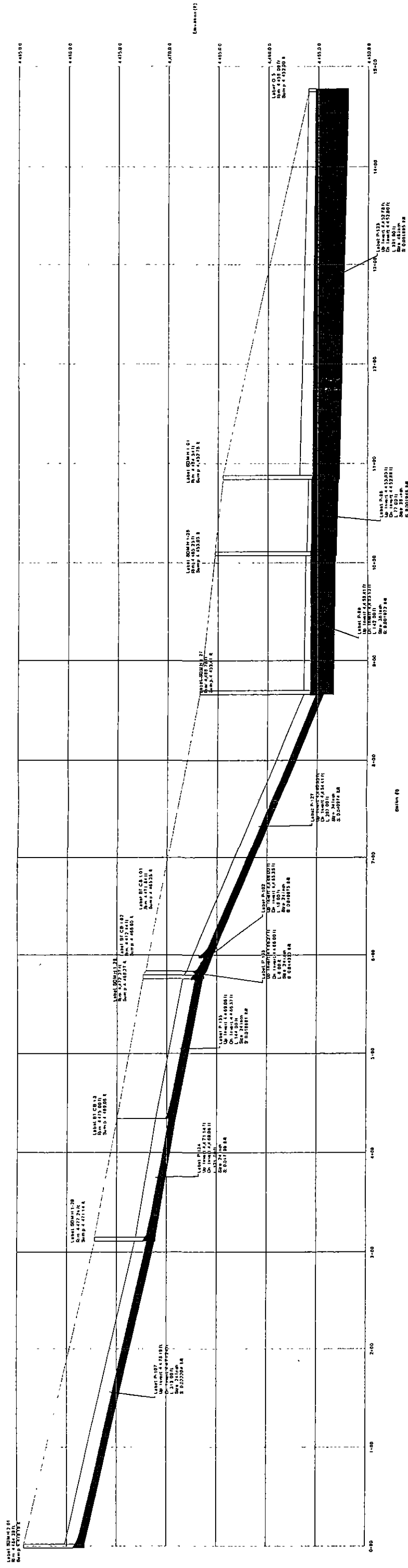
Scenario: Base

Junction Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Set Rim Equal to Ground Elevation?	Rim Elevation (ft)	Sump Elevation (ft)	Bolted Cover?	Structure Diameter (ft)	Description
SDMH 1-31	5+13	4,465.30	true	4,465.30	4,459.98	false	4.00	
SDMH 1-32	8+63	4,466.88	true	4,466.88	4,461.83	false	4.00	
SDMH 2-01	14+77	4,484.29	true	4,484.29	4,478.19	false	4.00	
SDMH 2-02	16+30	4,488.69	true	4,488.69	4,482.59	true	0.00	
SDMH 2-03	18+44	4,494.20	true	4,494.20	4,488.10	false	4.00	
SDMH 2-04	19+88	4,497.11	true	4,497.11	4,491.01	false	4.00	
SDMH 2-05	23+24	4,507.20	true	4,507.20	4,501.10	false	4.00	
SDMH 2-06	24+24	4,510.91	true	4,510.91	4,504.81	false	4.00	
SDMH 2-07	25+24	4,514.61	true	4,514.61	4,508.51	false	4.00	
SDMH 2-08	26+20	4,517.31	true	4,517.31	4,511.21	false	4.00	
SDMH 2-09	27+29	4,518.81	true	4,518.81	4,512.71	false	4.00	
SDMH 2-10	29+39	4,521.60	true	4,521.60	4,515.60	false	4.00	
SDMH 2-11	13+96	4,472.78	true	4,472.78	4,466.68	false	4.00	
SDMH 2-12	15+58	4,475.52	true	4,475.52	4,469.42	false	4.00	
SDMH 2-13	17+18	4,478.73	true	4,478.73	4,472.63	false	4.00	
SDMH 2-14	18+69	4,481.75	true	4,481.75	4,475.65	false	4.00	
SDMH 2-15	20+29	4,485.35	true	4,485.35	4,479.35	false	4.00	
SDMH 2-16	21+57	4,488.45	true	4,488.45	4,482.35	false	4.00	
SDMH 2-17	23+72	4,493.54	true	4,493.54	4,487.44	false	4.00	
SDMH 2-18	24+80	4,496.00	true	4,496.00	4,489.90	false	4.00	
SDMH 2-19	25+99	4,498.59	true	4,498.59	4,492.49	false	4.00	
SDMH 2-20	17+25	4,477.07	true	4,477.07	4,470.97	false	4.00	
SDMH 2-21	18+81	4,479.70	true	4,479.70	4,473.60	false	4.00	
SDMH 2-22	20+25	4,482.15	true	4,482.15	4,476.05	false	4.00	
SDMH 2-23	22+11	4,487.05	true	4,487.05	4,480.95	false	4.00	
SDMH 2-24	2+29	4,527.24	true	4,527.24	4,521.14	false	4.00	
SDMH 2-25	5+80	4,554.59	true	4,554.59	4,548.59	false	4.00	
SDMH 2-26	2+53	4,521.68	true	4,521.68	4,516.68	false	4.00	
SDMH 2-27	1+11	4,520.00	true	4,520.00	4,514.88	false	4.00	

Profile
Scenario: Base

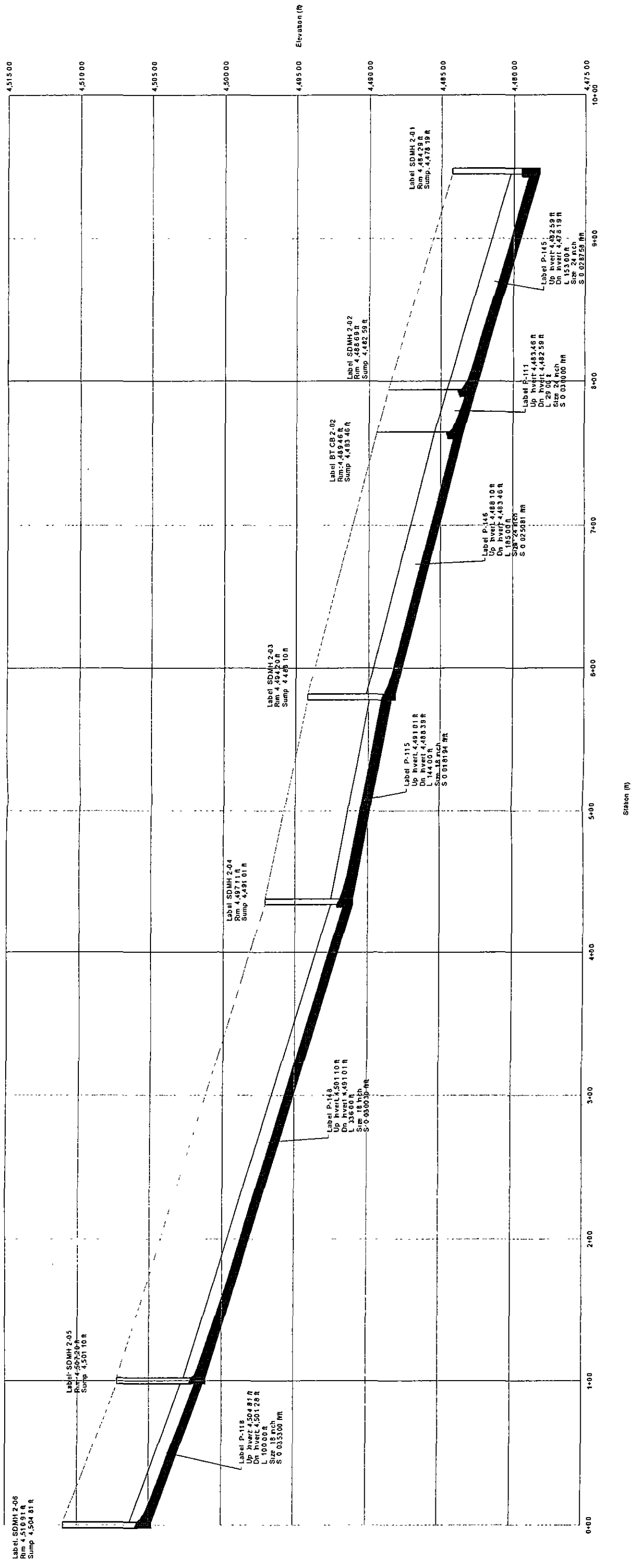
Profile: GOLD RIVER NORTH - A
Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER NORTH - B

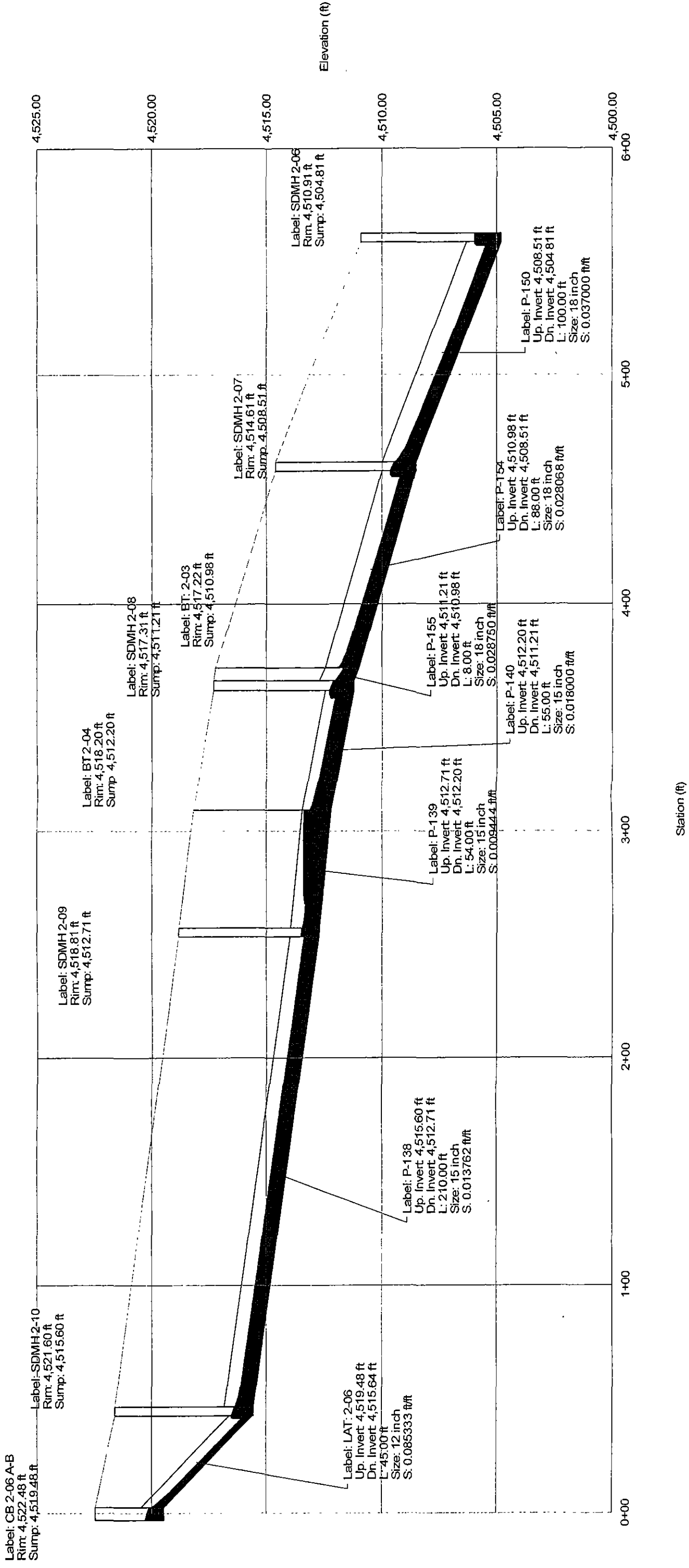
Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER NORTH - C

Scenario: Base

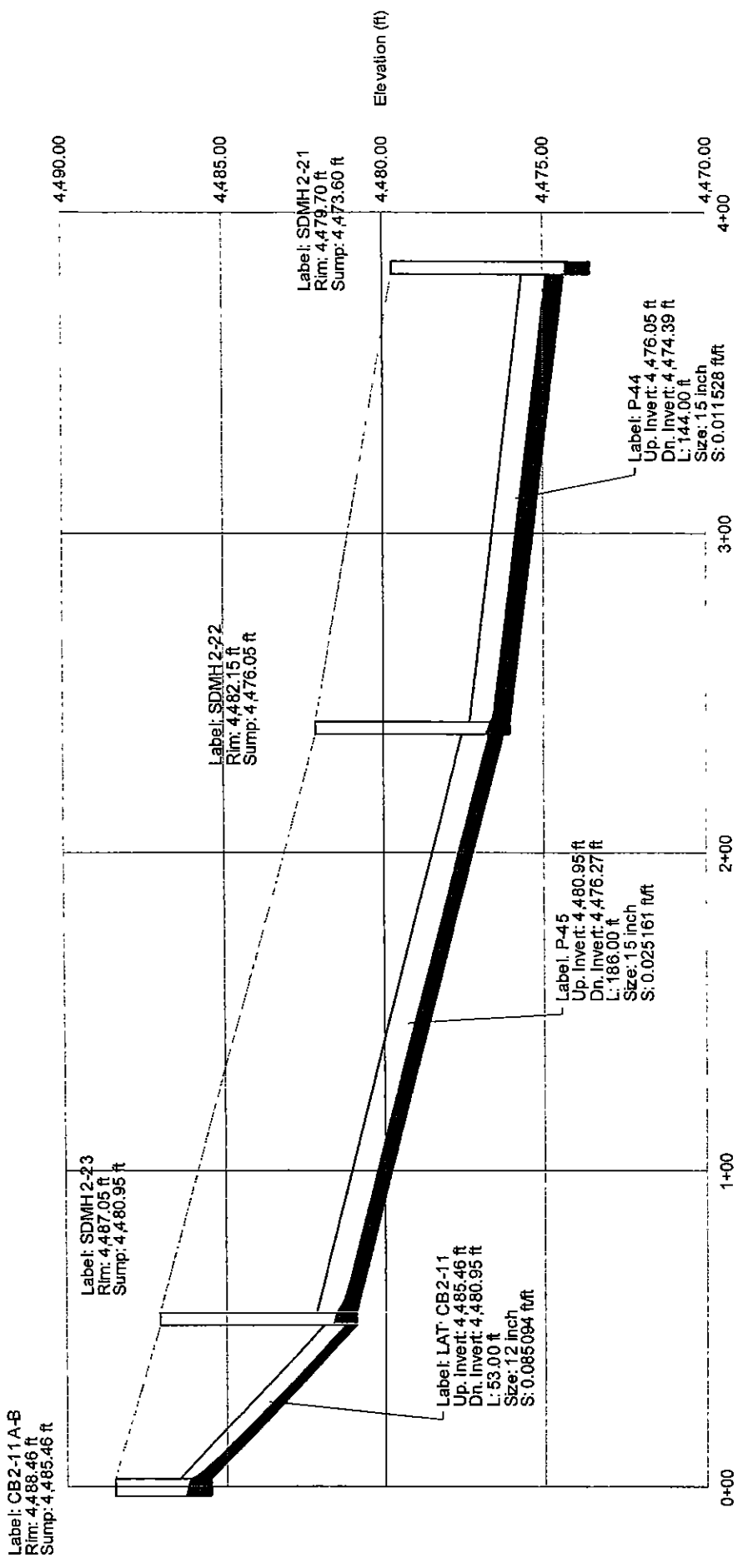




Scenario: Base

Profile: HOLLOW BASIN - A

Scenario: Base

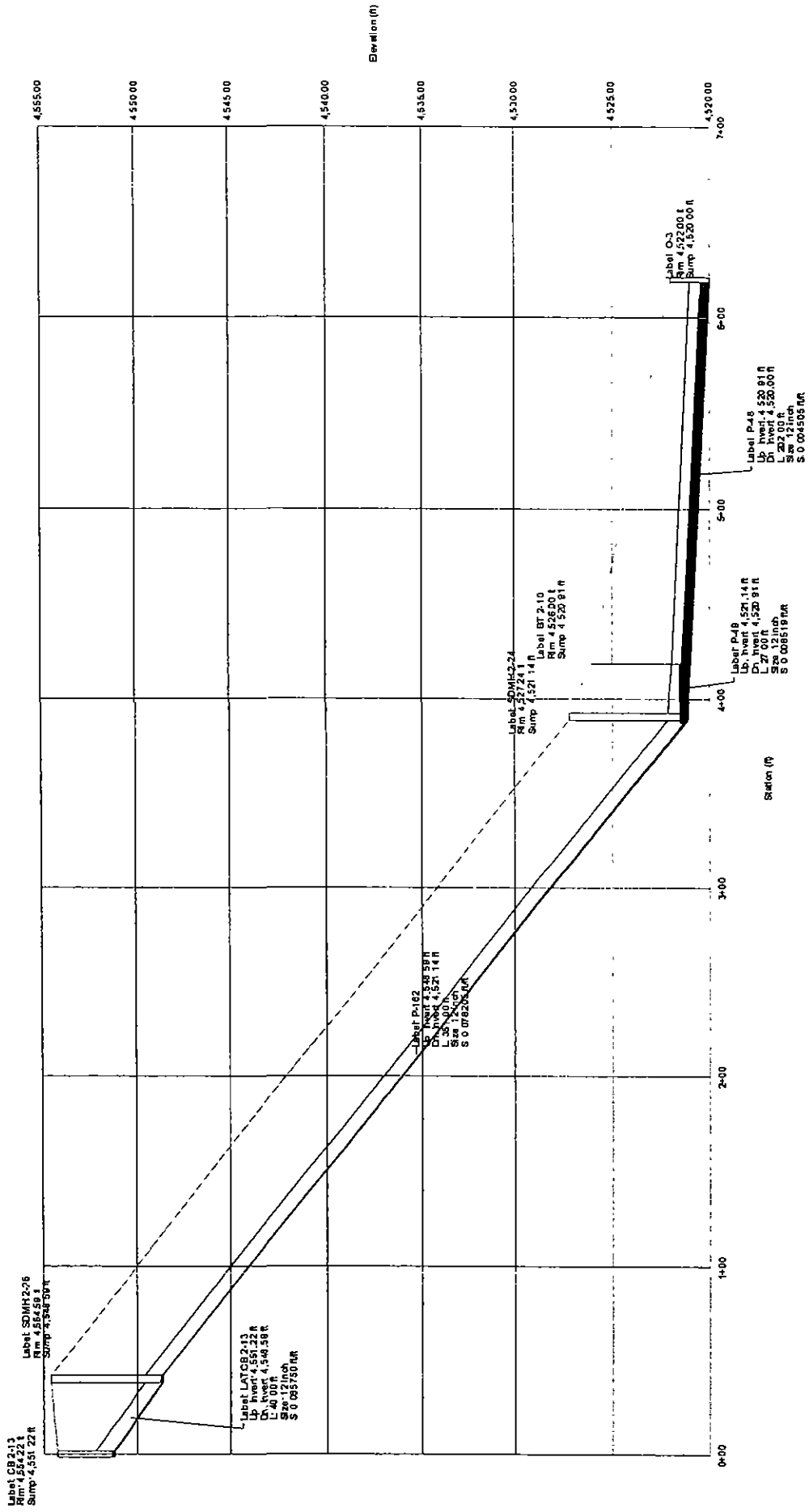


ofile

Scenario: Base

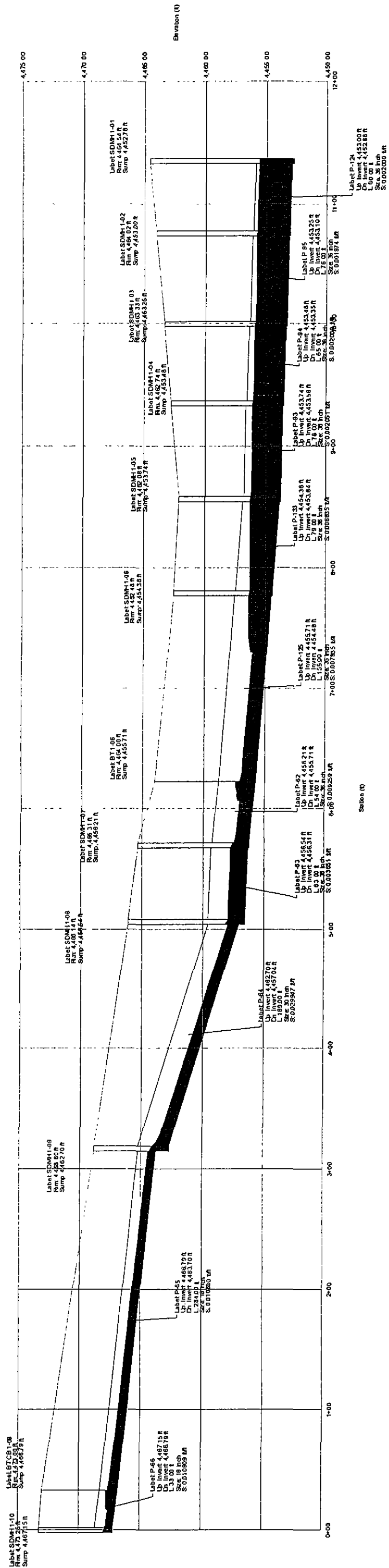
Profile: HOLLOW BASIN - B

Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER SOUTH - A
Scenario: Base

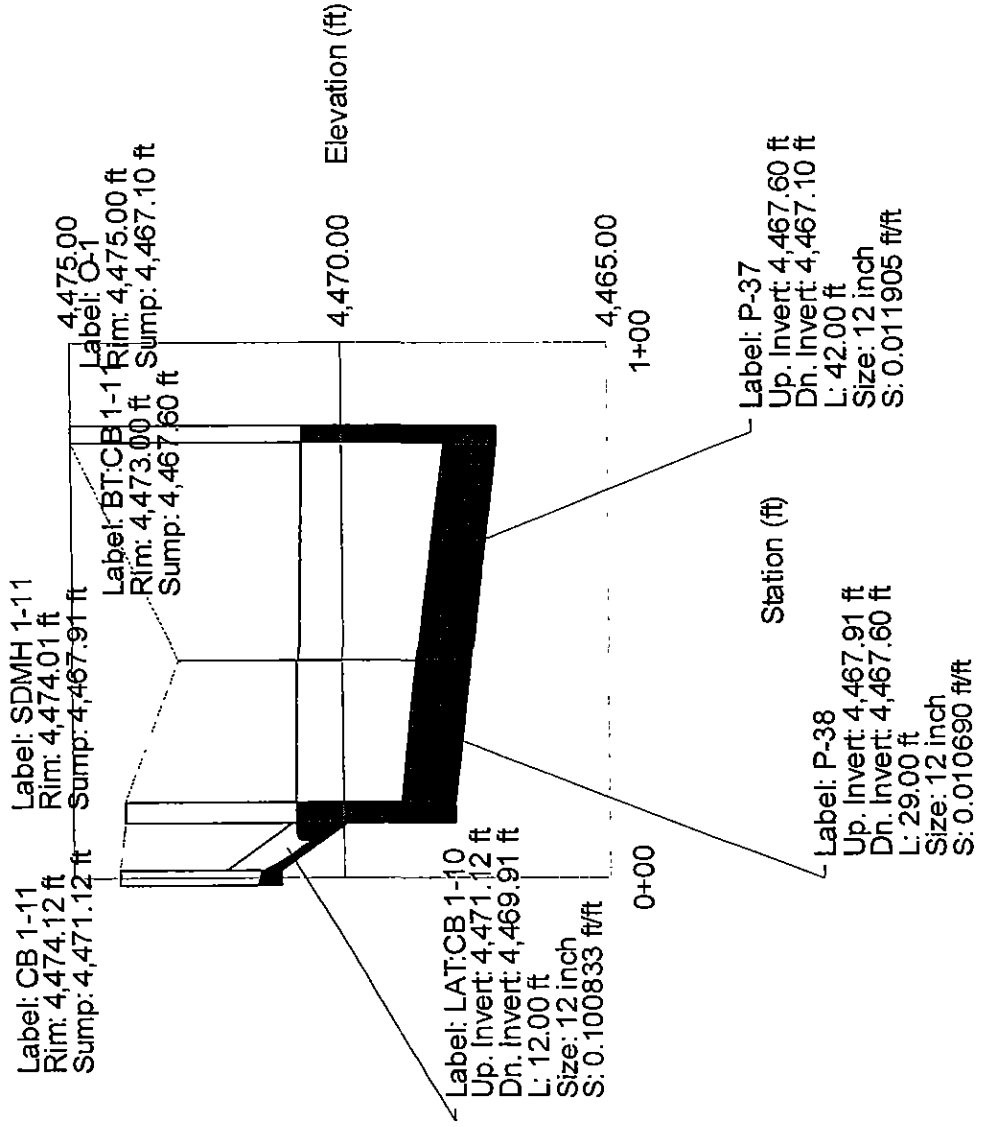




Scenario: Base

Profile: GOLD RIVER SOUTH - B

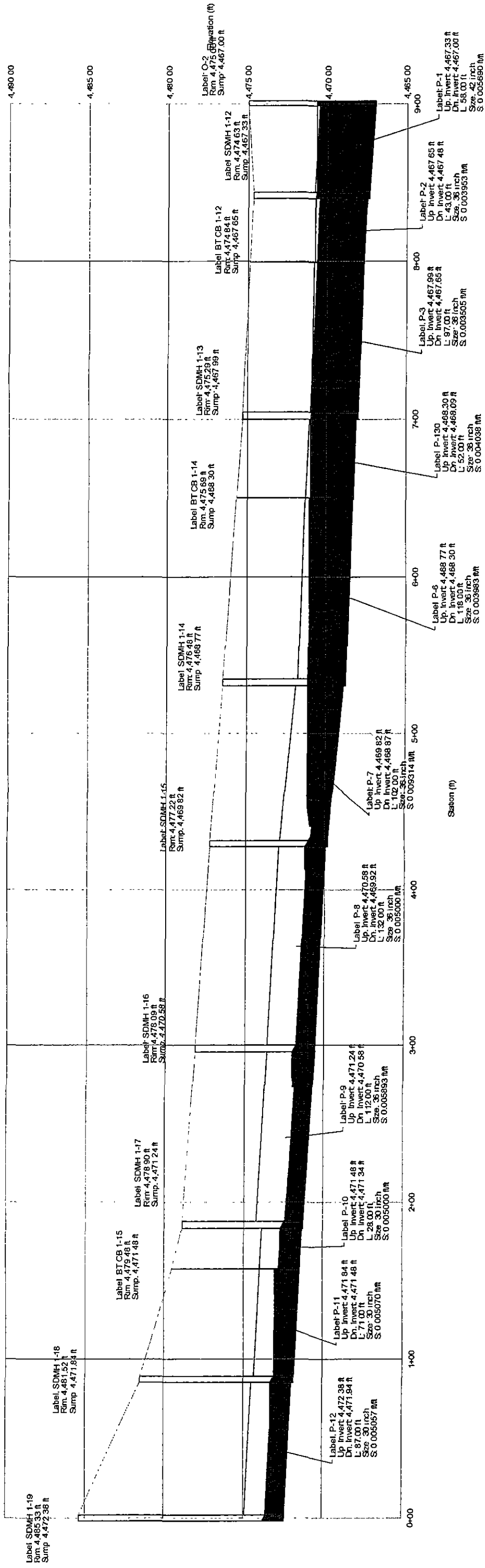
Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER SOUTH - C

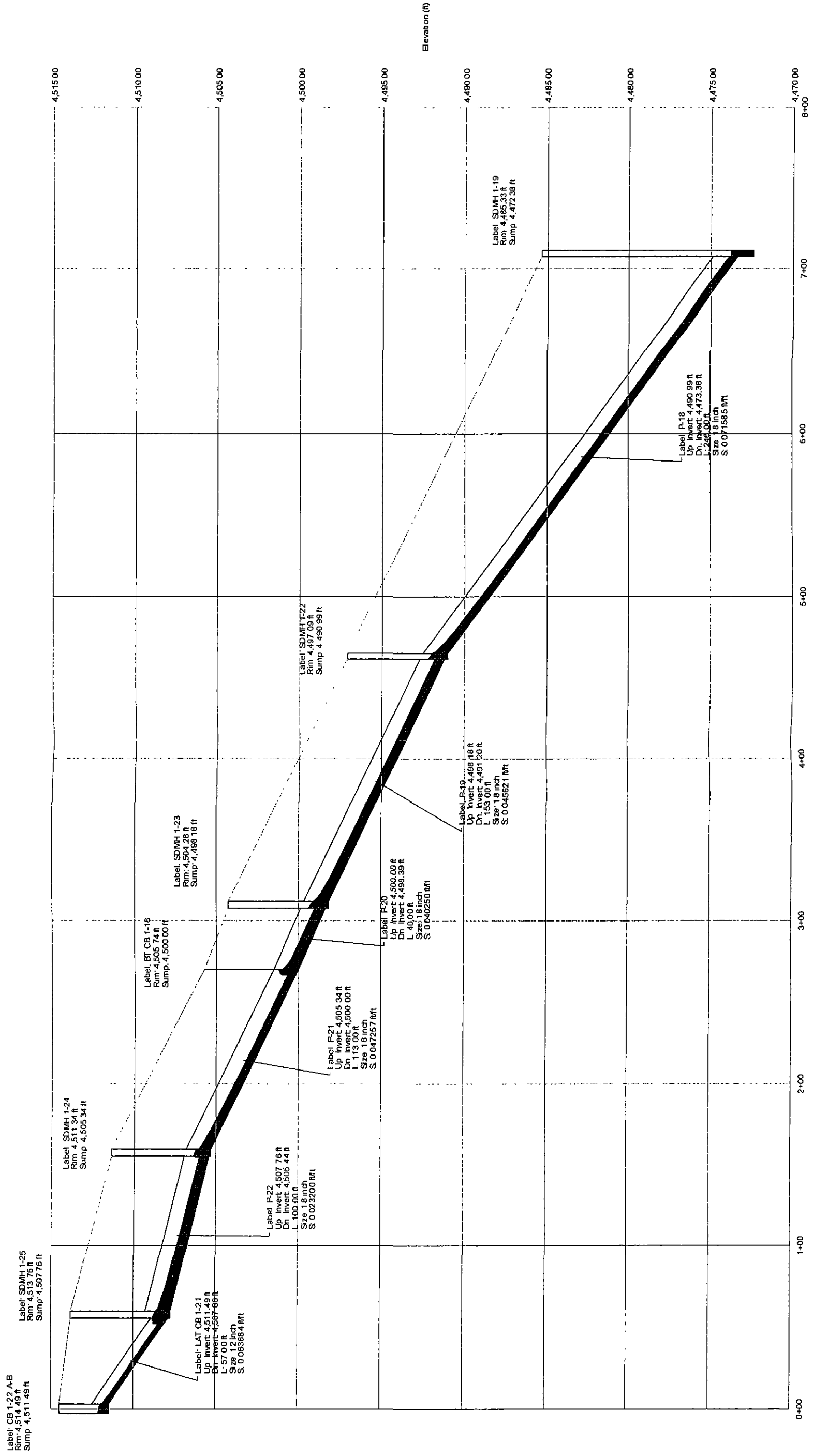
Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER SOUTH - D

Scenario: Base

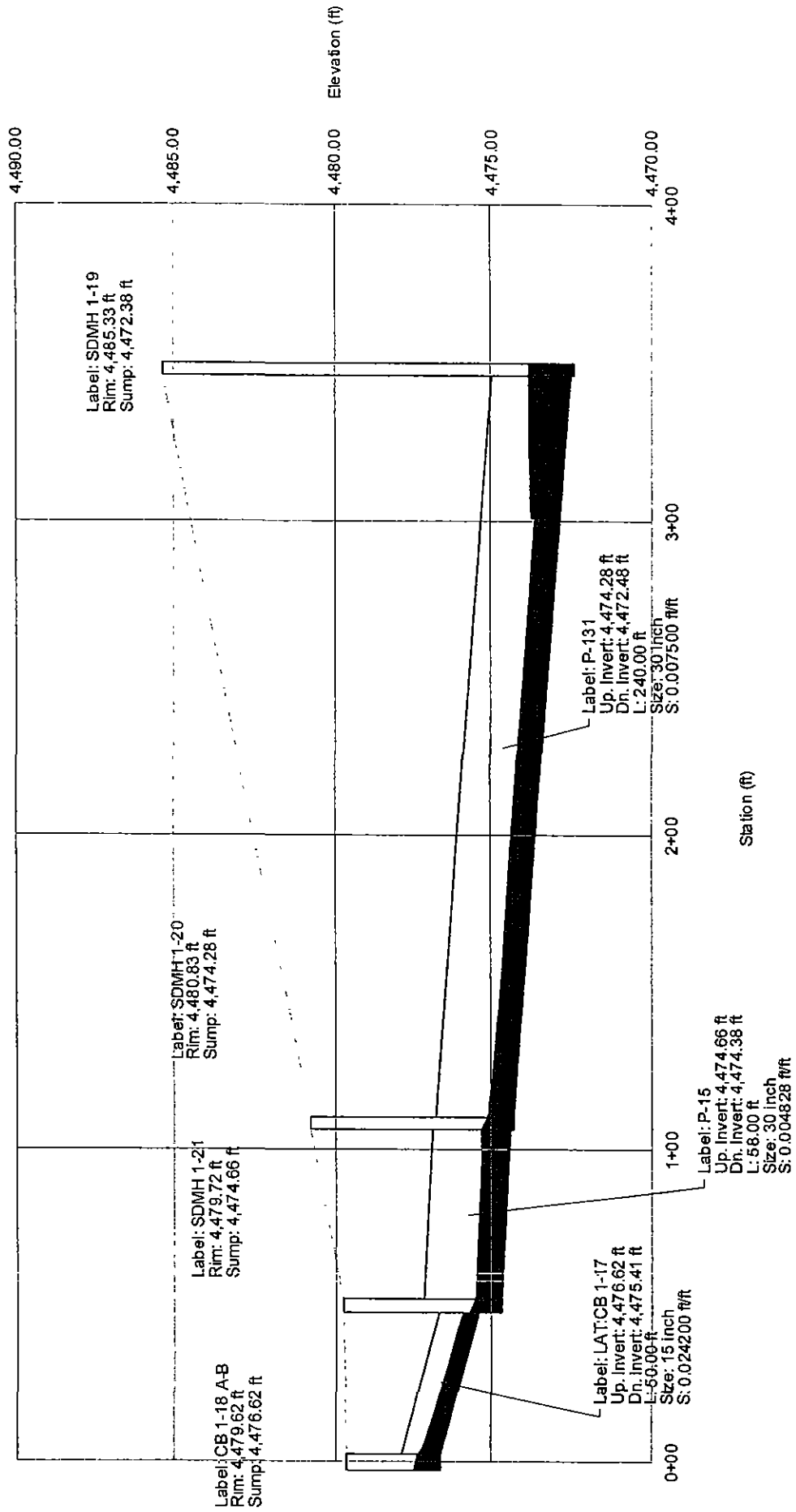




Scenario: Base

Profile: DRY GULCH - A

Scenario: Base

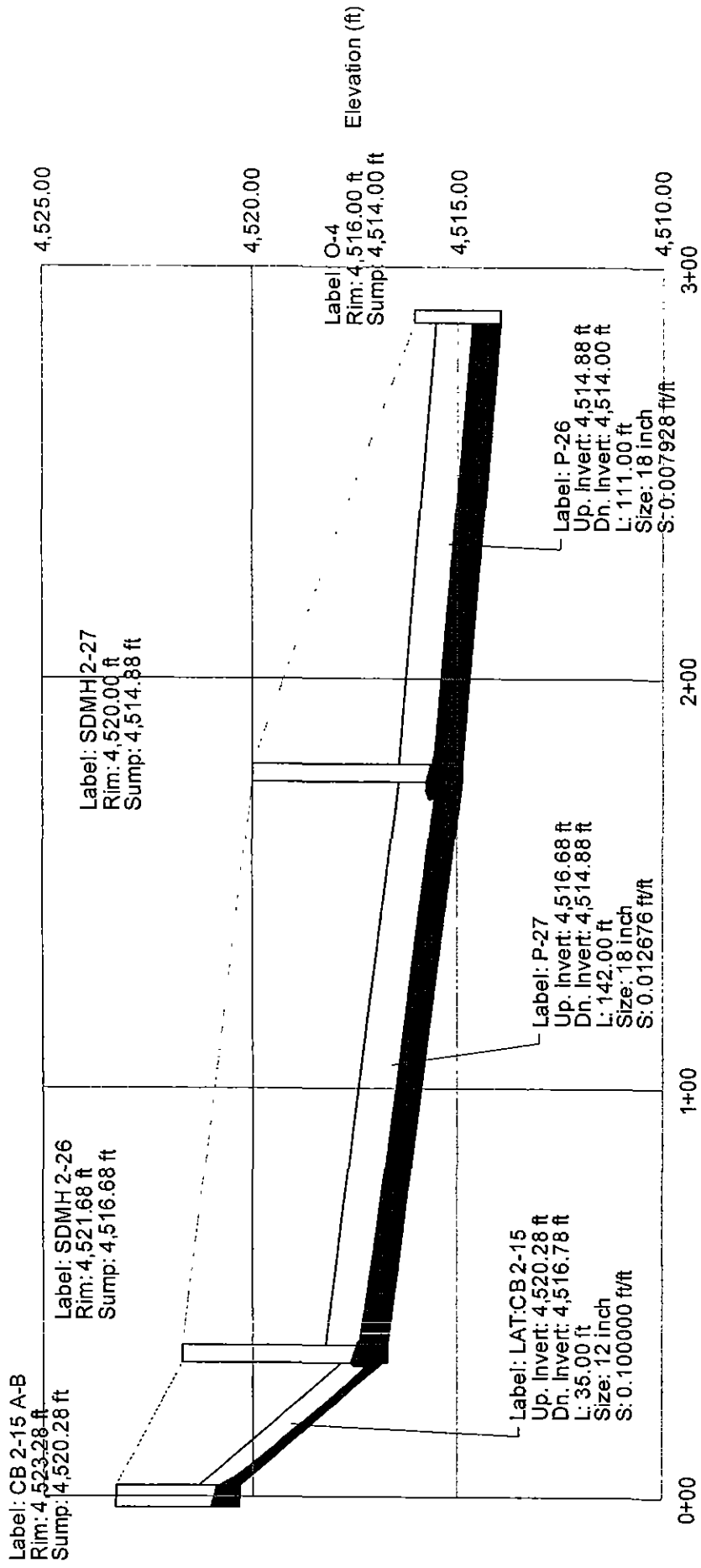




Scenario: Base

Profile: DRY GULCH - B

Scenario: Base



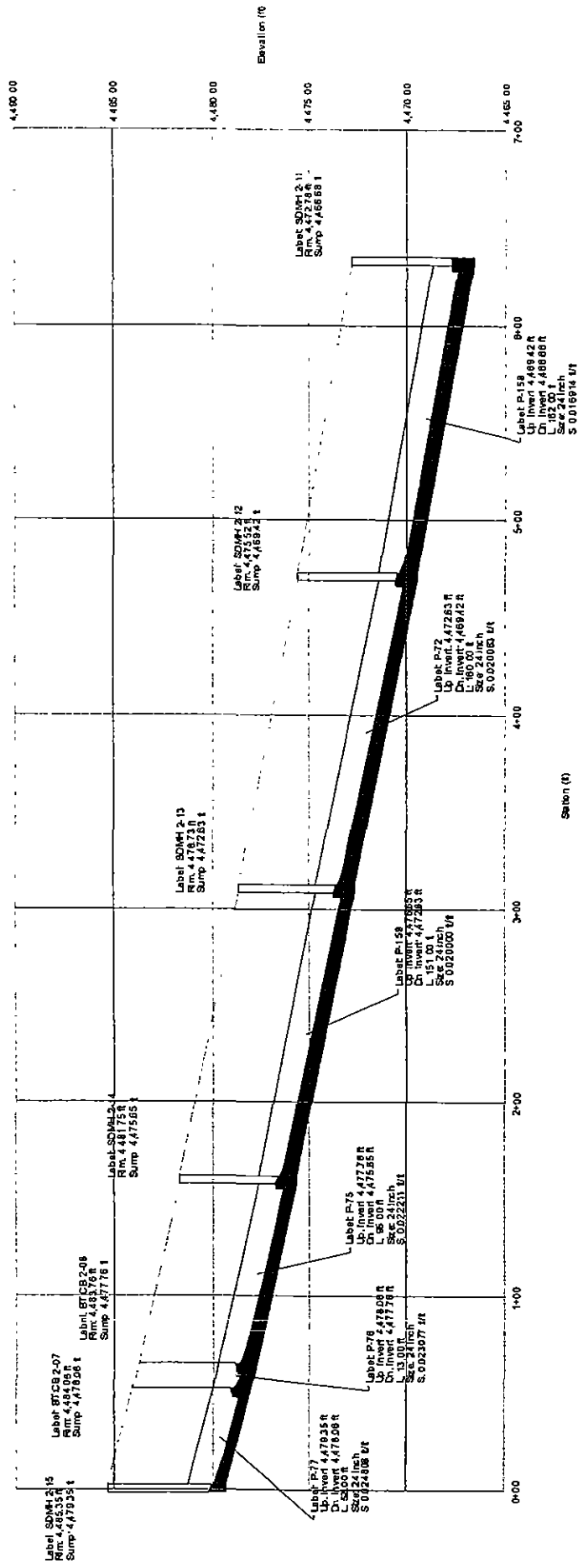
Station (ft)

Profile

Scenario: Base

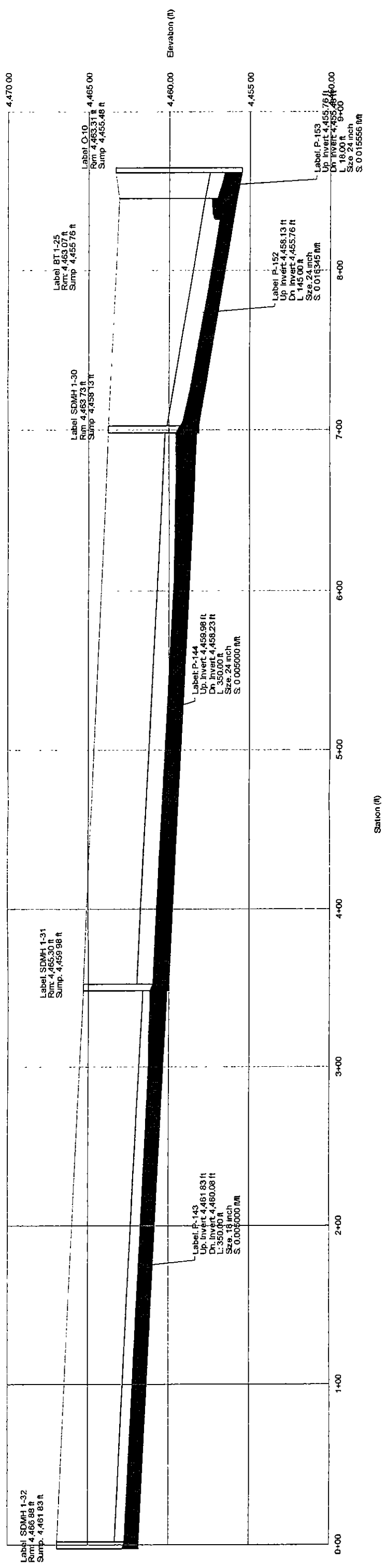
Profile: ORE CIRCLE - A

Scenario: Base



Profile
Scenario: Base

Profile: DESERT WAY
Scenario: Base





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Project: GOLDEN HIGHLANDS
MODIFIED FORM 2

100-YEAR STORM EVENT

Sub-Basin Data	Initial Overland						Channelized Flow						Tc		Tc Urbanized Basin		Final		Region 2		Final intensity		Check Flow		Check Flow	
	R10	Area (ac)	Li (ft)	Slope (%)	Tt (min)	Lt (ft)	Slope (%)	Vel. (fps)	Tt (min)	(Tt+Tb) (min)	Check Total Length	Tc (check)	Min	Tc	INTENSITIES (min)	10	15	(in/hr)	Q=CIA (cfs)	INTERCEPTED Q	STORMCAD BYPASSED Q	STORMCAD BYPASSED Q	Q=CIA (cfs)	INTERCEPTED Q	STORMCAD BYPASSED Q	STORMCAD BYPASSED Q
B1	0.53	3.17	200.00	3.50	9.60	625.00	0.64	1.60	6.51	16.11	825.00	14.58	14.58	3.29	2.72	2.77	2.77	4.65	2.32	2.37	2.37	4.65	2.32	2.37	2.37	CB 1-12
B2	0.53	2.91	142.00	1.65	10.36	717.00	5.00	4.47	2.67	13.04	859.00	14.77	13.04	3.29	2.72	2.94	2.94	4.54	6.98	0	0	4.54	6.98	0	0	
B3	0.53	4.40	151.00	4.90	7.46	800.00	5.00	4.47	2.98	10.44	951.00	15.28	10.44	3.29	2.72	3.24	3.24	7.55	9.81	0	0	7.55	9.81	0	0	
B4	0.53	3.66	166.00	6.10	7.28	736.00	4.70	4.34	2.83	10.11	902.00	15.01	10.11	3.29	2.72	3.28	3.28	6.36	6.41	0	0	6.36	6.41	0	0	
B5	0.53	6.01	166.00	1.94	10.59	799.00	4.09	4.04	3.29	13.88	964.00	15.36	13.88	3.29	2.72	2.85	2.85	9.07	9.14	0	0	9.07	9.14	0	0	
B6	0.53	4.45	124.00	2.10	8.94	577.00	5.10	4.52	2.13	11.07	701.00	13.89	11.07	3.29	2.72	3.17	3.17	7.47	7.53	0	0	7.47	7.53	0	0	
B7	0.53	1.81	216.00	5.50	8.59	179.00	4.03	4.01	0.74	9.33	395.00	12.19	10.00	3.29	2.72	3.29	3.29	3.16	4.97	0	0	3.16	4.97	0	0	
B8	0.53	2.64	134.00	1.98	9.48	825.00	6.78	5.21	2.64	12.12	959.00	15.33	12.12	3.29	2.72	3.05	3.05	4.27	2.64	1.66	1.66	4.27	2.64	1.66	1.66	CB 1-19
B9	0.53	4.88	200.00	6.90	7.67	883.00	6.39	5.06	2.91	10.58	1083.00	16.02	10.58	3.29	2.72	3.22	3.22	8.34	3.84	4.56	4.56	8.34	3.84	4.56	4.56	CB 1-22
B10	0.53	0.35	2.00	2.00	1.15	369.00	0.60	1.55	3.97	5.12	371.00	12.06	10.00	3.29	2.72	3.29	3.29	0.61	5.27	0	0	0.61	5.27	0	0	
B11	0.53	3.23	137.00	1.75	9.98	812.00	5.82	4.82	2.80	12.79	949.00	15.27	12.79	3.29	2.72	2.97	2.97	5.09	3.12	2.01	2.01	5.09	3.12	2.01	2.01	CB 1-15
B12	0.53	3.48	198.00	7.11	7.56	830.00	5.65	4.75	2.91	10.47	1028.00	15.71	10.47	3.29	2.72	3.24	3.24	5.97	3.38	2.64	2.64	5.97	3.38	2.64	2.64	CB 1-14
B13	0.53	0.06	4.00	2.00	1.63	106.00	2.00	2.83	0.62	2.26	110.00	10.61	10.00	3.29	2.72	3.29	3.29	0.10	2.92	0	0	0.10	2.92	0	0	
B14	0.53	0.35	20.00	20.00	1.71	269.00	0.54	1.47	3.05	4.76	289.00	11.61	10.00	3.29	2.72	3.29	3.29	0.61	2.94	0	0	0.61	2.94	0	0	
B15	0.53	2.59	66.00	1.30	7.64	1300.00	3.89	3.94	5.49	13.14	1366.00	17.59	13.14	3.29	2.72	2.93	2.93	4.03	2.41	2.07	2.07	4.03	2.41	2.07	2.07	CB 1-11
B16	0.53	3.14	156.00	9.20	6.16	372.00	5.07	4.50	1.38	7.54	528.00	12.93	10.00	3.29	2.72	3.29	3.29	5.48	5.52	0	0	5.48	5.52	0	0	
B17	0.53	1.45	77.00	1.16	8.57	642.00	7.41	5.44	1.97	10.54	719.00	13.99	10.54	3.29	2.72	3.23	3.23	2.48	2.04	0.46	0.46	2.48	2.04	0.46	0.46	CB 1-10
B18	0.53	0.17	4.00	2.00	1.63	280.00	7.96	5.64	0.83	2.46	284.00	11.58	10.00	3.29	2.72	3.29	3.29	0.30	0.3	0	0	0.30	0.3	0	0	
B19	0.53	3.42	77.00	1.17	8.55	852.00	1.24	2.23	6.38	14.92	929.00	15.16	14.92	3.29	2.72	2.73	2.73	4.95	7.26	0	0	4.95	7.26	0	0	
B20	0.53	4.59	124.00	1.13	10.97	936.00	1.26	2.24	6.95	17.92	1060.00	15.89	15.89	3.29	2.72	2.62	2.62	6.37	6.54	0	0	6.37	6.54	0	0	
B21	0.53	2.99	116.00	1.06	10.84	543.00	1.63	2.55	3.54	14.38	659.00	13.66	13.66	3.29	2.72	2.87	2.87	4.55	4.59	0	0	4.55	4.59	0	0	
B22	0.53	2.90	148.00	1.41	11.14	723.00	2.12	2.91	4.14	15.28	871.00	14.84	14.84	3.29	2.72	2.74	2.74	4.21	6.68	0	0	4.21	6.68	0	0	
B23	0.53	2.87	151.00	1.78	10.42	657.00	2.16	2.94	3.73	14.15	808.00	14.49	14.15	3.29	2.72	2.82	2.82	4.29	9.42	0	0	4.29	9.42	0	0	
B24	0.53	2.01	152.00	2.79	9.02	560.00	2.53	3.18	2.93	11.95	712.00	13.96	11.95	3.29	2.72	3.07	3.07	3.27	2.81	2.58	2.58	3.27	2.81	2.58	2.58	CB 1-08
B25	0.53	3.42	227.00	7.36	8.00	738.00	2.36	3.07	4.00	12.00	985.00	15.36	12.00	3.29	2.72	3.10	3.10	5.55	2.87	2.72	2.72	5.55	2.87	2.72	2.72	CB 1-07
B26	0.53	5.74	225.00	10.75	7.03	917.00	2.67	3.27	4.68	11.71	1142.00	16.34	11.71	3.29	2.72	3.10	3.10	9.42	9.49	0	0	9.42	9.49	0	0	
B27	0.53	2.96	119.00	1.05	11.01	830.00	2.75	3.32	4.17	15.18	949.00	15.27	15.18	3.29	2.72	2.70	2.70	4.23	2.44	1.85	1.85	4.23	2.44	1.85	1.85	CB 2-08
B28	0.53	1.49	62.00	1.10	7.83	728.00	2.25	3.00	4.04	11.87	790.00	14.39	11.87	3.29	2.72	3.08	3.08	2.43	2.7	2.56	2.56	2.43	2.7	2.56	2.56	CB 1-04
B29	0.53	1.40	163.00	1.42	11.30	199.00	1.00	2.00	1.66	12.96	352.00	11.96	11.96	3.29	2.72	3.07	3.07	2.28	6.47	0	0	2.28	6.47	0	0	
B30	0.53	3.72	247.00	2.02	12.79	958.00	2.97	3.45	4.63	17.42	1205.00	16.69	16.69	3.29	2.72	2.53	2.53	4.98	2.81	2.4	2.4	4.98	2.81	2.4	2.4	CB 1-02
B31	0.53	2.80	145.00	1.94	9.93	839.00	3.08	3.51	3.98	13.91	984.00	15.47	13.91	3.29	2.72	2.84	2.84	4.22	2.85	2.49	2.49	4.22	2.85	2.49	2.49	CB 1-01
B32	0.53	0.07	107.00	1.11	10.25	300.00	1.32	2.30	2.18	12.43	407.00	12.26	12.26	3.29	2.72	3.03	3.03	0.11	1.8	1.16	1.16	0.11	1.8	1.16	1.16	CB 2-02
B33	0.53	1.47	192.00	3.10	9.79	307.00	1.32	2.30	2.23	12.01	499.00	12.77	12.01	3.29	2.72	3.06	3.06	2.38	5.93	0	0	2.38	5.93	0	0	
B34	0.53	3.60	255.00	4.60	9.90	891.00	1.98	2.81	5.28	15.18	1146.00	16.37	15.18	3.29	2.72	2.70	2.70	5.15	2.59	2.62	2.62	5.15	2.59	2.62	2.62	CB 1-08
B35	0.53	5.12	110.00	1.00	10.76	2435.00	2.42	10.17	3.99	14.75	2545.00	24.14	14.75	3.29	2.72	2.75	2.75	7.46	0	0	0	7.46	0	0	0	to channel
B36	0.53	1.71	76.00	1.17	8.49	780.00	1.21	2.20	5.91	14.40	856.00	14.76	14.40	3.29	2.72	2.79	2.79	2.53	2.55	0	0	2.53	2.55	0	0	
B37	0.53	2.24	147.00	1.00	12.44	581.00	1.20	2.19	4.42	16.86	728.00	14.04	14.04	3.29	2.72	2.83	2.83	3.36	3.39	0	0	3.36	3.39	0	0	
B38	0.53	2.29	107.00	1.07	10.38	620.00	2.30	3.03	3.41	13.79	727.00	14.04	13.79	3.29	2.72	2.86	2.86	3.47	2.11	1.39	1.39	3.47	2.11	1.39	1.39	CB 1-01
B39	0.53	5.16	310.00	8.24	9.01	985.00	2.64	3.25	5.05	14.06	1295.00	17.19	14.06	3.29	2.72	2.83	2.83	7.73	4.54	3.25	3.25	7.73	4.54	3.25	3.25	CB 2-04
B40	0.53	3.51	118.00	1.40	9.97	1030.00	2.64	3.25	5.28	15.26	1148.00	16.38	15.26	3.29	2.72	2.69	2.69	5.01	2.53	2.54	2.54	5.01	2.53	2.54	2.54	CB 2-03
B41	0.53	1.67	726.00	2.04	21.85	147.00	0.50	1.41	1.73	23.58	873.00	14.85	14.85	3.29	2.72	2.74	2.74	2.42	7.36	0	0	2.42	7.36	0	0	
B42	0.53	5.94	687.00	2.04	21.25	350.00	0.50	1.41	4.12	25.38	1037.00	15.76	15.76	3.29	2.72	2.63	2.63	8.29	7.14	4.83	4.83	8.29	7.14	4.83	4.83	CB 1-25
B43	0.53	6.56	647.00	2.04	20.63	350.00	0.50	1.41	4.12	24.75	997.00	15.54	15.54	3.29	2.72	2.66	2.66	9.24	5.92	3.5	3.5	9.24	5.92	3.5	3.5	CB 1-26
B44	0.53	10.55	145.00	1.00	12.35	1950.00	5.64	4.75	6.84	19.20	2095.00	21.64	19.20	3.29	2.72	2.24	2.24	12.53	0	0	0	12.53	0	0	0	to channel
B45	0.53	4.33	131.00	1.00	11.74	1050.00	1.14	2.14	8.20	19.94	1181.00	16.56	16.56	3.29	2.72	2.54	2.54	5.83	0	0	0	5.83	0	0	0	to channel

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Inlet Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Manning's n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
P-163	SDMH 2-2	SDMH 2-20	N/A	5.35	156.00	0.016889	15 inch	0.014	7.79	4,473.60	4,470.97	4,479.70	4,477.07	4,474.54	4,472.13
P-162	SDMH 2-24	SDMH 2-24	N/A	0.30	351.00	0.078205	12 inch	0.014	9.25	4,548.59	4,521.14	4,554.59	4,527.24	4,548.81	4,521.83
P-161	SDMH 2-18	SDMH 2-18	N/A	10.73	119.00	0.021765	18 inch	0.014	14.39	4,492.49	4,489.90	4,498.59	4,496.00	4,493.75	4,491.51
P-160	SDMH 2-17	SDMH 2-16	N/A	10.63	215.00	0.023674	18 inch	0.014	15.01	4,487.44	4,482.35	4,493.54	4,488.45	4,488.69	4,483.95
P-159	SDMH 2-14	SDMH 2-13	N/A	15.28	151.00	0.020000	24 inch	0.014	29.71	4,475.65	4,472.63	4,481.75	4,478.73	4,477.06	4,474.36
P-158	SDMH 2-11	SDMH 2-11	N/A	15.09	162.00	0.016914	24 inch	0.014	27.32	4,469.42	4,466.68	4,475.52	4,472.78	4,470.82	4,468.39
P-156	CB 1-27 A	SDMH 1-31	0.53	5.92	22.00	0.095455	12 inch	0.014	10.22	4,462.18	4,460.08	4,465.18	4,465.30	4,463.13	4,461.42
P-155	SDMH 2-06	BT: 2-03	N/A	11.86	8.00	0.028750	18 inch	0.014	16.54	4,511.21	4,510.98	4,517.31	4,517.22	4,512.52	4,512.35
P-154	BT: 2-03	SDMH 2-07	N/A	13.43	88.00	0.028088	18 inch	0.014	16.34	4,510.98	4,508.51	4,517.22	4,514.61	4,512.35	4,510.36
P-153	BT 1-25	O-10	N/A	24.18	18.00	0.015556	24 inch	0.014	26.20	4,455.76	4,455.48	4,463.07	4,463.31	4,457.50	4,457.07
P-152	SDMH 1-30	BT 1-25	N/A	17.26	145.00	0.016345	24 inch	0.014	26.85	4,468.13	4,455.76	4,463.73	4,463.07	4,459.63	4,458.04
P-151	CB 1-23	BT 1-23	0.53	3.39	61.00	0.067705	12 inch	0.014	8.61	4,460.95	4,456.82	4,463.95	4,460.00	4,461.74	4,458.21
P-150	SDMH 2-01	SDMH 2-06	N/A	13.39	100.00	0.037000	18 inch	0.014	18.76	4,508.51	4,504.81	4,514.61	4,510.91	4,509.87	4,506.66
P-149	BT 1-24	BT 1-23	N/A	2.54	41.00	0.005122	12 inch	0.014	2.37	4,457.03	4,456.82	4,460.00	4,460.00	4,458.45	4,458.21
P-148	SDMH 2-01	SDMH 2-04	N/A	13.30	336.00	0.030030	18 inch	0.014	16.90	4,501.10	4,491.01	4,507.20	4,497.11	4,502.46	4,492.84
P-147	BT 1-23	O-9	N/A	5.81	28.00	0.076429	12 inch	0.014	9.15	4,456.82	4,454.68	4,460.00	4,460.26	4,457.77	4,455.30
P-146	SDMH 2-01	BT:CB 2-04	N/A	13.06	185.00	0.025081	24 inch	0.014	33.27	4,488.10	4,483.46	4,494.20	4,489.46	4,489.40	4,485.21
P-145	SDMH 2-01	SDMH 2-01	N/A	18.25	153.00	0.028758	24 inch	0.014	35.62	4,492.59	4,478.19	4,488.69	4,484.29	4,484.13	4,480.11
P-144	SDMH 1-31	SDMH 1-30	N/A	10.42	350.00	0.005000	24 inch	0.014	14.85	4,459.98	4,458.23	4,465.30	4,463.73	4,461.21	4,459.99
P-143	SDMH 1-31	SDMH 1-31	N/A	4.50	350.00	0.005000	18 inch	0.014	6.90	4,461.83	4,460.08	4,466.88	4,465.30	4,462.71	4,461.42
P-142	I-43	SDMH 1-32	0.00	4.50	116.00	0.027328	12 inch	0.010	7.86	4,465.00	4,461.83	4,468.00	4,466.88	4,465.89	4,462.85
P-140	BT 2-04	SDMH 2-06	N/A	11.89	55.00	0.018000	15 inch	0.014	8.05	4,512.20	4,511.21	4,518.20	4,517.31	4,515.09	4,512.93
P-139	SDMH 2-04	BT 2-04	N/A	6.77	54.00	0.009444	15 inch	0.014	5.83	4,512.71	4,512.20	4,518.81	4,518.20	4,516.51	4,515.82
P-138	SDMH 2-10	SDMH 2-09	N/A	6.87	210.00	0.013762	15 inch	0.014	7.04	4,515.60	4,512.71	4,521.60	4,518.81	4,519.26	4,516.51
P-135	BT:CB 1-3	SDMH 1-28	N/A	19.69	144.00	0.018681	24 inch	0.014	28.71	4,469.06	4,466.37	4,475.00	4,472.37	4,470.65	4,468.68
P-134	SDMH 1-28	BT:CB 1-3	N/A	17.94	121.00	0.017190	24 inch	0.014	27.54	4,471.14	4,469.06	4,477.24	4,475.00	4,472.67	4,470.65
P-133	SDMH 1-06	SDMH 1-06	N/A	41.40	79.00	0.006835	36 inch	0.014	51.20	4,454.38	4,453.84	4,462.48	4,462.08	4,461.19	4,460.84
P-132	CB 1-05 A	SDMH 1-06	0.53	6.54	21.00	0.071429	12 inch	0.014	8.84	4,459.24	4,457.74	4,462.24	4,462.08	4,461.66	4,460.84
P-131	SDMH 1-20	SDMH 1-19	N/A	15.64	240.00	0.007500	30 inch	0.014	32.98	4,474.28	4,472.48	4,480.83	4,485.33	4,477.45	4,477.05
P-130	BT:CB 1-11	SDMH 1-13	N/A	40.27	52.00	0.004038	36 inch	0.014	39.36	4,468.30	4,468.09	4,475.69	4,475.29	4,472.73	4,472.51
P-129	SDMH 2-11	BT:CB 1-06	N/A	14.99	152.00	0.022763	24 inch	0.014	31.59	4,466.68	4,463.22	4,472.78	4,469.00	4,468.08	4,467.11
P-127	BT:CB 1-01	SDMH 1-27	N/A	26.98	267.00	0.040974	24 inch	0.014	42.52	4,465.35	4,454.41	4,471.84	4,466.78	4,467.16	4,457.59
P-125	BT 1-06	SDMH 1-06	N/A	41.83	155.00	0.007935	36 inch	0.014	55.17	4,455.71	4,454.48	4,464.00	4,462.48	4,462.16	4,461.45
P-124	SDMH 1-01	SDMH 1-01	N/A	53.19	60.00	0.002000	36 inch	0.014	27.70	4,453.00	4,452.88	4,464.02	4,464.54	4,457.41	4,456.97
P-123	SDMH 1-01	O-5	N/A	78.51	391.00	0.001995	48 inch	0.014	59.57	4,452.78	4,452.00	4,464.54	4,456.00	4,456.66	4,455.27

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Inlet Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Mannings n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
P-118	SDMH 2-08	SDMH 2-09	N/A	13.35	100.00	0.035300	18 inch	0.014	18.33	4,504.81	4,501.28	4,510.91	4,507.20	4,506.17	4,502.95
P-115	SDMH 2-04	SDMH 2-05	N/A	13.14	144.00	0.018194	18 inch	0.014	13.16	4,491.01	4,488.39	4,497.11	4,494.20	4,492.37	4,489.62
P-111	BT-CB 2-01	SDMH 2-02	N/A	15.53	29.00	0.030000	24 inch	0.014	36.38	4,463.46	4,482.59	4,489.46	4,488.69	4,484.88	4,484.51
P-107	SDMH 2-01	SDMH 1-29	N/A	18.16	313.00	0.022204	24 inch	0.014	31.30	4,478.19	4,471.24	4,484.29	4,477.24	4,479.72	4,473.04
P-103	SDMH 1-20	BT-CB 1-02	N/A	19.58	6.00	0.044333	24 inch	0.014	44.23	4,466.27	4,466.00	4,472.37	4,472.14	4,468.38	4,468.33
P-102	BT-CB 1-01	BT-CB 1-01	N/A	21.75	16.00	0.040875	24 inch	0.014	42.47	4,466.00	4,465.35	4,472.14	4,471.84	4,467.95	4,467.79
P-99	SDMH 1-21	SDMH 1-26	N/A	26.78	142.00	0.001972	36 inch	0.014	27.50	4,453.41	4,453.13	4,466.78	4,465.25	4,457.48	4,457.22
P-98	SDMH 1-20	SDMH 1-01	N/A	26.38	77.00	0.001948	36 inch	0.014	27.33	4,453.03	4,452.88	4,465.25	4,464.54	4,457.11	4,456.97
P-95	SDMH 1-01	SDMH 1-02	N/A	53.41	76.00	0.001974	36 inch	0.014	27.51	4,453.25	4,453.10	4,463.33	4,464.02	4,458.42	4,457.85
P-94	SDMH 1-04	SDMH 1-03	N/A	53.60	65.00	0.002000	36 inch	0.014	27.70	4,453.48	4,453.35	4,462.74	4,463.33	4,459.35	4,458.86
P-93	SDMH 1-03	SDMH 1-04	N/A	53.82	78.00	0.002051	36 inch	0.014	28.05	4,453.74	4,453.58	4,462.08	4,462.74	4,460.38	4,459.80
P-83	SDMH 2-18	SDMH 2-17	N/A	10.68	108.00	0.022778	18 inch	0.014	14.72	4,489.90	4,487.44	4,496.00	4,493.54	4,491.15	4,489.05
P-78	SDMH 2-16	SDMH 2-15	N/A	10.54	128.00	0.022500	18 inch	0.014	14.63	4,482.35	4,479.47	4,488.45	4,485.35	4,483.60	4,480.75
P-77	SDMH 2-14	BT-CB 2-07	N/A	10.48	52.00	0.024808	24 inch	0.014	33.08	4,479.35	4,478.06	4,485.35	4,484.06	4,480.51	4,479.64
P-76	BT-CB 2-01	BT-CB 2-08	N/A	12.93	13.00	0.023077	24 inch	0.014	31.91	4,478.06	4,477.76	4,483.76	4,483.76	4,479.35	4,479.50
P-75	BT-CB 2-08	SDMH 2-14	N/A	15.34	95.00	0.022211	24 inch	0.014	31.30	4,477.76	4,475.65	4,483.76	4,481.75	4,479.17	4,477.38
P-72	SDMH 2-13	SDMH 2-12	N/A	15.19	160.00	0.020063	24 inch	0.014	29.75	4,472.63	4,469.42	4,478.73	4,475.52	4,474.04	4,471.14
P-67	BT-CB 1-06	SDMH 1-09	N/A	29.71	34.00	0.000588	24 inch	0.014	5.09	4,463.22	4,463.20	4,469.00	4,468.80	4,466.42	4,465.74
P-66	SDMH 1-10	BT-CB 1-08	N/A	7.29	33.00	0.010909	18 inch	0.014	10.19	4,467.15	4,466.79	4,473.25	4,473.00	4,468.75	4,468.57
P-65	BT-CB 1-08	SDMH 1-09	N/A	9.36	284.00	0.010880	18 inch	0.014	10.17	4,466.79	4,463.70	4,473.00	4,468.80	4,468.35	4,465.74
P-64	SDMH 1-09	SDMH 1-08	N/A	38.50	189.00	0.029947	30 inch	0.014	65.91	4,462.70	4,457.04	4,468.80	4,466.14	4,465.26	4,463.33
P-63	SDMH 1-08	SDMH 1-07	N/A	38.14	63.00	0.003651	36 inch	0.014	37.42	4,456.54	4,456.31	4,466.14	4,465.31	4,463.10	4,462.86
P-62	SDMH 1-07	BT 1-06	N/A	37.97	54.00	0.009259	36 inch	0.014	59.59	4,456.21	4,455.71	4,465.31	4,464.00	4,462.64	4,462.43
P-49	SDMH 2-24	BT 2-10	N/A	0.29	27.00	0.008519	12 inch	0.014	3.05	4,521.14	4,520.91	4,527.24	4,526.00	4,521.83	4,521.83
P-48	BT 2-10	O-3	N/A	2.26	202.00	0.004505	12 inch	0.014	2.22	4,520.91	4,520.00	4,526.00	4,522.00	4,521.75	4,520.64
P-45	SDMH 2-21	SDMH 2-22	N/A	5.51	186.00	0.025161	15 inch	0.014	9.51	4,480.95	4,476.27	4,487.05	4,482.15	4,481.90	4,477.23
P-44	SDMH 2-21	SDMH 2-21	N/A	5.43	144.00	0.011528	15 inch	0.014	6.44	4,476.05	4,474.39	4,482.15	4,479.70	4,476.99	4,475.27
P-41	SDMH 2-20	BT-CB 1-09	N/A	5.28	160.00	0.016750	15 inch	0.014	7.76	4,470.97	4,468.29	4,477.07	4,474.29	4,471.90	4,469.70
P-40	BT-CB 1-09	SDMH 1-10	N/A	7.31	38.00	0.027368	15 inch	0.014	9.92	4,468.29	4,467.25	4,474.29	4,473.25	4,469.37	4,468.88
P-38	SDMH 1-11	BT-CB 1-11	N/A	2.93	29.00	0.010690	12 inch	0.014	3.42	4,467.91	4,467.60	4,474.01	4,473.00	4,472.63	4,472.40
P-37	BT-CB 1-11	O-1	N/A	5.82	42.00	0.011905	12 inch	0.014	3.61	4,467.60	4,467.10	4,473.00	4,475.00	4,471.98	4,470.68
P-27	SDMH 2-28	SDMH 2-27	N/A	6.21	142.00	0.012876	18 inch	0.014	10.98	4,516.68	4,514.88	4,521.68	4,520.00	4,517.64	4,516.04
P-26	SDMH 2-27	O-4	N/A	6.12	111.00	0.007928	18 inch	0.014	6.68	4,514.88	4,514.00	4,520.00	4,516.00	4,515.84	4,514.93
P-22	SDMH 1-23	SDMH 1-24	N/A	11.14	100.00	0.023200	18 inch	0.014	14.86	4,507.76	4,505.44	4,513.76	4,511.34	4,509.04	4,506.99
P-21	SDMH 1-24	BT-CB 1-18	N/A	11.06	113.00	0.047257	18 inch	0.014	21.20	4,505.34	4,500.00	4,511.34	4,505.74	4,506.61	4,502.04

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Inlet Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Manning's n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
P-20	BT:CB 1-18	SDMH 1-23	N/A	15.54	40.00	0.040250	18 inch	0.014	19.57	4,500.00	4,498.39	4,505.74	4,504.28	4,501.42	4,500.22
P-19	SDMH 1-22	SDMH 1-22	N/A	15.51	153.00	0.045621	18 inch	0.014	20.83	4,498.18	4,491.20	4,504.28	4,497.09	4,499.60	4,493.02
P-18	SDMH 1-22	SDMH 1-19	N/A	15.39	246.00	0.071585	18 inch	0.014	26.10	4,490.99	4,473.38	4,497.09	4,485.33	4,492.40	4,477.05
P-15	SDMH 1-22	SDMH 1-20	N/A	15.83	58.00	0.004828	30 inch	0.014	26.46	4,474.66	4,474.38	4,479.72	4,480.83	4,477.63	4,477.53
P-12	SDMH 1-18	SDMH 1-18	N/A	28.91	87.00	0.005057	30 inch	0.014	27.08	4,472.38	4,471.94	4,485.33	4,481.52	4,476.78	4,476.28
P-11	SDMH 1-18	BT:CB 1-15	N/A	28.75	71.00	0.005070	30 inch	0.014	27.12	4,471.84	4,471.48	4,481.52	4,479.48	4,476.01	4,475.61
P-10	BT:CB 1-18	SDMH 1-17	N/A	33.82	28.00	0.005000	30 inch	0.014	26.93	4,471.48	4,471.34	4,479.48	4,478.90	4,475.24	4,475.02
P-9	SDMH 1-17	SDMH 1-16	N/A	33.77	112.00	0.005893	36 inch	0.014	47.54	4,471.24	4,470.58	4,478.90	4,478.09	4,474.84	4,474.51
P-8	SDMH 1-16	SDMH 1-16	N/A	33.47	132.00	0.005000	36 inch	0.014	43.78	4,470.58	4,469.92	4,478.09	4,477.22	4,474.33	4,473.95
P-7	SDMH 1-16	SDMH 1-14	N/A	33.12	102.00	0.009314	36 inch	0.014	59.77	4,469.82	4,468.87	4,477.22	4,476.48	4,473.78	4,473.49
P-6	SDMH 1-16	BT:CB 1-14	N/A	32.85	118.00	0.003983	36 inch	0.014	39.09	4,468.77	4,468.30	4,476.48	4,475.69	4,473.32	4,472.99
P-3	SDMH 1-16	BT:CB 1-12	N/A	46.17	97.00	0.003505	36 inch	0.014	36.67	4,467.99	4,467.55	4,475.29	4,474.84	4,472.18	4,471.64
P-2	BT:CB 1-16	SDMH 1-12	N/A	48.03	43.00	0.003953	36 inch	0.014	38.94	4,467.65	4,467.48	4,474.84	4,474.63	4,471.28	4,471.03
P-1	SDMH 1-16	O-2	N/A	47.92	58.00	0.005690	42 inch	0.014	70.47	4,467.33	4,467.00	4,474.63	4,475.00	4,470.83	4,470.68
LAT:I-35	DITCH 2-1	O-8	0.00	0.00	57.00	0.020000	12 inch	0.014	4.68	4,530.00	4,528.86	4,533.00	4,531.86	4,530.00	4,528.86
LAT:CB 2-15	CB 2-15 A	SDMH 2-26	0.53	3.12	35.00	0.100000	12 inch	0.014	10.46	4,520.28	4,516.78	4,523.28	4,521.68	4,521.04	4,517.85
LAT:CB 2-14	CB 2-14 A	SDMH 2-26	0.53	3.38	26.00	0.145385	12 inch	0.014	12.61	4,520.56	4,516.78	4,523.28	4,521.68	4,521.35	4,517.85
LAT:CB 2-13	CB 2-13	SDMH 2-25	0.53	0.30	40.00	0.065750	12 inch	0.014	8.48	4,551.22	4,548.59	4,554.22	4,554.59	4,551.44	4,548.85
LAT:CB 2-12	CB 2-12	BT 2-10	0.53	2.04	25.00	0.161200	12 inch	0.014	13.28	4,525.94	4,521.91	4,528.94	4,526.00	4,526.55	4,522.18
LAT:CB 2-10	CB 2-10 A	SDMH 2-19	0.53	9.49	31.00	0.135484	12 inch	0.014	12.18	4,496.69	4,492.49	4,499.69	4,498.59	4,497.68	4,494.10
LAT:CB 2-09	CB 2-09	SDMH 2-19	0.53	2.44	49.00	0.088367	12 inch	0.014	9.83	4,496.82	4,492.49	4,499.82	4,498.59	4,497.49	4,494.10
LAT:CB 2-08	CB 2-08 A	BT:CB 2-08	0.53	2.81	24.00	0.112917	12 inch	0.014	11.12	4,480.97	4,478.26	4,483.97	4,483.76	4,481.69	4,479.50
LAT:CB 2-07	CB 2-07 A	BT:CB 2-07	0.53	2.87	7.00	0.384286	12 inch	0.014	20.51	4,481.25	4,478.56	4,484.25	4,484.06	4,481.98	4,479.64
LAT:CB 1-21	CB 1-22 A	SDMH 1-25	0.53	5.27	57.00	0.063684	12 inch	0.014	8.35	4,511.49	4,507.86	4,514.49	4,513.76	4,512.42	4,509.41
LAT:CB 1-20	CB 1-21 A	SDMH 1-25	0.53	3.84	40.00	0.096000	12 inch	0.014	10.25	4,511.70	4,507.86	4,514.70	4,513.76	4,512.53	4,509.41
LAT:CB 1-19	CB 1-20	SDMH 1-25	0.53	2.64	33.00	0.123030	12 inch	0.014	11.60	4,511.92	4,507.86	4,514.92	4,513.76	4,512.62	4,509.41
LAT:CB 1-18	CB 1-19 A	BT:CB 1-18	0.53	4.97	36.00	0.086111	12 inch	0.014	9.71	4,503.60	4,500.50	4,506.60	4,505.74	4,504.52	4,502.04
LAT:CB 1-17	CB 1-18 A	SDMH 1-21	0.53	7.53	50.00	0.024200	15 inch	0.014	9.33	4,476.62	4,475.41	4,479.62	4,479.72	4,478.50	4,477.71
LAT:CB 1-16	CB 1-17 A	SDMH 1-21	0.53	9.14	58.00	0.020862	15 inch	0.014	8.66	4,476.62	4,475.41	4,479.62	4,479.72	4,479.06	4,477.71
LAT:CB 1-15	CB 1-16	BT:CB 1-15	0.53	6.41	5.00	0.732000	12 inch	0.014	28.30	4,476.64	4,472.98	4,479.64	4,479.48	4,477.61	4,475.61
LAT:CB 1-14	CB 1-15 A	BT:CB 1-14	0.53	9.81	7.00	0.397143	12 inch	0.014	20.85	4,472.97	4,470.19	4,475.97	4,475.69	4,473.96	4,472.99
LAT:CB 1-13	CB 1-14	SDMH 1-13	0.53	6.98	26.00	0.135000	12 inch	0.014	12.15	4,473.50	4,469.99	4,476.50	4,475.29	4,474.47	4,472.51
LAT:CB 1-12	CB 1-13	BT:CB 1-12	0.53	2.32	27.00	0.128148	12 inch	0.014	11.84	4,472.06	4,468.60	4,475.06	4,474.84	4,472.71	4,471.64
LAT:CB 1-11	CB 1-12	BT:CB 1-11	0.53	2.92	12.00	0.140000	12 inch	0.014	12.38	4,471.12	4,469.44	4,474.12	4,473.00	4,472.50	4,472.40
LAT:CB 1-10	CB 1-11	SDMH 1-11	0.53	2.94	12.00	0.100833	12 inch	0.014	10.50	4,471.12	4,469.91	4,474.12	4,474.01	4,472.83	4,472.74

Pipe Report

Label	Upstream Node	Downstream Node	Upstream Inlet Rational Coefficient	Total System Flow (cfs)	Length (ft)	Constructed Slope (ft/ft)	Section Size	Manning's n	Full Capacity (cfs)	Upstream Invert Elevation (ft)	Downstream Invert Elevation (ft)	Upstream Ground Elevation (ft)	Downstream Ground Elevation (ft)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)
LAT:CB 1-09	CB 1-10	BT:CB 1-09	0.53	2.41	34.00	0.055882	12 inch	0.014	7.82	4,471.19	4,469.29	4,474.19	4,474.29	4,471.85	4,469.67
LAT:CB 1-08	CB 1-09 A	BT:CB 1-08	0.53	2.59	7.00	0.134286	12 inch	0.014	12.12	4,470.00	4,469.06	4,473.00	4,473.00	4,470.69	4,469.45
LAT:CB 1-06	CB 1-07 A	BT:CB 1-06	0.53	6.68	7.00	0.341429	12 inch	0.014	19.33	4,466.11	4,463.72	4,469.11	4,469.00	4,467.40	4,467.11
LAT:CB 1-05	CB 1-06	BT 1-06	0.53	4.59	54.00	0.090741	12 inch	0.014	9.97	4,461.61	4,456.71	4,464.61	4,464.00	4,463.47	4,462.43
LAT:CB 1-02	CB 1-02 A	BT:CB 1-02	0.53	2.70	6.00	0.435000	12 inch	0.014	21.82	4,469.11	4,466.50	4,472.11	4,472.14	4,469.81	4,468.33
LAT:CB 2-11	CB 2-11 A	SDMH 2-23	0.53	5.52	53.00	0.085094	12 inch	0.014	9.65	4,485.46	4,480.95	4,488.46	4,487.05	4,486.40	4,482.14
LAT:CB 1-08	CB 1-08 A	BT:CB 1-08	0.53	9.42	26.00	0.106538	12 inch	0.010	15.12	4,466.49	4,463.72	4,469.49	4,469.00	4,468.18	4,467.11
LAT:CB 1-03	CB 1-04 A	SDMH 1-08	0.53	7.26	34.00	0.073529	12 inch	0.010	12.56	4,459.24	4,456.74	4,462.35	4,462.08	4,461.67	4,460.84
LAT: 2-06	CB 2-06 A	SDMH 2-10	0.53	4.54	45.00	0.086333	12 inch	0.014	9.66	4,519.48	4,515.64	4,522.48	4,521.60	4,520.37	4,519.50
LAT: 2-05	CB 2-05	SDMH 2-10	0.53	2.53	27.00	0.117778	12 inch	0.014	11.35	4,518.82	4,515.64	4,521.82	4,521.60	4,519.57	4,519.50
LAT: 2-03	CB 2-03 A	BT: 2-03	0.53	1.80	32.00	0.115000	12 inch	0.010	15.71	4,514.66	4,510.98	4,517.66	4,517.22	4,515.23	4,512.35
LAT: 1-25	CB 1-25	BT 1-25	0.53	7.36	23.00	0.182174	12 inch	0.014	14.12	4,459.95	4,455.76	4,462.95	4,463.07	4,460.93	4,458.04
LAT 2-04	CB 2-04 A	BT 2-04	0.53	5.93	7.00	0.458571	12 inch	0.014	22.40	4,515.41	4,512.20	4,518.41	4,518.20	4,516.36	4,515.82
LAT 2-02	CB 2-02 A	BT:CB 2-02	0.53	2.85	26.00	0.087308	12 inch	0.014	9.77	4,486.73	4,484.46	4,489.73	4,489.46	4,487.45	4,485.21
LAT 2-01	CB 2-01 A	SDMH 2-02	0.53	2.81	10.00	0.233000	12 inch	0.014	15.97	4,485.92	4,483.59	4,488.92	4,488.69	4,486.64	4,484.51
LAT 1-3	CB 1-03	BT:CB 1-3	0.53	2.11	24.00	0.117083	12 inch	0.010	15.85	4,472.37	4,469.56	4,475.37	4,475.00	4,472.99	4,470.65
LAT 1-26	CB 1-26 A	SDMH 1-30	0.53	7.14	22.00	0.108182	12 inch	0.010	15.23	4,460.61	4,458.23	4,463.61	4,463.73	4,461.59	4,459.99
LAT 1-24	CB 1-24	BT 1-24	0.53	2.55	54.00	0.072593	12 inch	0.014	8.91	4,460.95	4,457.03	4,463.95	4,460.00	4,461.63	4,458.53
LAT 1-01	CB 1-01 A	BT:CB 1-01	0.53	6.47	54.00	0.053889	12 inch	0.014	7.68	4,468.80	4,465.89	4,471.80	4,471.84	4,469.86	4,467.79

Inlet Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Rim Elevation (ft)	Sump Elevation (ft)	Area (acres)	Inlet C	Inlet CA (acres)	Total Flow To Inlet (cfs)	Total Intercepted Flow (cfs)	Total Bypassed Flow (cfs)	Bypass Target	Time of Concentration (min)	Inlet Location	Known Flow (cfs)	Inlet
CB 1-01 A-E	9+31	4,471.80	4,471.80	4,468.80	1.40	0.53	0.74	6.47	6.47	0.00		11.96	In Sag	0.00	Combination DUAL
CB 1-02 A-E	8+99	4,472.11	4,472.11	4,469.11	1.49	0.53	0.79	5.27	2.70	2.56	CB 1-04 A-	11.87	On Grade	0.00	Combination DUAL
CB 1-03	10+67	4,475.37	4,475.37	4,472.37	2.29	0.53	1.21	3.50	2.11	1.39	CB 1-01 A-	13.79	On Grade	0.00	Combination 4R
CB 1-04 A-E	7+04	4,462.35	4,462.35	4,459.24	3.42	0.53	1.81	7.26	7.26	0.00		14.92	In Sag	0.00	Combination DUAL
CB 1-05 A-E	6+91	4,462.24	4,462.24	4,459.24	4.59	0.53	2.43	6.54	6.54	0.00		15.89	In Sag	0.00	Combination DUAL
CB 1-06	9+58	4,464.61	4,464.61	4,461.61	2.99	0.53	1.58	4.59	4.59	0.00		13.66	In Sag	0.00	Combination 4R
CB 1-07 A-E	12+51	4,469.11	4,469.11	4,466.11	2.90	0.53	1.54	6.68	6.68	0.00		14.84	In Sag	0.00	Combination DUAL
CB 1-08 A-E	12+70	4,469.49	4,469.49	4,466.49	2.87	0.53	1.52	9.42	9.42	0.00		14.15	In Sag	0.00	Combination DUAL
CB 1-09 A-E	15+01	4,473.00	4,473.00	4,470.00	3.60	0.53	1.91	5.21	2.59	2.62	CB 1-08 A-	15.18	On Grade	0.00	Combination DUAL
CB 1-10	15+99	4,474.19	4,474.19	4,471.19	2.59	0.53	1.37	4.48	2.41	2.07	CB 1-11	13.14	On Grade	0.00	Combination 4R
CB 1-11	0+83	4,474.12	4,474.12	4,471.12	0.35	0.53	0.19	2.94	2.94	0.00		10.00	In Sag	0.00	Combination 4R
CB 1-12	0+54	4,474.12	4,474.12	4,471.12	0.06	0.53	0.03	2.92	2.92	0.00		10.00	In Sag	0.00	Combination 4R
CB 1-13	1+28	4,475.06	4,475.06	4,472.06	3.17	0.53	1.68	4.69	2.32	2.37	CB 1-12	14.58	On Grade	0.00	Combination 4R
CB 1-14	2+24	4,476.50	4,476.50	4,473.50	2.91	0.53	1.54	6.98	6.98	0.00		13.04	In Sag	0.00	Combination 4R
CB 1-15 A-E	2+57	4,475.97	4,475.97	4,472.97	4.40	0.53	2.33	9.81	9.81	0.00		10.44	In Sag	0.00	Combination DUAL
CB 1-16	7+47	4,479.64	4,479.64	4,476.64	3.66	0.53	1.94	6.41	6.41	0.00		10.11	In Sag	0.00	Combination 4R
CB 1-17 A-E	12+56	4,479.62	4,479.62	4,476.62	6.01	0.53	3.19	9.14	9.14	0.00		13.88	In Sag	0.00	Combination DUAL
CB 1-18 A-E	12+48	4,479.62	4,479.62	4,476.62	4.45	0.53	2.36	7.53	7.53	0.00		11.07	In Sag	0.00	Combination DUAL
CB 1-19 A-E	13+75	4,506.60	4,506.60	4,503.60	1.81	0.53	0.96	4.97	4.97	0.00		10.00	In Sag	0.00	Combination DUAL
CB 1-20	15+85	4,514.92	4,514.92	4,511.92	2.64	0.53	1.40	4.30	2.64	1.66	CB 1-19 A-	12.12	On Grade	0.00	Combination 4R
CB 1-21 A-E	15+92	4,514.70	4,514.70	4,511.70	4.88	0.53	2.59	8.40	3.84	4.56	CB 1-22 A-	10.58	On Grade	0.00	Combination DUAL
CB 1-22 A-E	16+09	4,514.49	4,514.49	4,511.49	0.95	0.53	0.19	5.27	5.27	0.00		10.00	In Sag	0.00	Combination DUAL
CB 1-23	0+89	4,463.95	4,463.95	4,460.95	2.24	0.53	1.19	3.39	3.39	0.00		14.04	In Sag	0.00	Combination 4R
CB 1-24	1+23	4,463.95	4,463.95	4,460.95	1.71	0.53	0.91	2.55	2.55	0.00		14.40	In Sag	0.00	Combination 4R
CB 1-25	0+41	4,462.95	4,462.95	4,459.95	1.65	0.53	0.87	7.36	7.36	0.00		14.85	In Sag	0.00	Combination DUAL
CB 1-26 A-E	1+85	4,463.61	4,463.61	4,460.61	5.94	0.53	3.15	11.97	7.14	4.83	CB 1-25	15.76	On Grade	0.00	Combination DUAL
CB 1-27 A-E	5+35	4,465.18	4,465.18	4,462.18	6.56	0.53	3.48	9.42	5.92	3.50	CB 1-26 A-	15.54	On Grade	0.00	Combination DUAL
CB 2-01 A-E	16+40	4,488.92	4,488.92	4,485.92	3.72	0.53	1.97	5.21	2.81	2.40	CB 1-02 A-	16.69	On Grade	0.00	Combination DUAL
CB 2-02 A-E	16+85	4,489.73	4,489.73	4,486.73	2.80	0.53	1.48	5.35	2.85	2.49	CB 1-01 A-	13.91	On Grade	0.00	Combination DUAL
CB 2-03 A-E	26+44	4,517.66	4,517.66	4,514.66	0.07	0.53	0.04	2.96	1.80	1.16	CB 2-02 A-	12.26	On Grade	0.00	Combination DUAL
CB 2-04 A-E	26+82	4,518.41	4,518.41	4,515.41	1.47	0.53	0.78	5.93	5.93	0.00		12.01	In Sag	0.00	Combination DUAL
CB 2-05	29+66	4,521.82	4,521.82	4,518.82	3.51	0.53	1.86	5.07	2.53	2.54	CB 2-03 A-	15.26	On Grade	0.00	Combination Type4
CB 2-06 A-E	29+84	4,522.48	4,522.48	4,519.48	5.16	0.53	2.73	7.79	4.54	3.25	CB 2-04 A-	14.06	On Grade	0.00	Combination DUAL
CB 2-07 A-E	19+84	4,484.25	4,484.25	4,481.25	3.42	0.53	1.81	5.59	2.87	2.72	CB 1-07 A-	12.00	On Grade	0.00	Combination DUAL
CB 2-08 A-E	19+88	4,483.97	4,483.97	4,480.97	2.01	0.53	1.07	5.38	2.81	2.58	CB 1-08 A-	11.95	On Grade	0.00	Combination DUAL

Inlet Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Rim Elevation (ft)	Sump Elevation (ft)	Area (acres)	Inlet C	Inlet C/A (acres)	Total Flow To Inlet (cfs)	Total Intercepted Flow (cfs)	Total Bypassed Flow (cfs)	Bypass Target	Time of Concentration (min)	Inlet Location	Known Flow (cfs)	Inlet
CB 2-09	26+48	4,499.82	4,499.82	4,496.82	2.96	0.53	1.57	4.28	2.44	1.85	CB 2-08 A	15.18	On Grade	0.00	Combination 4R
CB 2-10 A-E	26+30	4,499.69	4,499.69	4,496.69	5.74	0.53	3.04	9.49	9.49	0.00		11.71	In Sag	0.00	Combination DUAL
CB 2-11 A-E	22+64	4,488.46	4,488.46	4,485.46	3.14	0.53	1.66	5.52	5.52	0.00		10.00	In Sag	0.00	Combination DUAL
CB 2-12	2+27	4,528.94	4,528.94	4,525.94	1.45	0.53	0.77	2.50	2.04	0.46	CB 1-10	10.54	On Grade	0.00	Combination 4R
CB 2-13	6+20	4,554.22	4,554.22	4,551.22	0.17	0.53	0.09	0.30	0.30	0.00	CB 2-04 A	10.00	On Grade	0.00	Combination 4R
CB 2-14 A-E	2+79	4,523.56	4,523.56	4,520.56	3.48	0.53	1.84	6.02	3.38	2.64	CB 1-14	10.47	On Grade	0.00	Combination DUAL
CB 2-15 A-E	2+88	4,523.28	4,523.28	4,520.28	3.23	0.53	1.71	5.13	3.12	2.01	CB 1-15 A	12.79	On Grade	0.00	Combination DUAL
DITCH 2-1	0+57	4,533.00	4,533.00	4,530.00	3.07	0.00	0.00	0.00	0.00	0.00		18.33	In Sag	0.00	Generic Default 10
I-43	9+79	4,468.00	4,468.00	4,465.00	0.00	0.00	0.00	4.50	4.50	0.00		0.00	In Sag	0.00	Generic Default 10

Scenario: Base

Junction Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Set Rim Equal to Ground Elevation?	Rim Elevation (ft)	Sump Elevation (ft)	Bolted Cover?	Structure Diameter (ft)	Description
BT 1-06	9+04	4,464.00	true	4,464.00	4,455.71	true	0.00	
BT 1-23	0+28	4,460.00	true	4,460.00	4,456.82	true	0.00	
BT 1-24	0+69	4,460.00	true	4,460.00	4,457.03	true	0.00	
BT 1-25	0+18	4,463.07	true	4,463.07	4,455.76	true	0.00	
BT 2-04	26+75	4,518.20	true	4,518.20	4,512.20	true	0.00	
BT 2-10	2+02	4,526.00	true	4,526.00	4,520.91	true	0.00	
BT: 2-03	26+12	4,517.22	true	4,517.22	4,510.98	true	0.00	
BT:CB 1-01	8+77	4,471.84	true	4,471.84	4,465.35	true	0.00	
BT:CB 1-02	8+93	4,472.14	true	4,472.14	4,466.00	true	0.00	
BT:CB 1-06	12+44	4,469.00	true	4,469.00	4,463.22	true	0.00	
BT:CB 1-08	14+94	4,473.00	true	4,473.00	4,466.79	true	0.00	
BT:CB 1-09	15+65	4,474.29	true	4,474.29	4,468.29	true	0.00	
BT:CB 1-11	0+42	4,473.00	true	4,473.00	4,467.60	true	0.00	
BT:CB 1-12	1+01	4,474.84	true	4,474.84	4,467.65	true	0.00	
BT:CB 1-14	2+50	4,475.69	true	4,475.69	4,468.30	true	0.00	
BT:CB 1-15	7+42	4,479.48	true	4,479.48	4,471.48	true	0.00	
BT:CB 1-18	13+39	4,505.74	true	4,505.74	4,500.00	true	0.00	
BT:CB 1-3	10+43	4,475.00	true	4,475.00	4,469.06	true	0.00	
BT:CB 2-02	16+59	4,489.46	true	4,489.46	4,483.46	true	0.00	
BT:CB 2-07	19+77	4,484.06	true	4,484.06	4,478.06	true	0.00	
BT:CB 2-08	19+64	4,483.76	true	4,483.76	4,477.76	true	0.00	
SDMH 1-01	3+91	4,464.54	true	4,464.54	4,452.78	false	4.00	
SDMH 1-02	4+51	4,464.02	true	4,464.02	4,453.00	false	4.00	
SDMH 1-03	5+27	4,463.33	true	4,463.33	4,453.25	false	4.00	
SDMH 1-04	5+92	4,462.74	true	4,462.74	4,453.48	false	4.00	
SDMH 1-05	6+70	4,462.08	true	4,462.08	4,453.74	false	4.00	
SDMH 1-06	7+49	4,462.48	true	4,462.48	4,454.38	false	4.00	
SDMH 1-07	9+58	4,465.31	true	4,465.31	4,456.21	false	4.00	
SDMH 1-08	10+21	4,466.14	true	4,466.14	4,456.54	false	4.00	
SDMH 1-09	12+10	4,468.80	true	4,468.80	4,462.70	false	4.00	
SDMH 1-10	15+27	4,473.25	true	4,473.25	4,467.15	false	4.00	
SDMH 1-11	0+71	4,474.01	true	4,474.01	4,467.91	false	4.00	
SDMH 1-12	0+58	4,474.63	true	4,474.63	4,467.33	false	4.00	
SDMH 1-13	1+98	4,475.29	true	4,475.29	4,467.99	false	4.00	
SDMH 1-14	3+68	4,476.48	true	4,476.48	4,468.77	false	4.00	
SDMH 1-15	4+70	4,477.22	true	4,477.22	4,469.82	false	4.00	
SDMH 1-16	6+02	4,478.09	true	4,478.09	4,470.58	false	4.00	
SDMH 1-17	7+14	4,478.90	true	4,478.90	4,471.24	false	4.00	
SDMH 1-18	8+13	4,481.52	true	4,481.52	4,471.84	false	4.00	
SDMH 1-19	9+00	4,485.33	true	4,485.33	4,472.38	false	4.00	
SDMH 1-20	11+40	4,480.83	true	4,480.83	4,474.28	false	4.00	
SDMH 1-21	11+98	4,479.72	true	4,479.72	4,474.66	false	4.00	
SDMH 1-22	11+46	4,497.09	true	4,497.09	4,490.99	false	4.00	
SDMH 1-23	12+99	4,504.28	true	4,504.28	4,498.18	false	4.00	
SDMH 1-24	14+52	4,511.34	true	4,511.34	4,505.34	false	4.00	
SDMH 1-25	15+52	4,513.76	true	4,513.76	4,507.76	false	4.00	
SDMH 1-26	4+68	4,465.25	true	4,465.25	4,453.03	false	4.00	
SDMH 1-27	6+10	4,466.78	true	4,466.78	4,453.41	false	4.00	
SDMH 1-28	8+99	4,472.37	true	4,472.37	4,466.27	false	4.00	
SDMH 1-29	11+64	4,477.24	true	4,477.24	4,471.14	false	4.00	
SDMH 1-30	1+63	4,463.73	true	4,463.73	4,458.13	false	4.00	

Scenario: Base

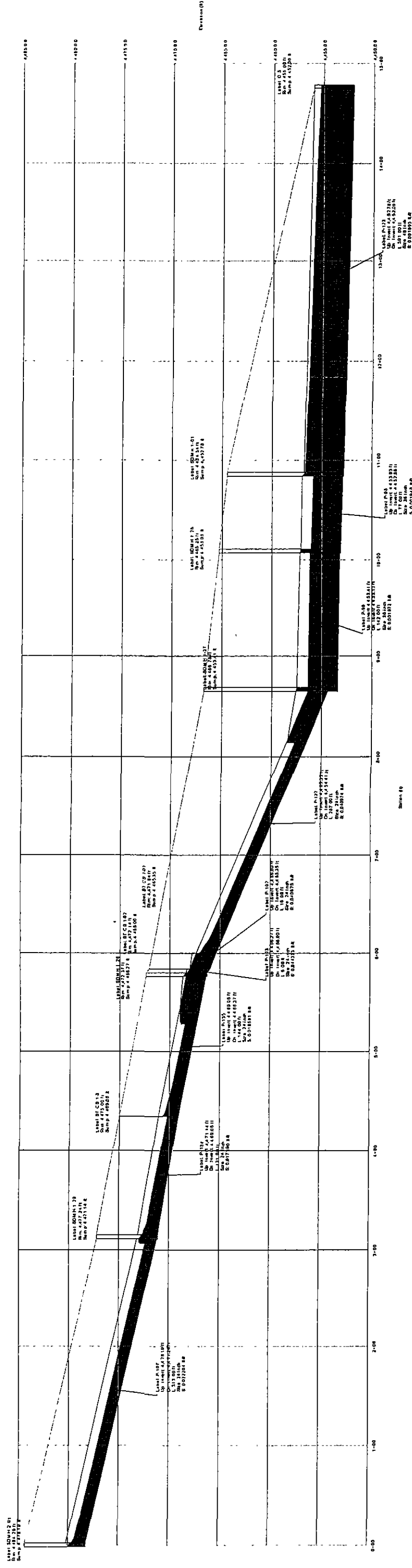
Junction Report

Label	Calculated Station (ft)	Ground Elevation (ft)	Set Rim Equal to Ground Elevation?	Rim Elevation (ft)	Sump Elevation (ft)	Bolled Cover?	Structure Diameter (ft)	Description
SDMH 1-31	5+13	4,465.30	true	4,465.30	4,459.98	false	4.00	
SDMH 1-32	8+63	4,466.88	true	4,466.88	4,461.83	false	4.00	
SDMH 2-01	14+77	4,484.29	true	4,484.29	4,478.19	false	4.00	
SDMH 2-02	16+30	4,488.69	true	4,488.69	4,482.59	true	0.00	
SDMH 2-03	18+44	4,494.20	true	4,494.20	4,488.10	false	4.00	
SDMH 2-04	19+88	4,497.11	true	4,497.11	4,491.01	false	4.00	
SDMH 2-05	23+24	4,507.20	true	4,507.20	4,501.10	false	4.00	
SDMH 2-06	24+24	4,510.91	true	4,510.91	4,504.81	false	4.00	
SDMH 2-07	25+24	4,514.61	true	4,514.61	4,508.51	false	4.00	
SDMH 2-08	26+20	4,517.31	true	4,517.31	4,511.21	false	4.00	
SDMH 2-09	27+29	4,518.81	true	4,518.81	4,512.71	false	4.00	
SDMH 2-10	29+39	4,521.60	true	4,521.60	4,515.60	false	4.00	
SDMH 2-11	13+96	4,472.78	true	4,472.78	4,466.68	false	4.00	
SDMH 2-12	15+58	4,475.52	true	4,475.52	4,469.42	false	4.00	
SDMH 2-13	17+18	4,478.73	true	4,478.73	4,472.63	false	4.00	
SDMH 2-14	18+69	4,481.75	true	4,481.75	4,475.65	false	4.00	
SDMH 2-15	20+29	4,485.35	true	4,485.35	4,479.35	false	4.00	
SDMH 2-16	21+57	4,488.45	true	4,488.45	4,482.35	false	4.00	
SDMH 2-17	23+72	4,493.54	true	4,493.54	4,487.44	false	4.00	
SDMH 2-18	24+80	4,496.00	true	4,496.00	4,489.90	false	4.00	
SDMH 2-19	25+99	4,498.59	true	4,498.59	4,492.49	false	4.00	
SDMH 2-20	17+25	4,477.07	true	4,477.07	4,470.97	false	4.00	
SDMH 2-21	18+81	4,479.70	true	4,479.70	4,473.60	false	4.00	
SDMH 2-22	20+25	4,482.15	true	4,482.15	4,476.05	false	4.00	
SDMH 2-23	22+11	4,487.05	true	4,487.05	4,480.95	false	4.00	
SDMH 2-24	2+29	4,527.24	true	4,527.24	4,521.14	false	4.00	
SDMH 2-25	5+80	4,554.59	true	4,554.59	4,548.59	false	4.00	
SDMH 2-26	2+53	4,521.68	true	4,521.68	4,516.68	false	4.00	
SDMH 2-27	1+11	4,520.00	true	4,520.00	4,514.88	false	4.00	

Profile
Scenario: Base

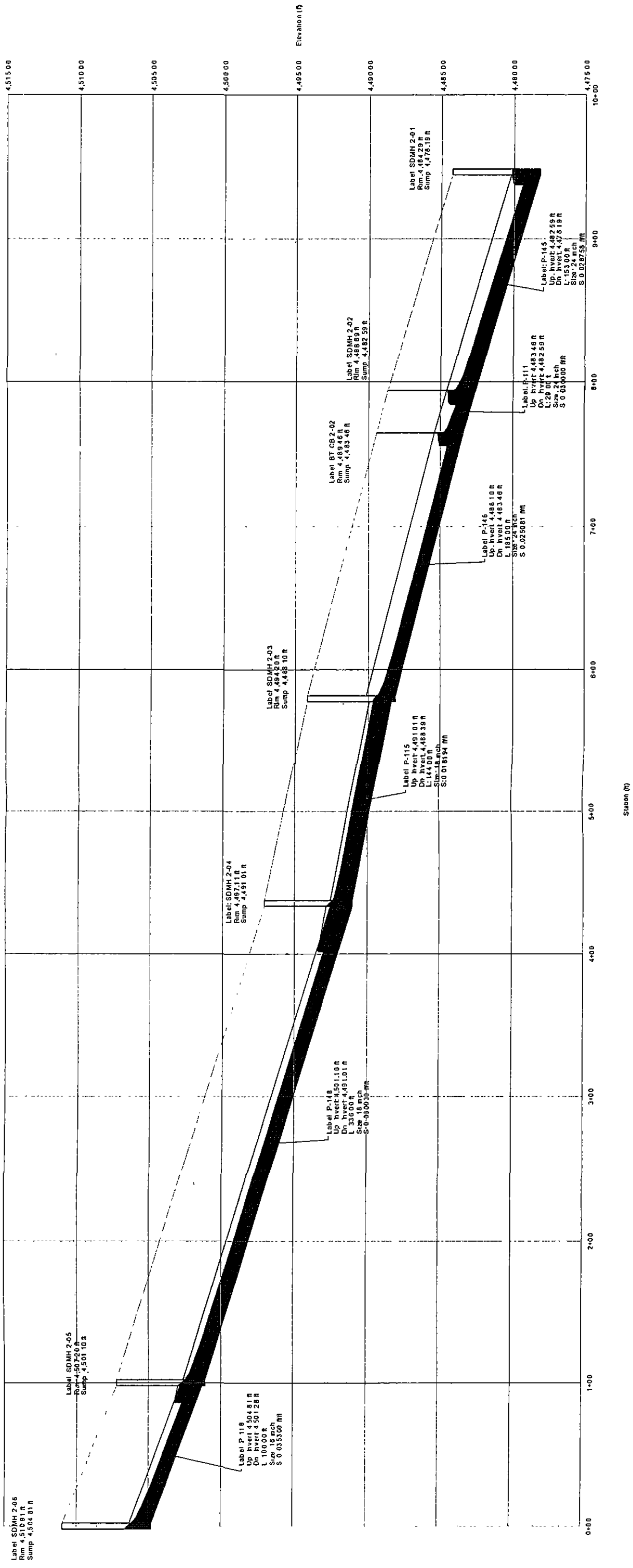
Profile: GOLD RIVER NORTH - A

Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER NORTH - B
Scenario: Base

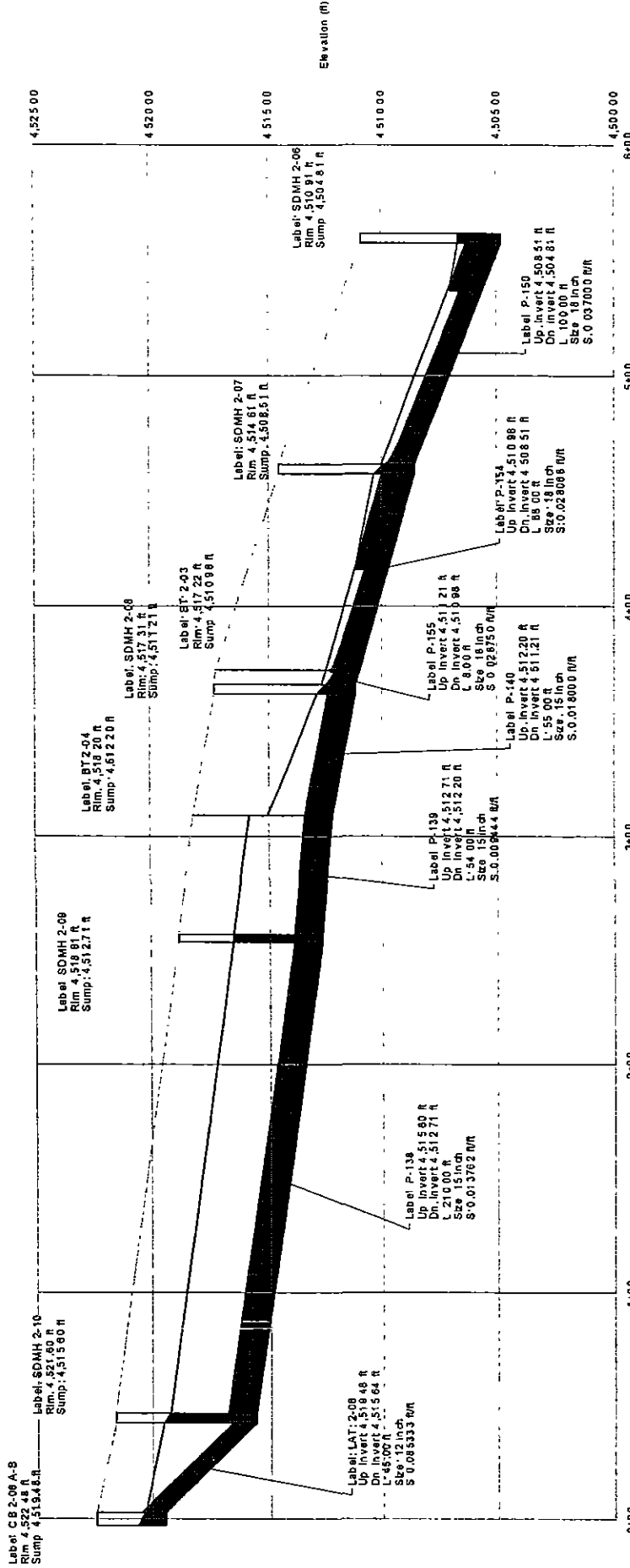




Scenario: Base

Profile: GOLD RIVER NORTH -C

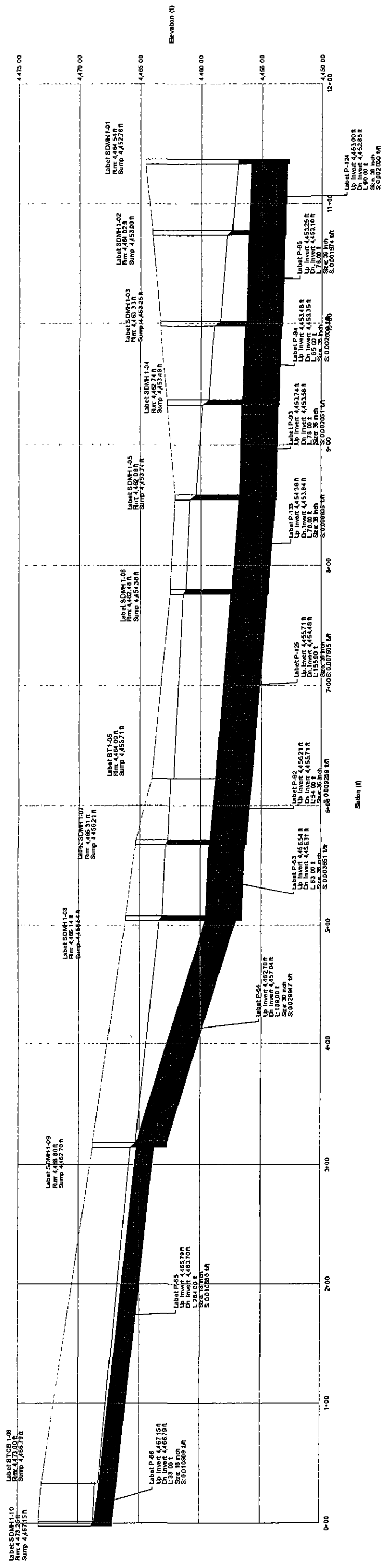
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Profile
Scenario: Base

Profile: GOLD RIVER SOUTH - A

Scenario: Base

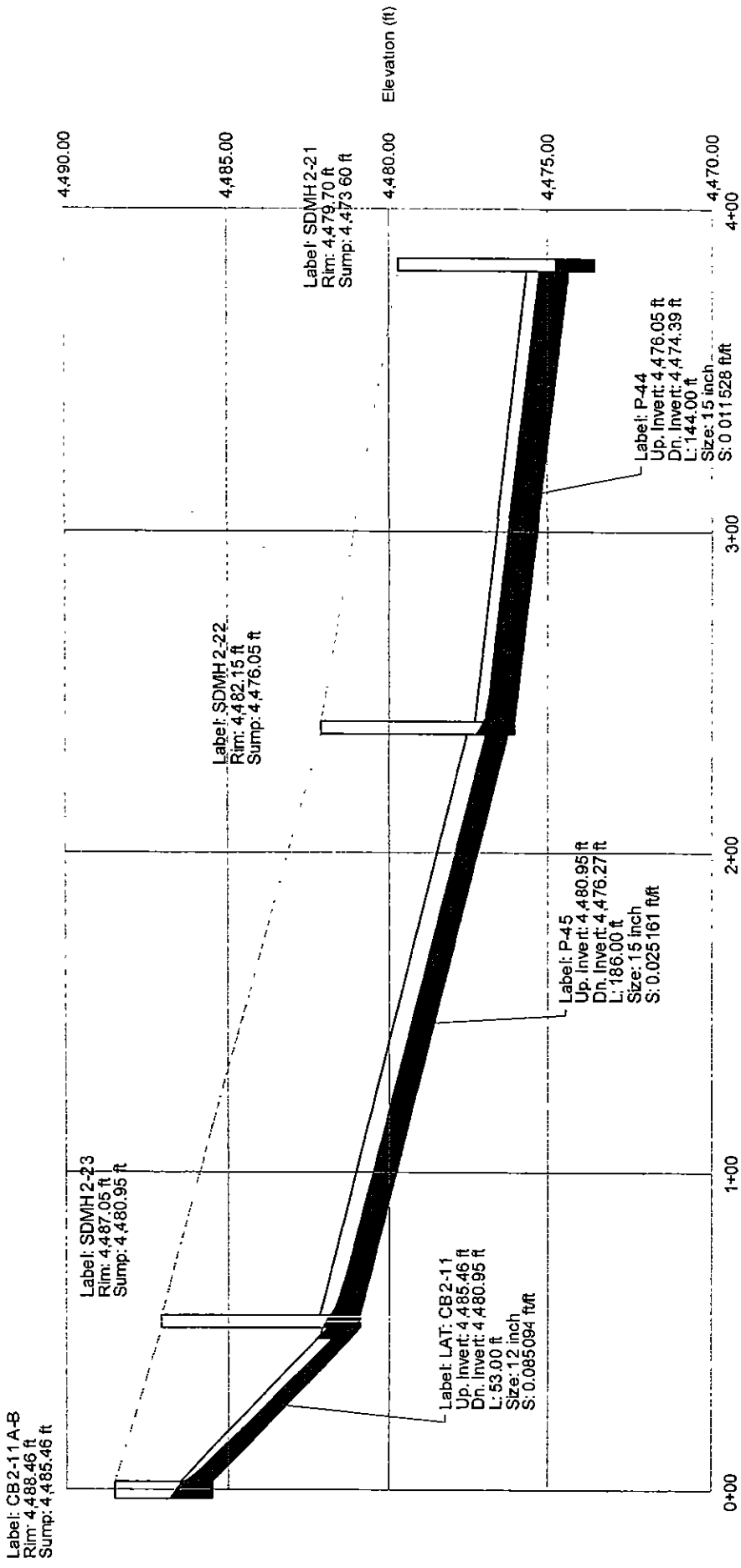




Scenario: Base

Profile: HOLLOW BASIN - A

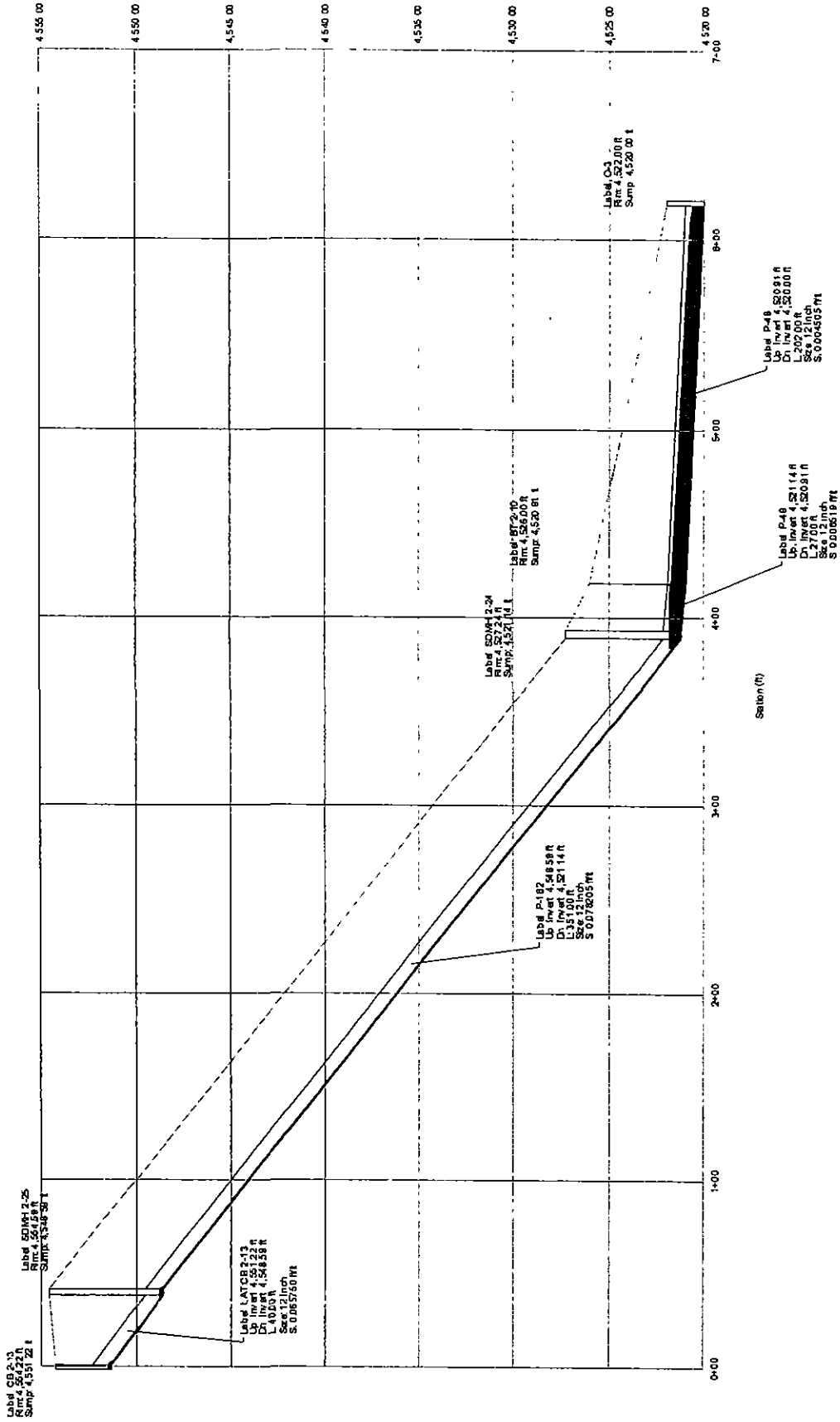
Scenario: Base



Station (ft)

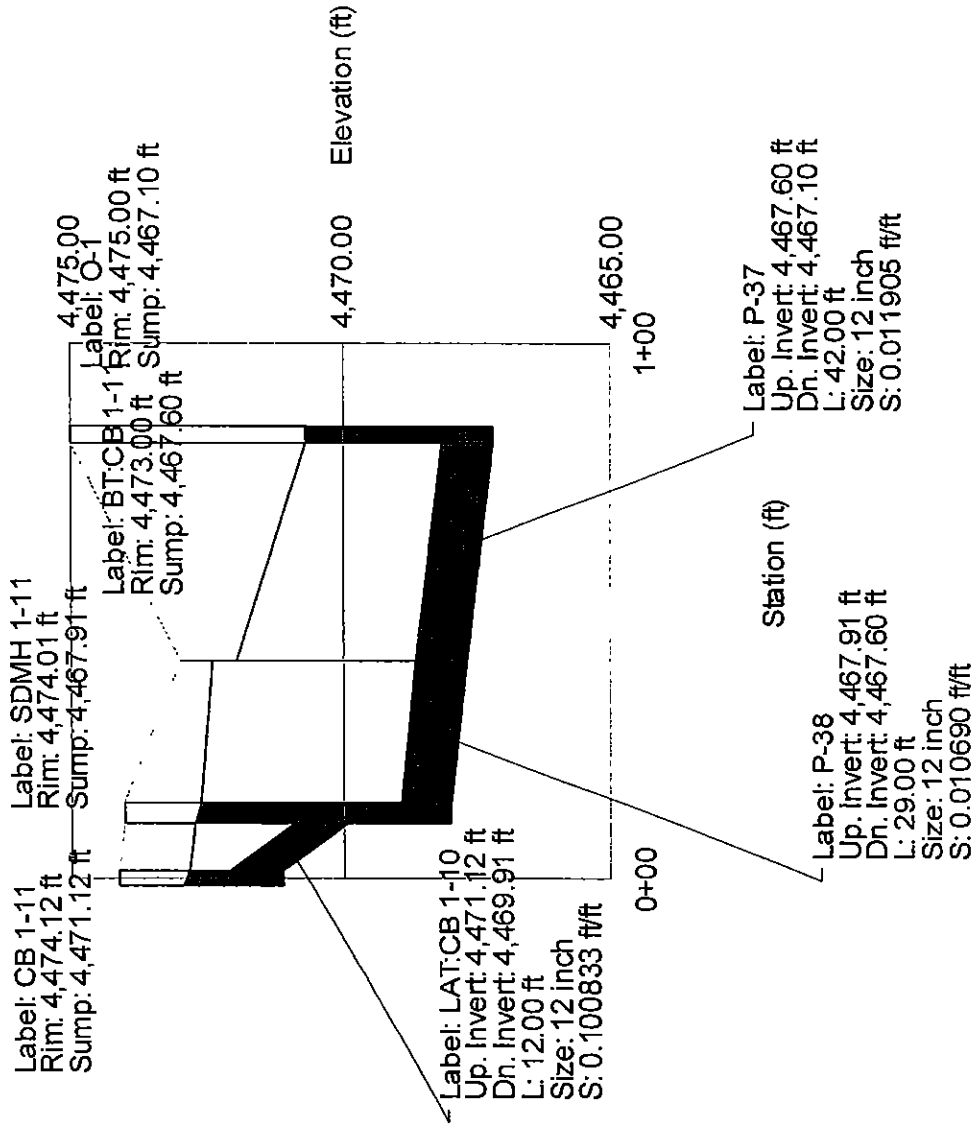
file
Scenario: Base

Profile: HOLLOWBASIN - B
Scenario: Base



Profile: GOLD RIVER SOUTH - B

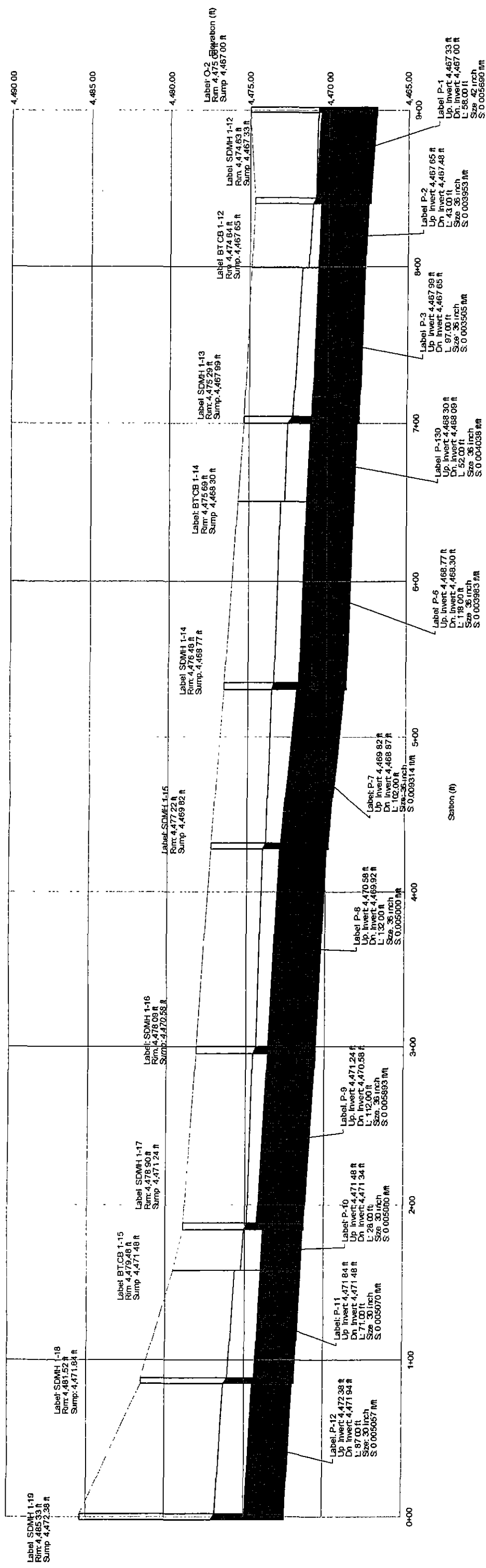
Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER SOUTH - C

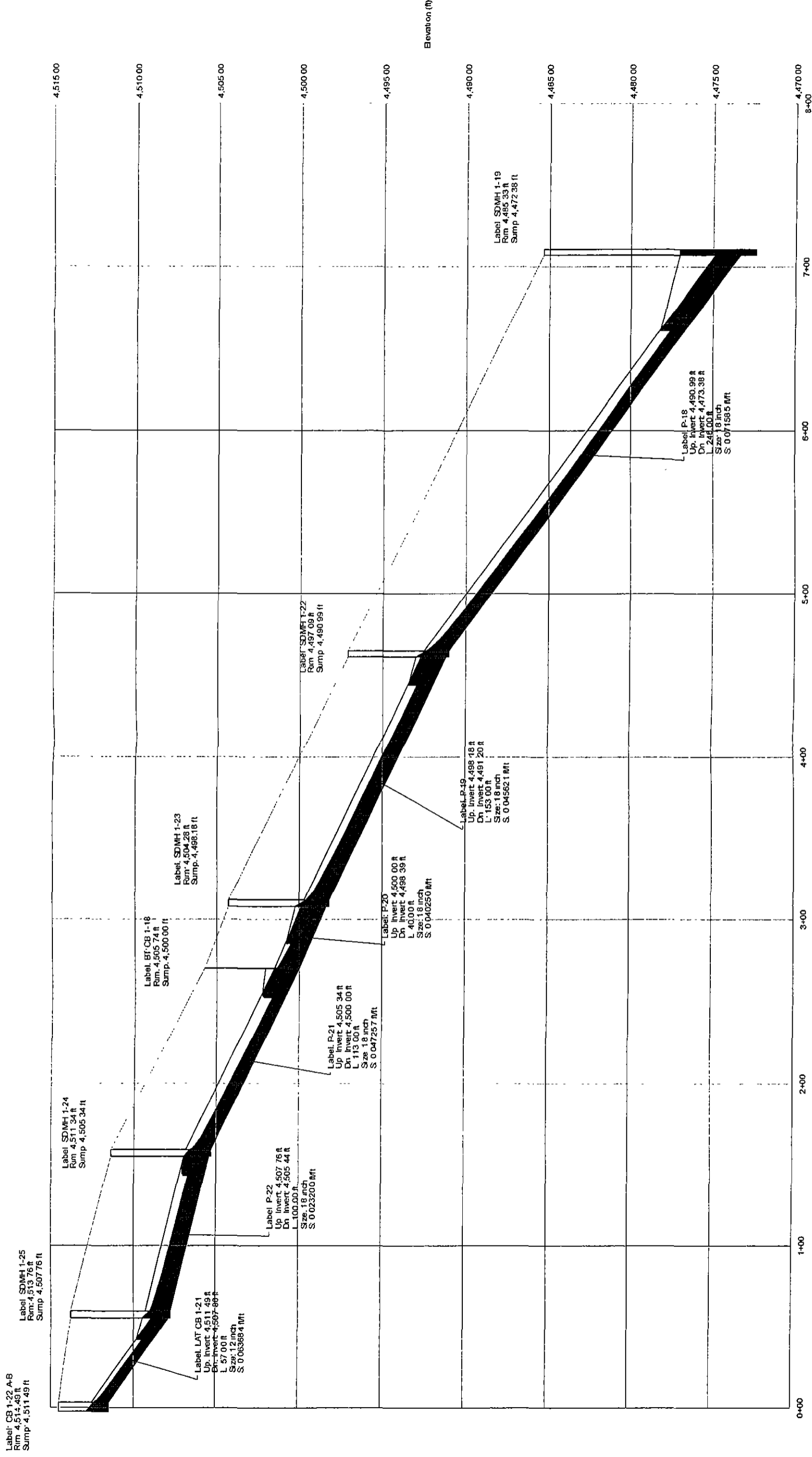
Scenario: Base



Profile
Scenario: Base

Profile: GOLD RIVER SOUTH - D

Scenario: Base

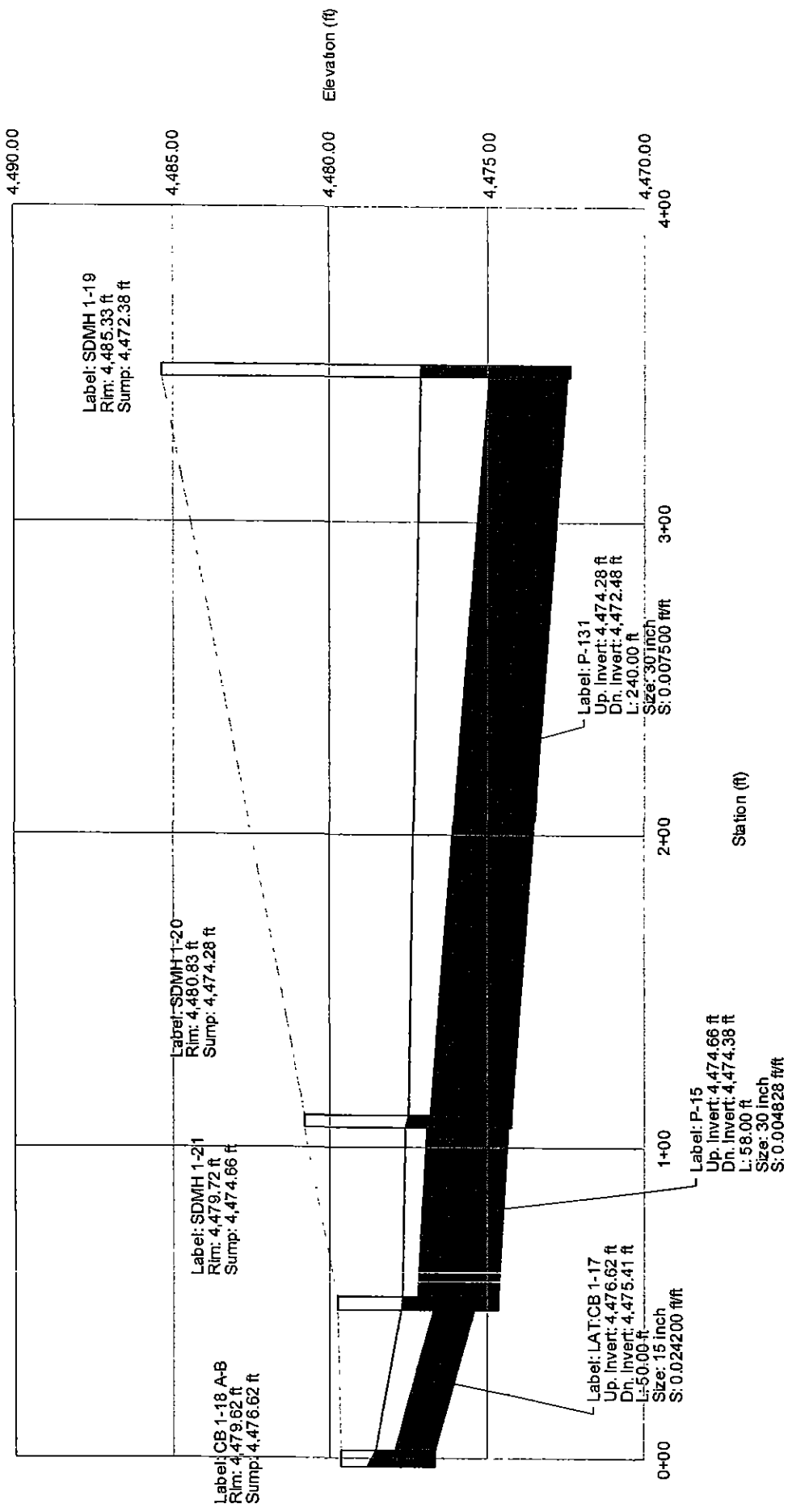




Scenario: Base

Profile: DRY GULCH - A

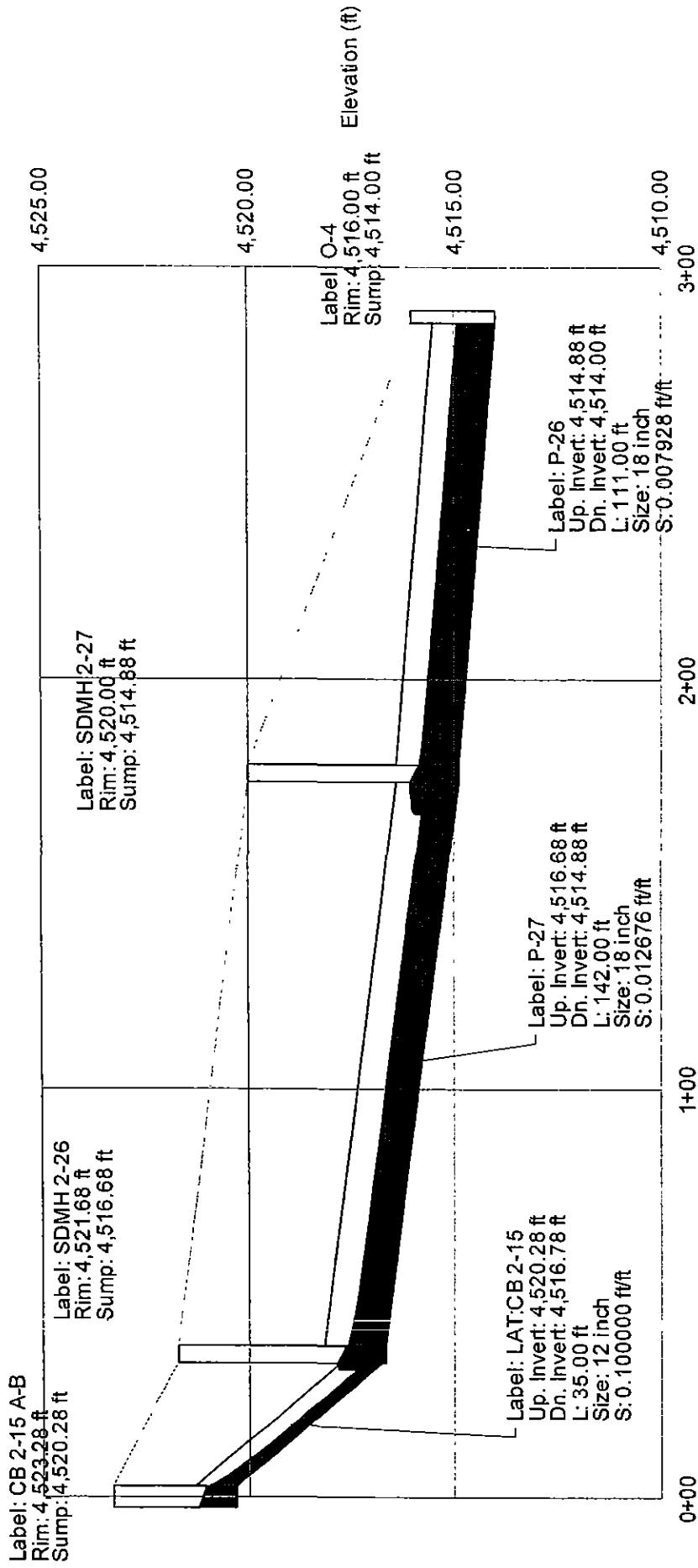
Scenario: Base



ofile
Scenario: Base

Profile: DRY GULCH - B

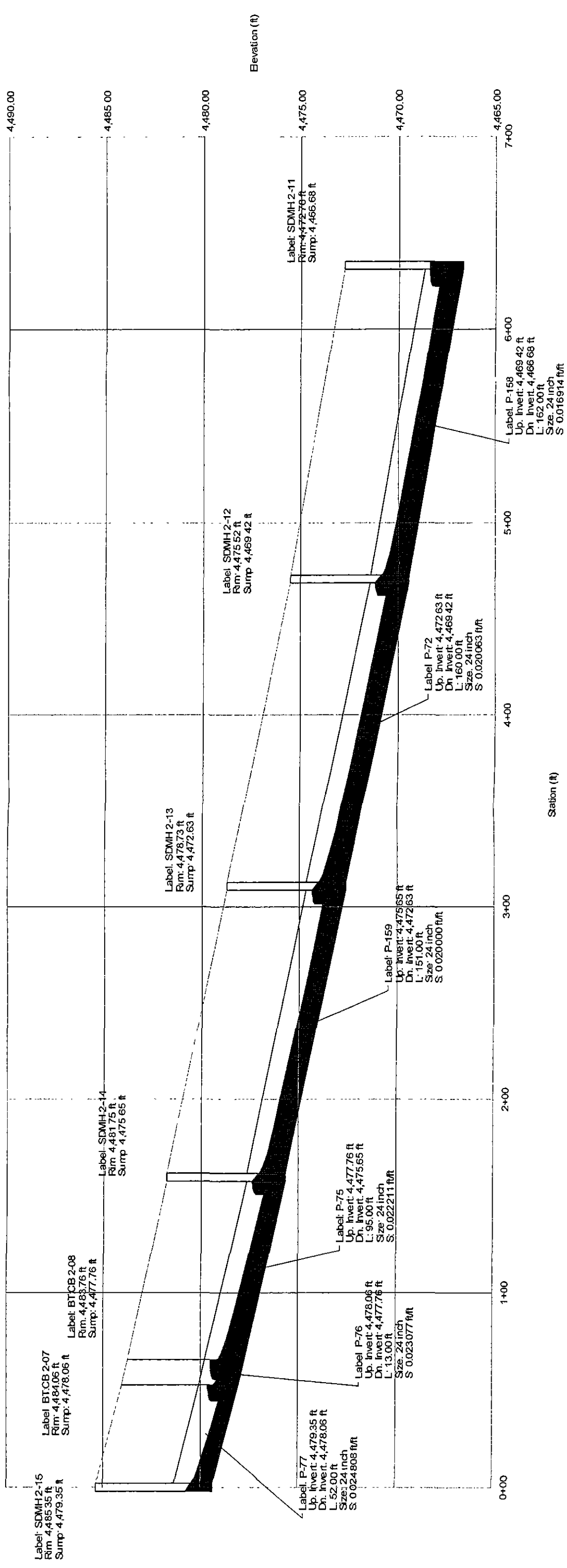
Scenario: Base



Station (ft)

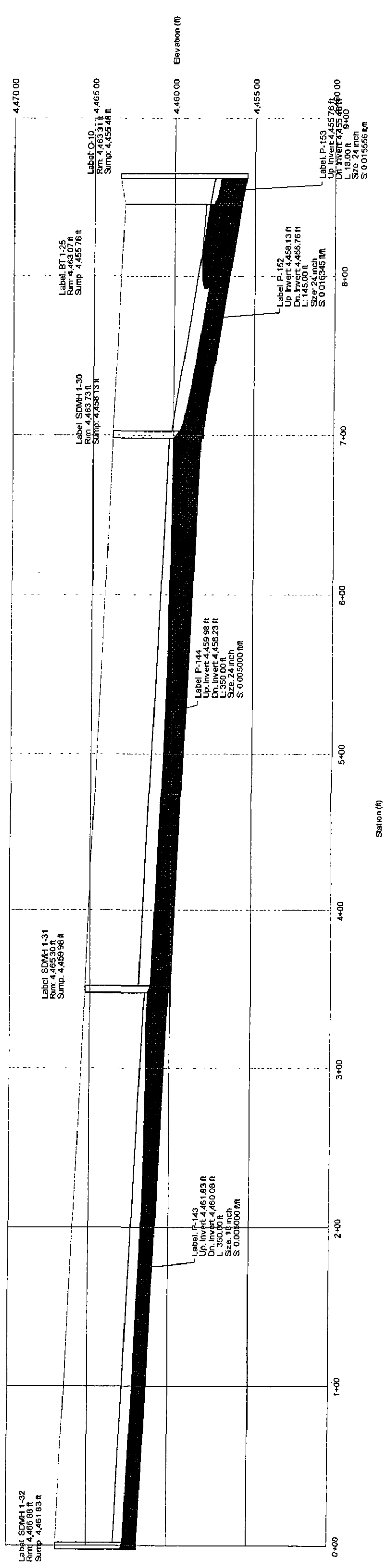
Profile
Scenario: Base

Profile: ORE CIRCLE - A
Scenario: Base



Profile
Scenario: Base

Profile: DESERT WAY
Scenario: Base



Appendix D
Channel Design Information

DAMONTE FOOTHILLS/GOLDEN HILLS
CHANNEL SECTIONS

PALISADES CHANNEL (OFF4 TO CP4)														
5' Bottom Width		(minimum Depth = 4.00')						(3:1 side slopes)						
Begin Station	End Station	Slope (%)	Q(100) (cfs)	d(100) (ft)	V(100) (fps)	Flow Type	Se (superelevation) (if necessary)	Freeboard (1' min.)	Channel Depth	Mannings n	Median Rock Size d50 (in)			
38+03.76	41+83.27	0.82	205.00	2.82	5.40	Subcritical	N/A	1.00	3.82	0.035	2			
41+83.27	47+74.14	5.90	205.00	1.89	10.14	Supercritical	N/A	1.31	3.20	0.040	12			
47+74.17	52+65.09	9.70	205.00	1.76	11.35	Supercritical	N/A	1.34	3.10	0.044	18			
52+65.09	57+23.66	2.74	205.00	2.13	8.43	Supercritical	N/A	1.27	3.40	0.035	6			
												Class 150	1.00	PYRAMAT
												Class 300	2.00	PYRAMAT
												Class 550	3.67	N/A
												Class 150	1.00	PYRAMAT

PALISADES CHANNEL (CP4 TO CP3)														
10' Bottom Width		(minimum Depth = 4.00')						(3:1 side slopes)						
Begin Station	End Station	Slope (%)	Q(100) (cfs)	d(100) (ft)	V(100) (fps)	Flow Type	Se (superelevation) (if necessary)	Freeboard (1' min.)	Channel Depth	Mannings n	Median Rock Size d50 (in)			
26+59.99	26+63.71	5.27	342.00	2.00	10.72	Supercritical	0.75 (Tw = 21.15, r = 50.50')	1.34	4.08	0.040	13			
26+63.71	27+40.31	5.27	342.00	2.00	10.72	Supercritical	0.64 (Tw = 21.15, r = 59.00')	1.34	3.96	0.040	13			
27+40.31	33+35.36	9.01	342.00	1.82	12.13	Supercritical	N/A	1.37	3.19	0.044	20			
33+35.36	35+35.72	5.33	342.00	1.99	10.77	Supercritical	N/A	1.34	3.33	0.040	13			
35+35.72	38+03.78	1.34	342.00	2.65	7.20	Subcritical	0.16 (Tw = 25.41, r = 130')	1.30	4.11	0.035	4			
												Class 300	2.00	PYRAMAT
												Class 300	2.00	PYRAMAT
												Class 550	3.67	N/A
												Class 300	2.00	PYRAMAT
												Class 150	1.00	PYRAMAT

DAMONTE FOOTHILLS/GOLDEN HILLS
CHANNEL SECTIONS

GOLDEN HILLS NORTH CHANNEL (CP3 TO CP1)														
12' Bottom Width		(2:1 side slopes)												
Begin Station	End Station	Slope (%)	Q(100) (cfs)	d(100) (ft)	V(100) (fps)	Flow Type	Se (super-elevation) (if necessary)	Freeboard (1' min.)	Channel Depth	Mannings n	Median Rock Size d50 (in)	Rock Rip-Rap Classification	Depth of Riprap (ft)	* Optional TRM Instead of Riprap
0+80.68	3+04.33	2.24	584.00	3.27	9.67	Supercritical	N/A	1.36	4.63	0.040	8	Class 300	2.00	PYRAMAT
3+04.33	5+08.33	1.46	584.00	3.41	9.09	Supercritical	N/A	1.34	4.75	0.035	6	Class 150	1.00	PYRAMAT
5+08.33	11+32.33	1.92	584.00	3.41	9.11	Supercritical	N/A	1.34	4.75	0.040	7	Class 300	2.00	PYRAMAT
11+32.33	14+50.51	2.20	584.00	3.29	9.56	Supercritical	N/A	1.36	4.65	0.040	8	Class 300	2.00	PYRAMAT
14+50.51	15+70.51	3.33	584.00	2.94	11.09	Supercritical	N/A	1.40	4.34	0.040	12	Class 300	2.00	PYRAMAT
15+70.51	17+60.51	2.63	584.00	3.14	10.19	Supercritical	N/A	1.37	4.51	0.040	9	Class 300	2.00	PYRAMAT
17+60.51	18+98.51	2.17	584.00	3.30	9.52	Supercritical	N/A	1.35	4.65	0.040	8	Class 300	2.00	PYRAMAT
18+98.51	21+18.51	3.64	584.00	2.87	11.45	Supercritical	N/A	1.41	4.28	0.040	13	Class 300	2.00	PYRAMAT
21+18.51	23+16.51	3.03	584.00	3.02	10.72	Supercritical	N/A	1.39	4.41	0.040	11	Class 300	2.00	PYRAMAT
23+16.51	23+70.51	5.56	584.00	2.70	12.43	Supercritical	N/A	1.43	4.13	0.044	18	Class 550	3.67	N/A
23+70.51	25+00.51	2.31	584.00	3.25	9.73	Supercritical	N/A	1.36	4.61	0.040	8	Class 300	2.00	PYRAMAT
25+00.51	25+59.99	1.68	584.00	3.29	9.56	Supercritical	N/A	1.36	4.65	0.035	7	Class 150	1.00	PYRAMAT

GOLDEN HILLS CENTRAL CHANNEL (CP8 TO CP7 & CP7 TO CP6)														
22' Bottom Width		(2:1 & 3:1 side slopes)												
Begin Station	End Station	Slope (%)	Q(100) (cfs)	d(100) (ft)	V(100) (fps)	Flow Type	Se (super-elevation) (if necessary)	Freeboard (1' min.)	Channel Depth	Mannings n	Median Rock Size d50 (in)	Rock Rip-Rap Classification	Depth of Riprap (ft)	* Optional TRM Instead of Riprap
10+00.00	16+00.00	1.50	695.00	3.82	8.52	Supercritical	1.24 (Tw = 32.90, r = 60.00')	1.33	6.39	0.035	5	Class 150	1.00	PYRAMAT
16+00.00	19+00.00	0.50	695.00	3.83	6.11	Subcritical	N/A	1.08	4.91	0.035	2	Class 150	1.00	PYRAMAT
19+00.00	20+50.00	1.00	695.00	3.16	7.77	Subcritical	N/A	1.44	4.60	0.035	4	Class 150	1.00	PYRAMAT
20+50.00	23+00.00	5.04	692.00	2.18	12.07	Supercritical	2.24 (Tw = 29.68, r = 60.00')	1.39	5.81	0.041	16	Class 400	2.67	PYRAMAT
23+00.00	30+00.00	4.56	692.00	2.24	11.67	Supercritical	2.11 (Tw = 29.90, r = 60.00')	1.38	5.73	0.041	15	Class 400	2.67	PYRAMAT
30+00.00 (3.1 sides)	40+00.00 (3.1 sides)	6.71	692.00	2.03	12.14	Supercritical	N/A	2.79	4.82	0.044	18	Class 550	3.67	N/A

DAMONTE FOOTHILLS/GOLDEN HILLS
CHANNEL SECTIONS

DESERT WAY CHANNEL (CP6 TO CP1)											
25' Bottom Width		(minimum Depth = 6.00')		(2.1 side slopes)							
Begin Station	End Station	Slope (%)	Q(100) (cfs)	d(100) (ft)	V(100) (fps)	Flow Type	Se (superlevation) (if necessary)	Freeboard (1' min.)	Channel Depth	Mannings n	Channel Lining
N/A	N/A	0.29	695.00	3.85	5.52	Subcritical	N/A	0.97	4.82	0.030	Grass
N/A	N/A	0.29	809.00	4.19	5.79	Subcritical	N/A	1.02	5.21	0.030	Grass
N/A	N/A	0.29	1274.00	5.38	6.63	Subcritical	N/A	1.18	6.56	0.030	Grass

Freeboard:

City of Reno Public Works Design Manual = 1.00' (minimum)
City of Sparks Hydrology Design Manual =

Superelevation:
Superelevation is the height that water will rise as it flows through a bend in the channel
City of Sparks Hydrology Design Manual = Se

Subcritical Flow

FB = $0.50 + (V^2 / (2 * g))$

Where:

$V = V(100)$ (fps)
 $g = 32.2$ ft/sec²

Supercritical Flow

FB = $1 + 0.025 * V * (d^{1/3})$

Where:

$V = V(100)$ (fps)
 $d = d(100)$ (ft)

Subcritical Flow

Se = $(C * V^2 * Tw) / (r * g)$

Where:

$C = 0.50$
 $V = V(100)$ (fps)
 $Tw =$ Top width of water on channel (ft)
 $r =$ radius (ft)
 $g = 32.2$ ft/sec²

Supercritical Flow

Se = $(C * V^2 * Tw) / (r * g)$

Where:

$C = 1.00$
 $V = V(100)$ (fps)
 $Tw =$ Top width of water on channel (ft)
 $r =$ radius (ft)
 $g = 32.2$ ft/sec²

Median Rock Size (d50) :

City of Sparks Hydrology Design Manual =

Equation 806

$d50 = (0.50 * V^2 * S^{0.34}) / (Sg - 1)^{1/3}$ 3332

Where:

$V = V(100)$ (fps)
 $S =$ Slope (ft/ft)
 $Sg =$ Specific Gravity of Rock (2.65 min)

Median Rock Size for Sleep Slopes (5.00% and greater) may also be determined by using Figures 812 ~ 816 of the City of Sparks Hydrology Design Manual
Reference Table 804 in the City of Sparks Hydrology Design Manual for Classification and Gradation of riprap.
All Class 150 rip rap is to be buried with native top soil and re-vegetated to protect from vandalism

Calculated Mannings n:

City of Sparks Hydrology Design Manual =

Equation 805

$n = 0.0395(d50)^{1/6}$

Where:

$d50 =$ from Table 804

Rock rip rap class	d50 (in)	Calculated n value	Depth of riprap placement (ft)
Class 150	6	0.035	1.00
Class 300	12	0.040	2.00
Class 400	16	0.041	2.67
Class 550	22	0.044	3.67
Class 700	28	0.045	4.67
Class 900	35	0.047	5.83

Equation 805 is not valid for grouted rock riprap or very shallow flow (i.e. hydraulic radius less than or equal to 2 times the maximum rock size)

* Instead of using traditional rip rap channel armor the contractor and/or developer may use a suitable Turf Reinforcement Mat (TRM) installed to the manufacturer's specifications and to the approval of the City of Reno Community Development Department.
PYRAMAT is a SI Geosolutions product and can be obtained through CONTECH Construction Products, Inc or ATTILA Environmental Products.

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=0.82% 5' Bottom Palisades
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.035
Channel Slope	008200 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	5.00 ft
Discharge	205.00 cfs

Results

Depth	2.82 ft
Flow Area	38.0 ft ²
Wetted Perim	22.84 ft
Top Width	21.93 ft
Critical Depth	2.41 ft
Critical Slope	0.016390 ft/ft
Velocity	5.40 ft/s
Velocity Head	0.45 ft
Specific Energ	3.27 ft
Froude Numb	0.72
Flow Type	Subcritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description	
Worksheet	S=5.90% 5' Bottom Palisade:
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Mannings Coeffc	0.040
Channel Slope	059000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	5.00 ft
Discharge	205.00 cfs

Results	
Depth	1.89 ft
Flow Area	20.2 ft ²
Wetted Perim	16.97 ft
Top Width	16.36 ft
Critical Depth	2.41 ft
Critical Slope	0.021412 ft/ft
Velocity	10.14 ft/s
Velocity Head	1.60 ft
Specific Energ	3.49 ft
Froude Numb	1.61
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=9.70% 5' Bottom Palisade:
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.044
Channel Slope	097000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	5.00 ft
Discharge	205.00 cfs

Results

Depth	1.76 ft
Flow Area	18.1 ft ²
Wetted Perim	16.12 ft
Top Width	15.55 ft
Critical Depth	2.41 ft
Critical Slope	0.025902 ft/ft
Velocity	11.35 ft/s
Velocity Head	2.00 ft
Specific Energ	3.76 ft
Froude Numb	1.86
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=2.74% 5' Bottom Palisades
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeff	0.035
Channel Slope	0.027400 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	5.00 ft
Discharge	205.00 cfs

Results

Depth	2.13 ft
Flow Area	24.3 ft ²
Wetted Perim	18.49 ft
Top Width	17.79 ft
Critical Depth	2.41 ft
Critical Slope	0.016390 ft/ft
Velocity	8.43 ft/s
Velocity Head	1.11 ft
Specific Energy	3.24 ft
Froude Number	1.27
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=5.27% 10' Bottom Palisade
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	0.052700 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft
Discharge	342.00 cfs

Results

Depth	2.00 ft
Flow Area	31.9 ft ²
Wetted Perim	22.62 ft
Top Width	21.97 ft
Critical Depth	2.56 ft
Critical Slope	0.020078 ft/ft
Velocity	10.72 ft/s
Velocity Head	1.79 ft
Specific Energ	3.78 ft
Froude Numb	1.57
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=9.01% 10' Bottom Palisade
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.044
Channel Slope	090100 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft
Discharge	342.00 cfs

Results

Depth	1.82 ft
Flow Area	28.2 ft ²
Wetted Perim.	21.53 ft
Top Width	20.93 ft
Critical Depth	2.56 ft
Critical Slope	0.024288 ft/ft
Velocity	12.13 ft/s
Velocity Head	2.29 ft
Specific Energy	4.11 ft
Froude Numb.	1.84
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=5.33% 10' Bottom Palisade
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	053300 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft
Discharge	342.00 cfs

Results

Depth	1.99 ft
Flow Area	31.8 ft ²
Wetted Perim _e	22.58 ft
Top Width	21.94 ft
Critical Depth	2.56 ft
Critical Slope	0.020079 ft/ft
Velocity	10.77 ft/s
Velocity Head	1.80 ft
Specific Energ _y	3.79 ft
Froude Numb _e	1.58
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=1 34% 10' Bottom Palisade
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeff	0.035
Channel Slope	013400 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft
Discharge	342.00 cfs

Results

Depth	2.65 ft
Flow Area	47.5 ft ²
Wetted Perim	26.74 ft
Top Width	25.88 ft
Critical Depth	2.56 ft
Critical Slope	0.015373 ft/ft
Velocity	7.20 ft/s
Velocity Head	0.81 ft
Specific Energ	3.45 ft
Froude Numb	0.94
Flow Type	Subcritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=2.24% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffc	0.040
Channel Slope	022400 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.27 ft
Flow Area	60.7 ft ²
Wetted Perim	26.63 ft
Top Width	25.09 ft
Critical Depth	3.44 ft
Critical Slope	0.018589 ft/ft
Velocity	9.63 ft/s
Velocity Head	1.44 ft
Specific Energ	4.71 ft
Froude Numb	1.09
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=1.46% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.035
Channel Slope	0.014600 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.41 ft
Flow Area	64.3 ft ²
Wetted Perim	27.27 ft
Top Width	25.66 ft
Critical Depth	3.44 ft
Critical Slope	0.014229 ft/ft
Velocity	9.09 ft/s
Velocity Head	1.28 ft
Specific Energ	4.70 ft
Froude Numb	1.01
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=1 92% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	019200 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.41 ft
Flow Area	64.1 ft ²
Wetted Perim	27.24 ft
Top Width	25.63 ft
Critical Depth	3.44 ft
Critical Slope	0.018594 ft/ft
Velocity	9.11 ft/s
Velocity Head	1.29 ft
Specific Energ	4.70 ft
Froude Numb	1.02
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=2.20% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	0.22000 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.29 ft
Flow Area	61.1 ft ²
Wetted Perim	26.70 ft
Top Width	25.15 ft
Critical Depth	3.44 ft
Critical Slope	0.018589 ft/ft
Velocity	9.56 ft/s
Velocity Head	1.42 ft
Specific Energ	4.71 ft
Froude Numb	1.08
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=3 33% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	033300 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	2.94 ft
Flow Area	52.7 ft ²
Wetted Perim	25.16 ft
Top Width	23.77 ft
Critical Depth	3.44 ft
Critical Slope	0.018589 ft/ft
Velocity	11.09 ft/s
Velocity Head	1.91 ft
Specific Energ	4.86 ft
Froude Numb	1.31
Flow Type	Supercritical

Worksheet
Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=2.63% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	0.26300 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.14 ft
Flow Area	57.3 ft ²
Wetted Perim	26.02 ft
Top Width	24.54 ft
Critical Depth	3.44 ft
Critical Slope	0.018589 ft/ft
Velocity	10.19 ft/s
Velocity Head	1.62 ft
Specific Enerç	4.75 ft
Froude Numb	1.18
Flow Type	supercritical

Worksheet
Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=2 17% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	021700 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.30 ft
Flow Area	61.4 ft ²
Wetted Perim	26.76 ft
Top Width	25.20 ft
Critical Depth	3.44 ft
Critical Slope	0.018590 ft/ft
Velocity	9.52 ft/s
Velocity Head	1.41 ft
Specific Energ	4.71 ft
Froude Numb	1.08
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=3.64% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	036400 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	2.87 ft
Flow Area	51.0 ft ²
Wetted Perim	24.85 ft
Top Width	23.50 ft
Critical Depth	3.44 ft
Critical Slope	0.018591 ft/ft
Velocity	11.45 ft/s
Velocity Head	2.04 ft
Specific Energ	4.91 ft
Froude Numb	1.37
Flow Type	Supercritical

Worksheet
Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=3.03% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	030300 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.02 ft
Flow Area	54.5 ft ²
Wetted Perim	25.50 ft
Top Width	24.08 ft
Critical Depth	3.44 ft
Critical Slope	0.018589 ft/ft
Velocity	10.72 ft/s
Velocity Head	1.79 ft
Specific Energ	4.81 ft
Froude Numb	1.26
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description	
Worksheet	S=5.56% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Mannings Coeffic	0.044
Channel Slope	0.055600 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results	
Depth	2.70 ft
Flow Area	47.0 ft ²
Wetted Perim	24.07 ft
Top Width	22.80 ft
Critical Depth	3.44 ft
Critical Slope	0.022496 ft/ft
Velocity	12.43 ft/s
Velocity Head	2.40 ft
Specific Energ	5.10 ft
Froude Numb	1.53
Flow Type	Supercritical

Worksheet
Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=2.31% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.040
Channel Slope	0.23100 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results

Depth	3.25 ft
Flow Area	60.0 ft ²
Wetted Perim	26.51 ft
Top Width	24.98 ft
Critical Depth	3.44 ft
Critical Slope	0.018585 ft/ft
Velocity	9.73 ft/s
Velocity Head	1.47 ft
Specific Enerç	4.72 ft
Froude Numb	1.11
Flow Type	supercritical

Worksheet
Worksheet for Trapezoidal Channel

Project Description	
Worksheet	S=1.68% 12' Bottom Golden Hill
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Mannings Coeffic	0.035
Channel Slope	016800 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	12.00 ft
Discharge	584.00 cfs

Results	
Depth	3.29 ft
Flow Area	61.1 ft ²
Wetted Perim	26.71 ft
Top Width	25.16 ft
Critical Depth	3.44 ft
Critical Slope	0.014233 ft/ft
Velocity	9.56 ft/s
Velocity Head	1.42 ft
Specific Energ	4.71 ft
Froude Numb	1.08
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description	
Worksheet	S=1.50% 22' Bottom Central
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Left Side Slope

Input Data	
Mannings Coeffic	0.035
Channel Slope	015000 ft/ft
Depth	2.72 ft
Right Side Slope	2.00 H : V
Bottom Width	22.00 ft
Discharge	695.00 cfs

Results	
Left Side Slop	3.82 H : V
Flow Area	81.5 ft ²
Wetted Perim	38.85 ft
Top Width	37.86 ft
Critical Depth	2.76 ft
Critical Slope	0.014259 ft/ft
Velocity	8.52 ft/s
Velocity Head	1.13 ft
Specific Energ	3.85 ft
Froude Numb	1.02
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description	
Worksheet	S=0.50% 22' Bottom Central
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Mannings Coeffic	0.035
Channel Slope	005000 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	22.00 ft
Discharge	695.00 cfs

Results	
Depth	3.83 ft
Flow Area	113.7 ft ²
Wetted Perim	39.14 ft
Top Width	37.33 ft
Critical Depth	2.87 ft
Critical Slope	0.014105 ft/ft
Velocity	6.11 ft/s
Velocity Head	0.58 ft
Specific Energ	4.41 ft
Froude Numb	0.62
Flow Type	Subcritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=1.00% 22' Bottom Central
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.035
Channel Slope	010000 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	22.00 ft
Discharge	695.00 cfs

Results

Depth	3.16 ft
Flow Area	89.4 ft ²
Wetted Perim	36.13 ft
Top Width	34.63 ft
Critical Depth	2.87 ft
Critical Slope	0.014104 ft/ft
Velocity	7.77 ft/s
Velocity Head	0.94 ft
Specific Enerç	4.10 ft
Froude Numb	0.85
Flow Type	Subcritical

Worksheet
Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=5.04% 22' Bottom Central
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffc	0.041
Channel Slope	050400 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	22.00 ft
Discharge	692.00 cfs

Results

Depth	2.18 ft
Flow Area	57.3 ft ²
Wetted Perim	31.73 ft
Top Width	30.70 ft
Critical Depth	2.86 ft
Critical Slope	0.019363 ft/ft
Velocity	12.07 ft/s
Velocity Head	2.26 ft
Specific Energ	4.44 ft
Froude Numb	1.56
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	S=4.56% 22' Bottom Central
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.041
Channel Slope	0.045600 ft/ft
Left Side Slope	2.00 H : V
Right Side Slope	2.00 H : V
Bottom Width	22.00 ft
Discharge	692.00 cfs

Results

Depth	2.24 ft
Flow Area	59.3 ft ²
Wetted Perim	32.01 ft
Top Width	30.96 ft
Critical Depth	2.86 ft
Critical Slope	0.019370 ft/ft
Velocity	11.67 ft/s
Velocity Head	2.12 ft
Specific Enerç	4.36 ft
Froude Numb	1.49
Flow Type	supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description	
Worksheet	S=6.71% 22' Bottom Central
Flow Element	Trapezoidal Channel
Method	Manning's Formula
Solve For	Channel Depth

Input Data	
Mannings Coeffic	0.044
Channel Slope	067100 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	22.00 ft
Discharge	692.00 cfs

Results	
Depth	2.03 ft
Flow Area	57.0 ft ²
Wetted Perim	34.83 ft
Top Width	34.17 ft
Critical Depth	2.75 ft
Critical Slope	0.022507 ft/ft
Velocity	12.14 ft/s
Velocity Head	2.29 ft
Specific Energ	4.32 ft
Froude Numb	1.66
Flow Type	Supercritical

CLASSIFICATION AND GRADATION OF LOOSE RIPRAP

RIPRAP CLASS DESIGNATION	% SMALLER THAN GIVEN SIZE BY WEIGHT	RIPRAP GRADATION (Inches)	d_{50}^* (Inches)
Class 150	100	10	6**
	35 - 50	6	
	0 - 15	2	
Class 300	100	20	12
	35 - 50	12	
	0 - 15	4	
Class 400	100	26	16
	35 - 50	16	
	0 - 15	6	
Class 550	100	37	22
	35 - 50	22	
	0 - 15	8	
Class 700	100	45	28
	35 - 50	28	
	0 - 15	10	
Class 900	100	57	35
	35 - 50	35	
	0 - 15	14	

* d_{50} = mean stone size

** Bury Class 150 riprap with native top soil and re-vegetate to protect from vandalism

VERSION: June 30, 1998

REFERENCE:

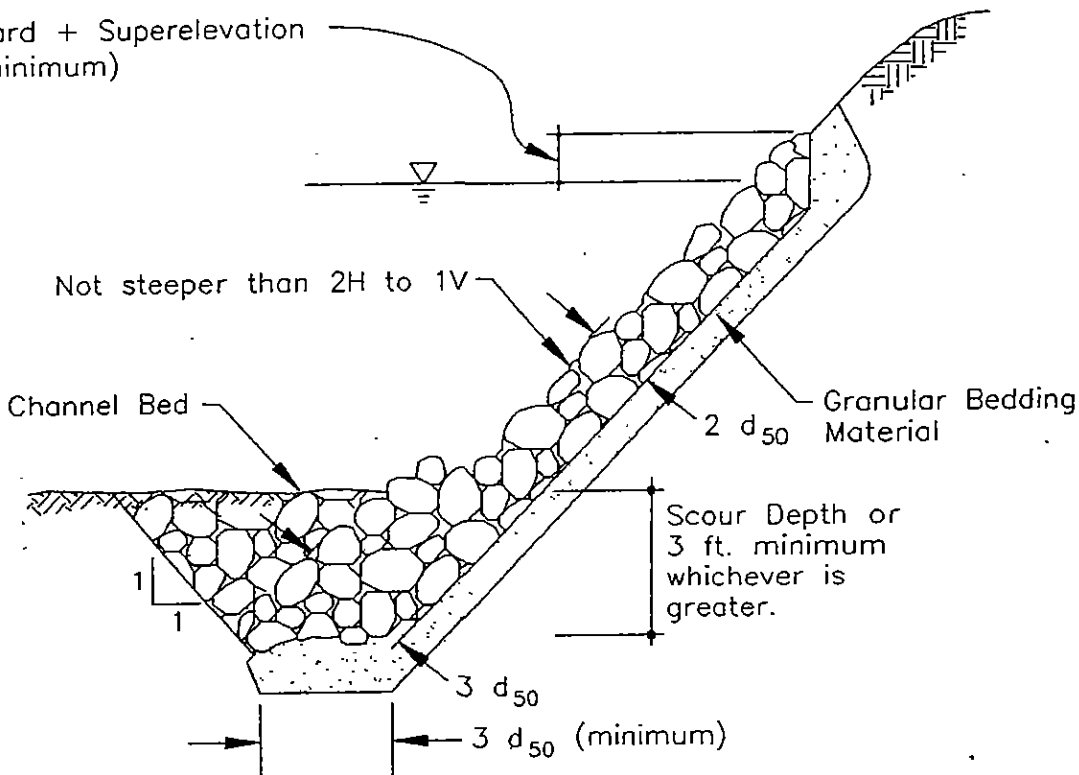
Draft, State of Nevada, Department of Transportation
Standard Specifications for Road and Bridge Construction,
 1996

TABLE
804

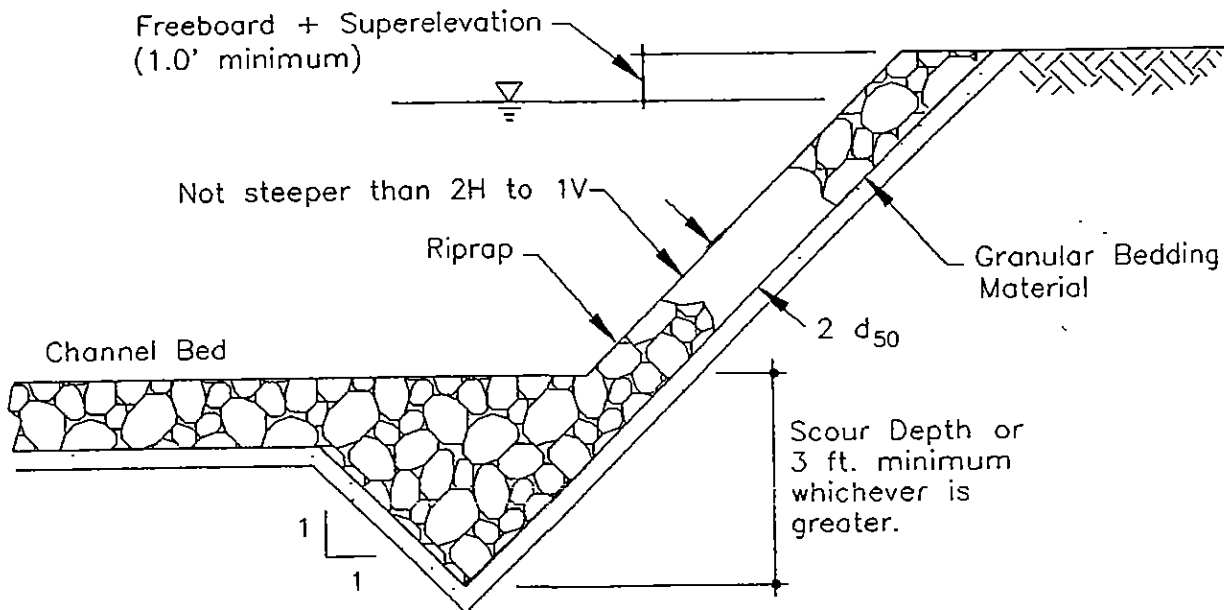


TYPICAL CROSS-SECTIONS FOR RIPRAP-LINED CHANNELS

Freeboard + Superelevation
 (1.0' minimum)



Freeboard + Superelevation
 (1.0' minimum)



1875, 1875&10 CWS, LCD, WRC7 P&P, 06-3-97, JUL

VERSION: July 31, 1998

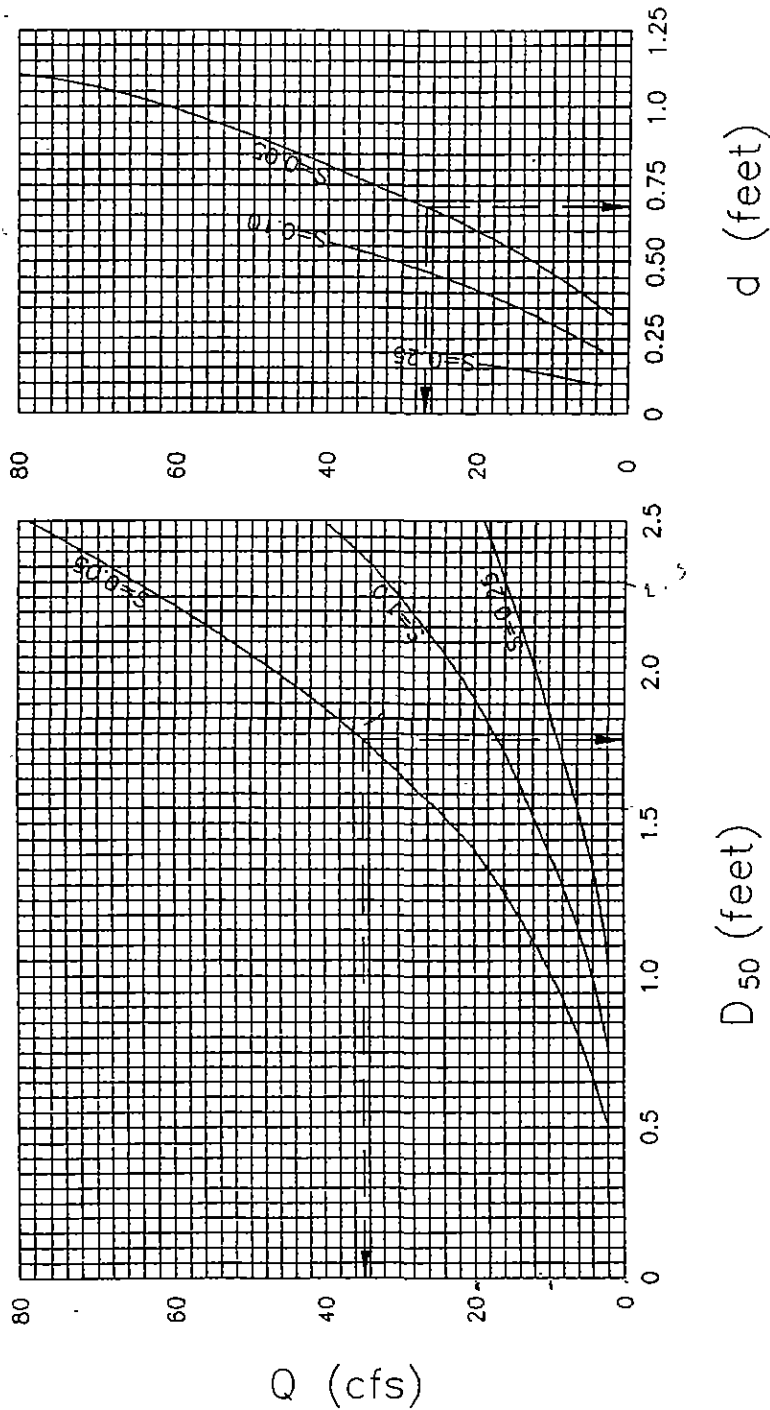
WRC NEVADA, INC

REFERENCE:

Modified from H.E.C. No. 11, USDOT, 1989

FIGURE
 810

STEEP SLOPE RIPRAP DESIGN, TRIANGULAR CHANNELS, 2:1 SIDESLOPES



WRC2.PCP 8-2-97 JH

VERSION: July 31, 1998

REFERENCE:

Simons, Li and Assoc.,
 1989

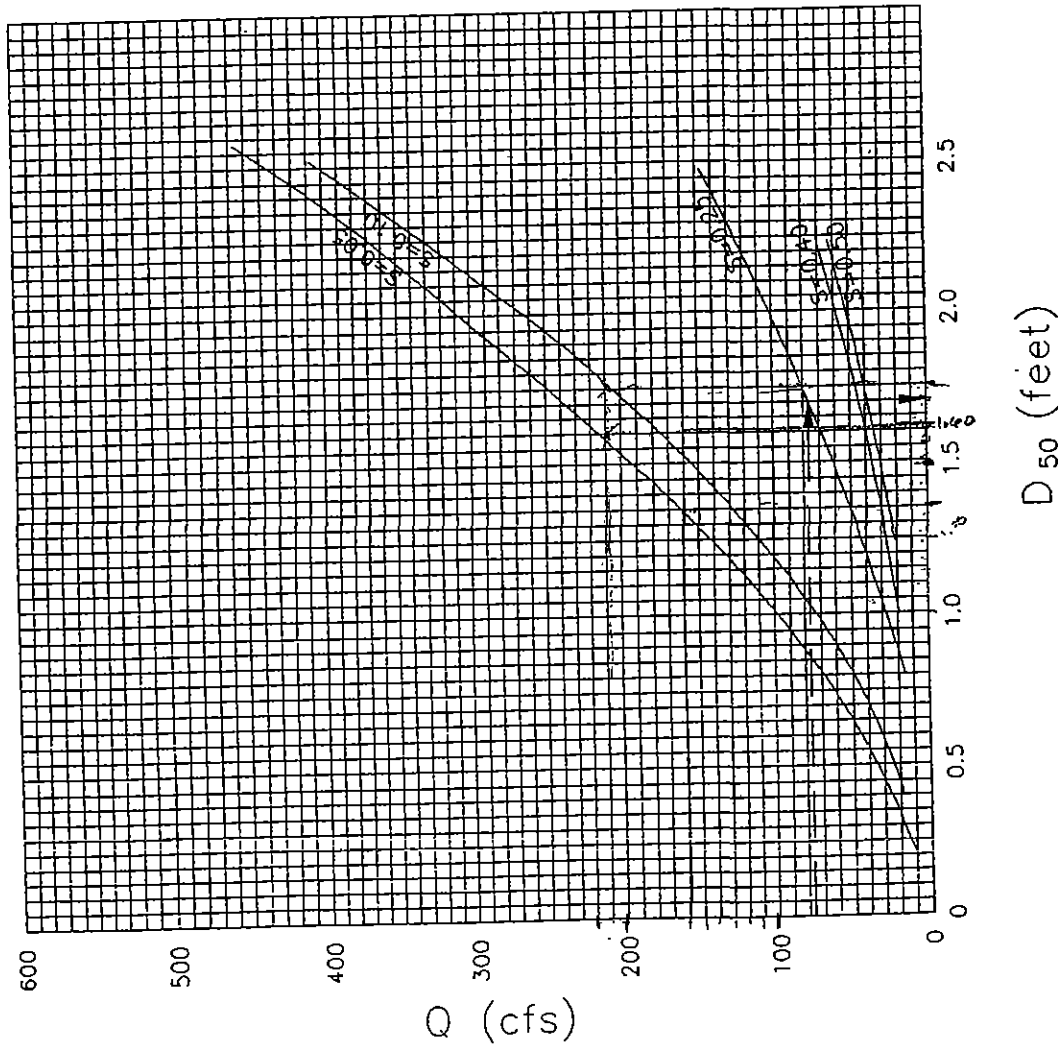
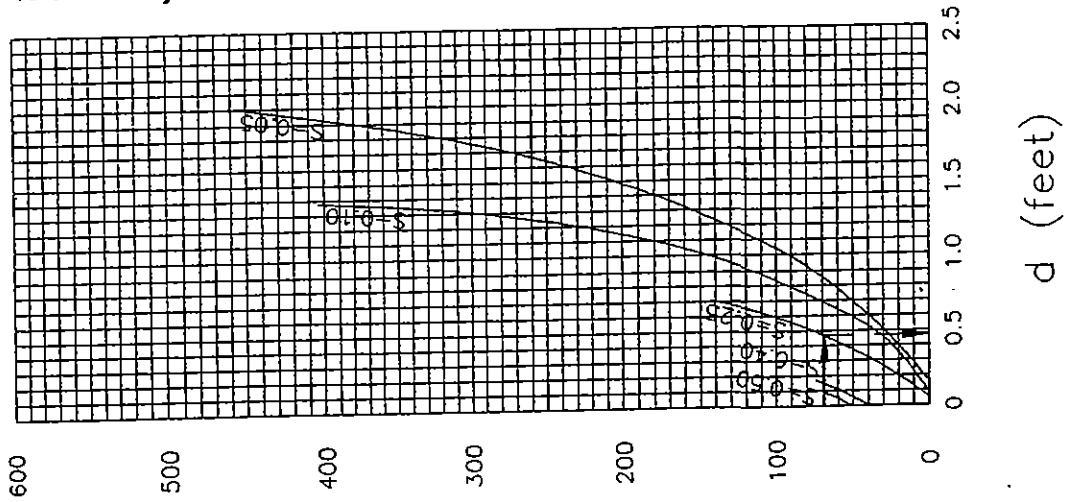
FIGURE

812

1876

WRC NEVADA, INC

STEEP SLOPE RIPRAP DESIGN, TRAPEZOIDAL CHANNELS, 2:1 SIDESLOPES, 6 FT BASE WIDTH



1876.1878813.DWG WRC2 PCP 8-2-97 JHJ

VERSION: July 31, 1998

WRC NEVADA, INC

REFERENCE:

Simons, Li and Assoc.,
 1989

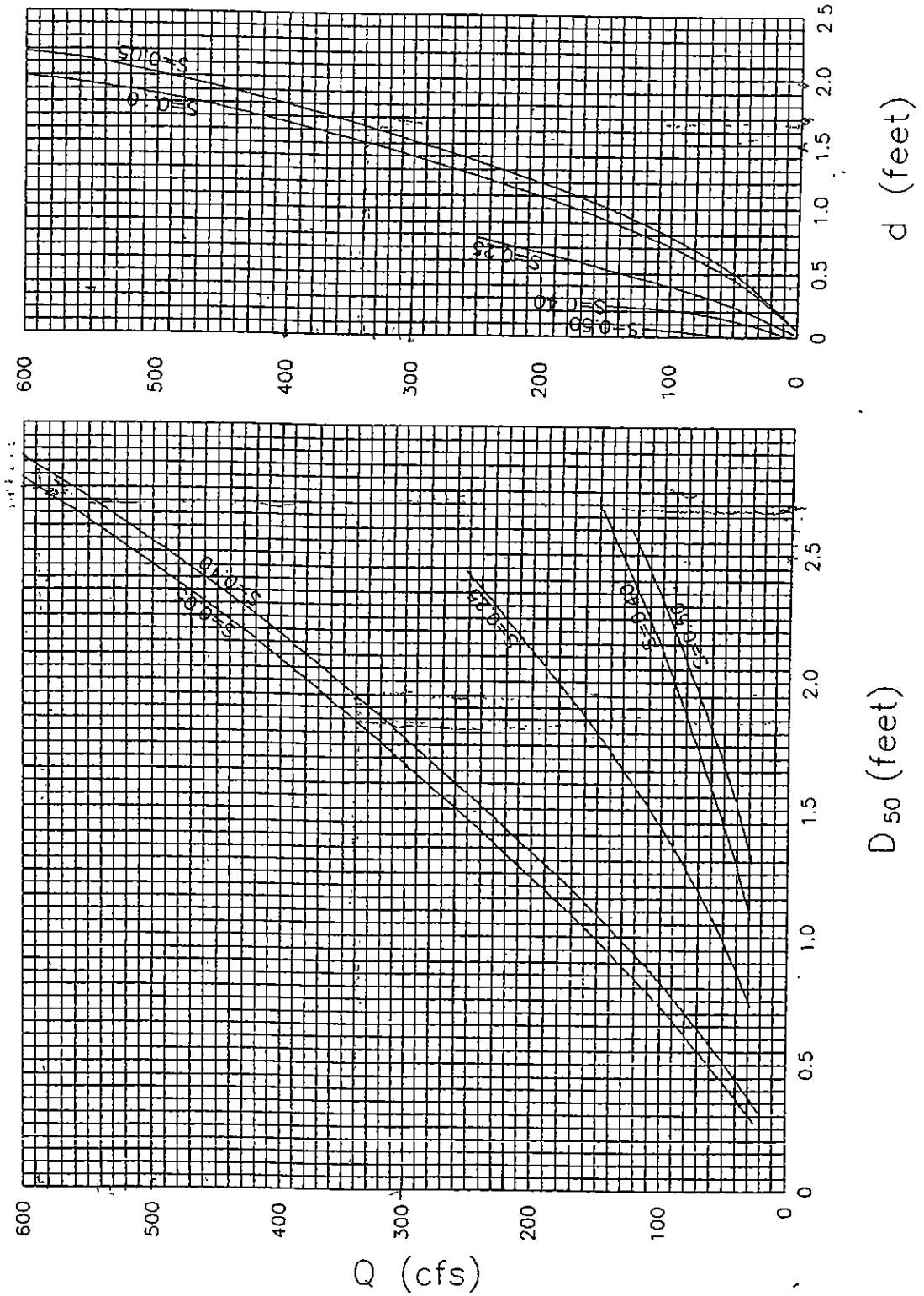
FIGURE

813

CITY OF SPARKS

HYDROLOGIC CRITERIA AND DRAINAGE DESIGN MANUAL

STEEP SLOPE RIPRAP DESIGN, TRAPEZOIDAL CHANNELS, 2:1 SIDESLOPES, 10 FT BASE WIDTH



VERSION: July 31, 1998

WRC NEVADA, INC

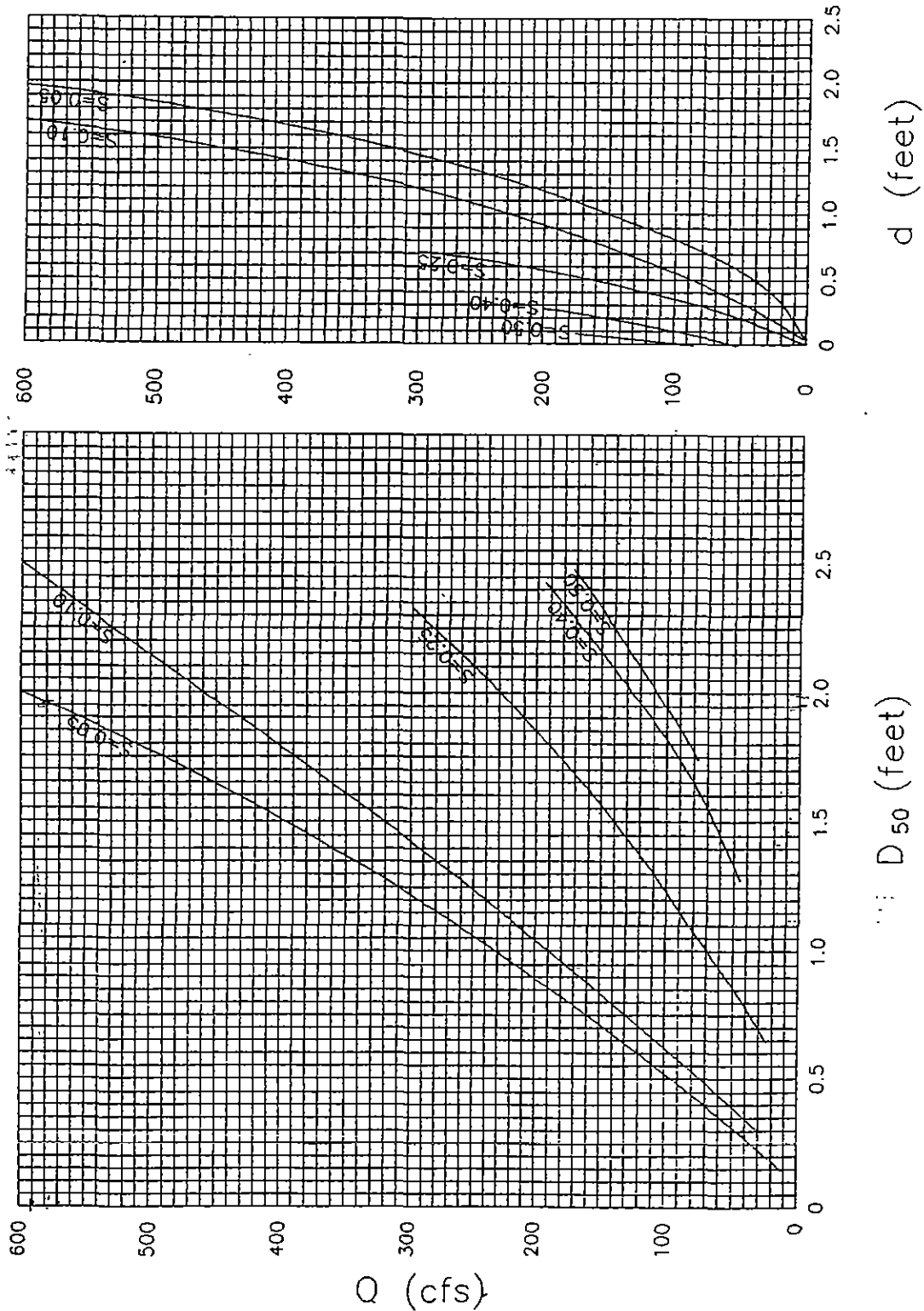
REFERENCE:

Simons, Li and Assoc.,
1989

FIGURE

814

STEEP SLOPE RIPRAP DESIGN, TRAPEZOIDAL CHANNELS, 2:1 SIDESLOPES, 14 FT BASE WIDTH



187A, 187A15.DWG, WRC2, PCC, 6-2-97, JLN

VERSION: July 31, 1998

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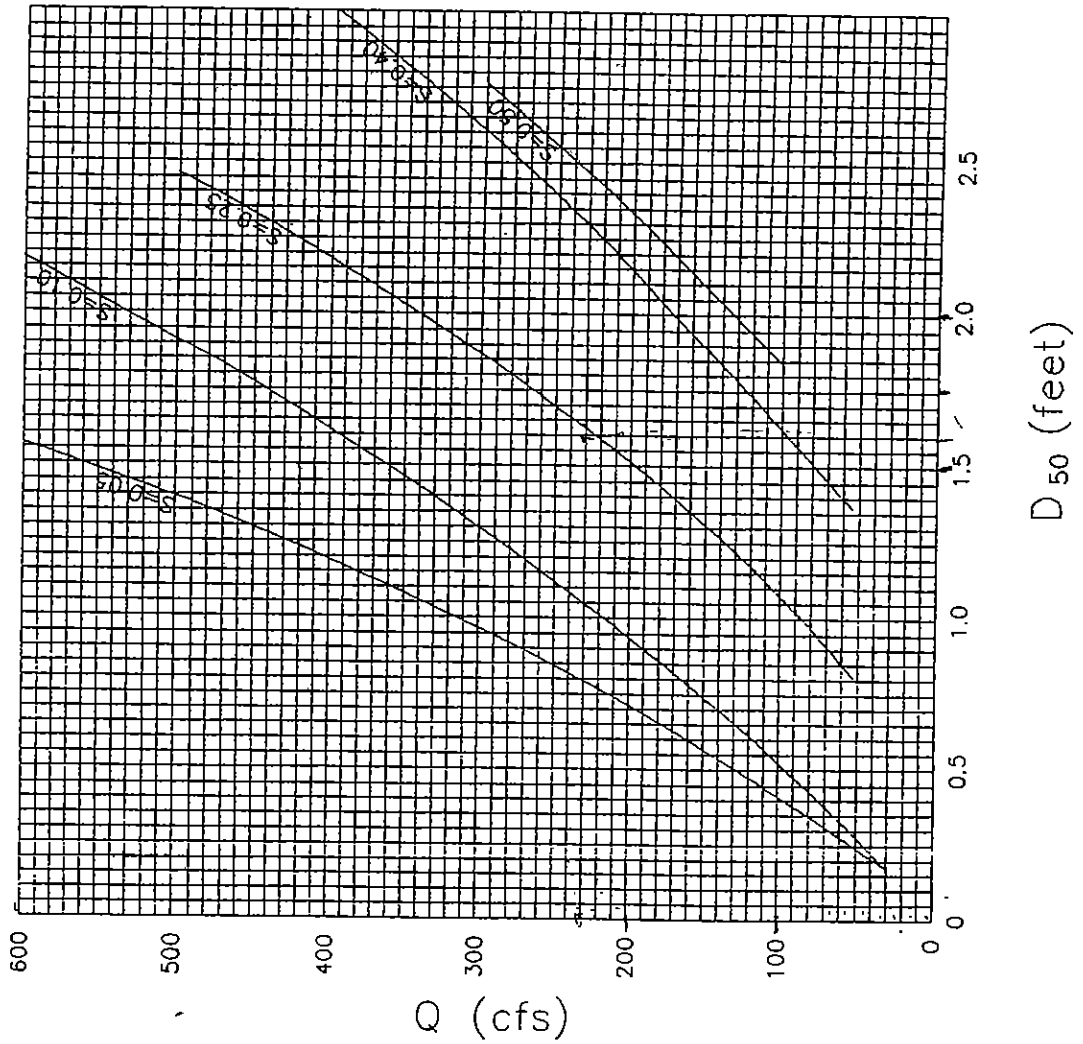
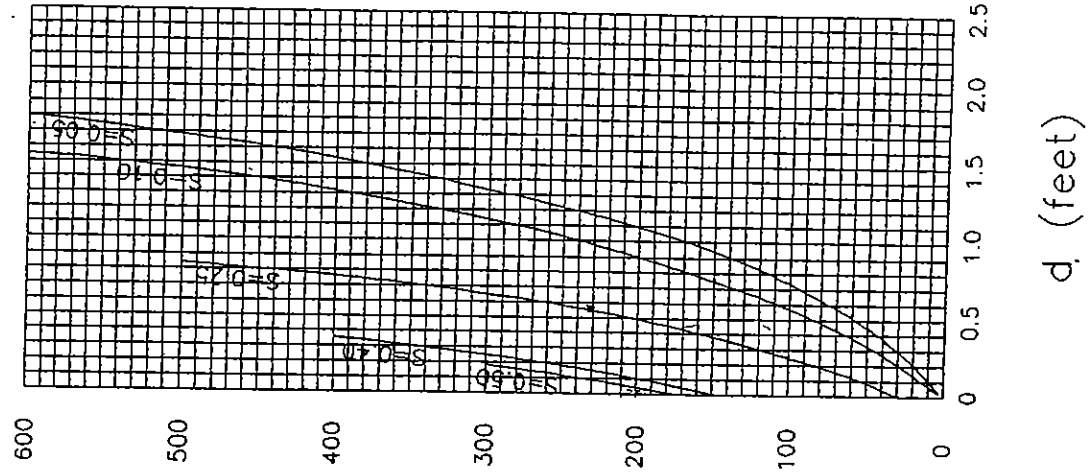
REFERENCE:

Simons, Li and Assoc.,
 1989

FIGURE

815

STEEP SLOPE RIPRAP DESIGN, TRAPEZOIDAL CHANNELS, 2:1 SIDESLOPES, 20 FT BASE WIDTH



1878, 1070016 DMC WRC7.PCP 6-3-97 JKH

VERSION: July 31, 1998
 WRC NEVADA, INC

REFERENCE:
 Simons, Li and Assoc.,
 1989

FIGURE
 816

Culvert Calculator Report

Dual 10x4 Box Culvert at CP6 - 100-year Storm Event

Comments: This analysis includes 1' of additional freeboard. discharge was obtained from Storm Drainage Master Plan by Wood Rodgers, Inc March, 2005.

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	4,463.00 ft	Headwater Depth/Height	1.41
Computed Headwater Elev:	4,461.64 ft	Discharge	695.00 cfs
Inlet Control HW Elev.	4,461.64 ft	Tailwater Elevation	4,458.40 ft
Outlet Control HW Elev.	4,461.36 ft	Control Type	Inlet Control

Grades			
Upstream Invert	4,456.00 ft	Downstream Invert	4,454.55 ft
Length	270.80 ft	Constructed Slope	0.005 ft/ft

Hydraulic Profile			
Profile	CompositeS1S2	Depth, Downstream	2.96 ft
Slope Type	Steep	Normal Depth	2.96 ft
Flow Regime	N/A	Critical Depth	3.35 ft
Velocity Downstream	11.74 ft/s	Critical Slope	0.004 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.014
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	4,461.36 ft	Upstream Velocity Head	1.67 ft
Ke	0.20	Entrance Loss	0.33 ft

Inlet Control Properties			
Inlet Control HW Elev.	4,461.64 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	80.0 ft²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Culvert Calculator Report

Dual 10x4 Box Culvert at CP6 - Capacity

Comments: This analysis is based on flow at the maximum water elevation before over topping the roadway

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	4,464.00 ft	Headwater Depth/Height	2.00
Computed Headwater Elev.	4,464.00 ft	Discharge	981.95 cfs
Inlet Control HW Elev	4,464.00 ft	Tailwater Elevation	4,458.40 ft
Outlet Control HW Elev.	4,463.61 ft	Control Type	Inlet Control

Grades			
Upstream Invert	4,456.00 ft	Downstream Invert	4,454.55 ft
Length	270.80 ft	Constructed Slope	0.005 ft/ft

Hydraulic Profile			
Profile	PressureProfile	Depth, Downstream	4.00 ft
Slope Type	N/A	Normal Depth	N/A ft
Flow Regime	N/A	Critical Depth	4.00 ft
Velocity Downstream	12.27 ft/s	Critical Slope	0.008 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.014
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	4,463.61 ft	Upstream Velocity Head	2.34 ft
Ke	0.20	Entrance Loss	0.47 ft

Inlet Control Properties			
Inlet Control HW Elev.	4,464.00 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	80.0 ft ²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Culvert Calculator Report

Dual 10x4 Box Culvert at CP7 - 100-year Storm Event

Comments This analysis includes 1' of additional freeboard, discharge was obtained from Storm Drainage Master Plan by Wood Rodgers, Inc March, 2005.

Solve For Headwater Elevation

Culvert Summary			
Allowable HW Elevation	4,473.21 ft	Headwater Depth/Height	1.40
Computed Headwater Elev.	4,473.20 ft	Discharge	692.00 cfs
Inlet Control HW Elev.	4,473.20 ft	Tailwater Elevation	4,466.86 ft
Outlet Control HW Elev.	4,472.93 ft	Control Type	Inlet Control
Grades			
Upstream Invert	4,467.59 ft	Downstream Invert	4,466.86 ft
Length	73.49 ft	Constructed Slope	0.010 ft/ft
Hydraulic Profile			
Profile	S2	Depth, Downstream	2.66 ft
Slope Type	Steep	Normal Depth	2.38 ft
Flow Regime	Supercritical	Critical Depth	3.34 ft
Velocity Downstream	13.03 ft/s	Critical Slope	0.004 ft/ft
Section			
Section Shape	Box	Mannings Coefficient	0.014
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		
Outlet Control Properties			
Outlet Control HW Elev.	4,472.93 ft	Upstream Velocity Head	1.67 ft
Ke	0.20	Entrance Loss	0.33 ft
Inlet Control Properties			
Inlet Control HW Elev.	4,473.20 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	80.0 ft²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Culvert Calculator Report

Dual 10x4 Box Culvert at CP7 - Capacity

Comments: This analysis is based on flow at the maximum water elevation before over topping the roadway.

Solve For: Discharge

Culvert Summary			
Allowable HW Elevation	4,474.21 ft	Headwater Depth/Height	1.66
Computed Headwater Elev:	4,474.21 ft	Discharge	827.53 cfs
Inlet Control HW Elev.	4,474.21 ft	Tailwater Elevation	4,466.86 ft
Outlet Control HW Elev.	4,473.61 ft	Control Type	Inlet Control

Grades			
Upstream Invert	4,467.59 ft	Downstream Invert	4,466.86 ft
Length	73.49 ft	Constructed Slope	0.010 ft/ft

Hydraulic Profile			
Profile	S2	Depth, Downstream	3.03 ft
Slope Type	Steep	Normal Depth	2.69 ft
Flow Regime	Supercritical	Critical Depth	3.76 ft
Velocity Downstream	13.67 ft/s	Critical Slope	0.004 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.014
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	4,473.61 ft	Upstream Velocity Head	1.88 ft
Ke	0.20	Entrance Loss	0.38 ft

Inlet Control Properties			
Inlet Control HW Elev.	4,474.21 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	80.0 ft ²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Appendix F
Storm Drainage Master Plan
(Wood Rodgers, Inc. March 2005)

STORM DRAINAGE MASTER PLAN
Golden Hills Subdivision / Damonte Foothills
Project # 1452.002
Section 14 of T18N, R20E MDM
Washoe County, Nevada

Prepared for:
Reynen & Bardis Development, LLC
1380 Greg Street, Suite 230
Sparks, NV 89431

March 28, 2005

Prepared by:
Mary Horvath, P.E.

Mark Gookin, P.E.



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FOR REVIEW ONLY

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TABLE OF CONTENTS

1.0	Introduction	2
1.1	Project Location.....	2
1.2	Regulatory Perspective	2
1.3	Previous Studies.....	3
2.0	Hydrologic Analysis	4
2.1	Design Rainfall	4
2.2	Existing Conditions.....	4
2.2.1	Drainage Subdrainage areas	4
2.2.2	Runoff Computation.....	4
2.2.3	Stormwater Routing.....	5
2.2.4	Existing Conditions Results	5
2.3	Proposed Conditions	6
2.3.1	Drainage Subdrainage areas	6
2.3.2	Runoff Computation.....	6
2.3.3	Stormwater Routing.....	7
2.3.4	Proposed Conditions Results.....	8
3.0	Proposed Drainage Facilities	10
3.1	Storm drains	10
3.2	Channels.....	10
3.3	Culverts.....	10
3.4	Maintenance Issues	10
4.0	Conclusion	11

LIST OF TABLES

Table 1: 5- and 100-Year Precipitation Depths.....	4
Table 2: Existing Conditions Runoff Parameters.....	5
Table 3: Existing Conditions Runoff Results.....	5
Table 4: Proposed Conditions Runoff Parameters	7
Table 5: Proposed Conditions Runoff Results	9
Table 6: Preliminary Channel Parameters.....	10
Table 7: Peak Flow Results.....	11

LIST OF FIGURES

- Figure 1: Vicinity Map
- Figure 2: Existing conditions Subdrainage area Delineation
- Figure 3: Proposed conditions Subdrainage area Delineation
- Figure 4: Preliminary Drainage Facilities

APPENDICES

- A: Runoff Computation
 - Precipitation Data
 - Time of Lag Calculations
 - Curve number Calculation
 - Soil types
- B: Drainage Facilities
 - Channel design
 - Culvert Design
- C: Existing Conditions HEC-1 model output: 5- and 100-year
- D: Proposed Conditions HEC-1 model output: 5- and 100-year

1.0 INTRODUCTION

This report presents the Master Drainage Plan for the Damonte Foothill Development, which encompasses the construction of three proposed subdivisions: Golden Hills, the Palisades and McCauley Ranch. The purpose of this report is to address the drainage issues off- and on-site that result from development of the property in accordance with Washoe County and City of Reno regulations. This report includes the overall hydrologic analyses for existing conditions, proposed conditions with the Damonte Foothills development, and general design parameters for on-site flood control facilities. The proposed facilities presented in this report are preliminary as the current design of the subdivisions is preliminary. This master drainage report is meant to establish the overall feasibility of the development with respect to flood control and the potential effects on the downstream properties and to provide general guidance for the design of the drainage facilities within the subdivisions. The final development of each subdivision will need to include additional hydraulic and hydrologic analysis and a more detailed drainage report. As the final design progresses, the detailed analysis for each subdivision will be reviewed by Wood Rodgers, Inc. to ensure conformance with the hydrologic master plan.

1.1 PROJECT LOCATION

The proposed Damonte Foothills Development study site covers approximately 365 acres within both the City of Reno and unincorporated Washoe County within the City of Reno sphere of influence. It is within Section 14 of Township 14 North, Range 20 East and it lies adjacent to and east of the Damonte Ranch development currently under construction. Please see Figure 1: Vicinity Map.

At present, the site is undisturbed rangeland with a vegetative cover of shrub/brush with areas of less dense grass/shrub in the southern portion. Approximately 4.7 square miles of undeveloped land to the east, southeast and northeast drain to the site in semi-defined channels that become unconcentrated shallow flow as they enter the site. Offsite slopes range from 5 to 20% and onsite slopes range from 5 to 20% along the eastern boundary and 3 to less than 1% along the western property boundary. Runoff in the southern portion of the site flows to a constructed channel along the boundary of the Damonte Ranch High School which outlets to a culvert beneath Desert Way and flows to the west to a channel constructed as part of Damonte Ranch. Runoff in the northern portion of the site flows to the western boundary to flow over Desert Way into a constructed channel that flows north and turns west to flow beneath culverts under Rio Wrangler Parkway.

1.2 REGULATORY PERSPECTIVE

The Damonte Foothills development is subject to the regulations of the City of Reno.

1.3 PREVIOUS STUDIES

The proposed subdivision is located just east of the Damonte Ranch development. Nimbus Engineers prepared a Master Drainage Report for Damonte Ranch and the Double Diamond Ranch and a CLOMR to change the floodplain boundaries of Steamboat Creek. These reports: Southeast Truckee Meadows Flood Control Master Plan (Nimbus, 1995) and Application for Conditional Letter of Map Revision (Nimbus, 2001) provided the hydrologic and hydraulic analysis and regional flood control design for the south Meadows area. The hydrologic analysis included the area covered by the proposed Damonte Foothills development as offsite flow; it was considered undeveloped in both existing and proposed conditions. The flood control facilities in the design of the Damonte Ranch and Double Diamond projects do not mitigate any increase in peak flow rates or volumes from the Damonte Foothills developments. However, the final concentration point at the northern boundary of Damonte Ranch to which the Damonte Foothills will contribute has a post-development peak flow that is much less than existing conditions.

The Damonte Foothills Boulevard is currently in design. A drainage study (Wood Rodgers, Inc., 2005) was prepared detailing the current conditions of the Damonte Ranch High School channel and the preliminary design of the proposed culverts that will convey the flow within the channel beneath the proposed road.

2.0 HYDROLOGIC ANALYSIS

2.1 DESIGN RAINFALL

The design rainfall was obtained from the NOAA 14 semi-arid southwest precipitation study for the 24-hour 5- and 100-year events. Table 1 contains the depths utilized in both the existing and proposed conditions hydrology models.

Table 1: 5- and 100-Year Precipitation Depths

Storm Event	Precipitation Depths (inches)			
	1-Hour	6-Hour	12-Hour	24-Hour
5-Year	0.56	1.20	1.68	2.25
100-Year	1.29	1.93	2.87	4.14

2.2 EXISTING CONDITIONS

Currently, runoff from several large drainage areas flows from the east to the eastern property boundary in concentrated or semi-concentrated drainages. As the drainages hit the shallow slopes and highly to semi-highly vegetated land on the proposed site, flow disperses into shallow wide flowpaths. Runoff leaves the property to the west. As part of the Damonte Ranch development, large trapezoidal earthen channels have been constructed to accept the flow from the site. One channel borders the Damonte Ranch High school to convey flows west to a culvert beneath Rio Wrangler Parkway and to a detention basin constructed as part of Damonte Ranch. A second channel runs along the western side of Desert Way to flow west to join the outlet of the detention basin.

2.2.1 Drainage Subdrainage areas

To analyze existing flow conditions, five existing drainage areas were delineated encompassing offsite and onsite areas. Please see Figure 2: Existing Conditions Drainage area Delineation.

Drainage area EX1 concentrates along the northern boundary of the property. Drainage area EX2 concentrates at the western property boundary and includes the northern portion of the site. Drainage area EX3 concentrates near the middle of the western boundary of the site and includes a large upstream offsite drainage area. Drainage area EX4 concentrates along the western boundary to flow to the pre-Damonte Ranch homes along Desert Way. Drainage area EX5 concentrates along the southern portion of the western boundary at what is now the channel bounding the high school.

2.2.2 Runoff Computation

We calculated the 5- and 100-year runoff hydrographs with precipitation depths taken from NOAA Atlas 14 and the SCS rainfall runoff and unit hydrograph methods in HEC-1 according to the methods outlined in the Washoe County Hydrologic Criteria and Drainage Design Manual. On-site topographic mapping was based on the aerial survey generated for this project with 1-ft contour interval and off-site topographic mapping was based on USGS 20-foot contours. Soil types were determined from NRCS Southern

Washoe County Soil Survey maps and vegetation cover was determined from aerial photos and site visits. Please see Table 2 for existing conditions runoff parameters and Appendix A for runoff computation.

Sub Drainage area	Area (acres)		Soil Data (acres)			L ₁ (mile)	L ₂ (mile)	S (ft/mile)	CN	K _n	T _{AG} (hours)
	Off-site	On-site	B	C	D						
EX1	1107	0	13	0	1094	3.4	2.4	1178	81.8	0.09	1.21
EX2	295	129	36	22	366	1.7	0.8	600	74.6	0.09	0.80
EX3	1421	49	119	4	1347	3.1	1.4	474	80.3	0.09	1.36
EX4	119	68	13	0	174	1.5	0.9	819	80.5	0.09	0.74
EX5	74	119	0	32	161	1.2	0.5	1200	82.1	0.09	0.51

Table 2: Existing Conditions Runoff Parameters

2.2.3 Stormwater Routing

The Muskingum Cunge routing subroutine was utilized within HEC-1 to simulate flood routing. Existing conditions drainage areas were routed according to the current channel configuration constructed as part of Damonte Ranch. The channel along Desert Way intercepts runoff from drainage areas EX1 through EX4. Drainage area EX4 was routed with a wide shallow channel from its outlet at the western property boundary to simulate its overland flow through the pre-Damonte Ranch properties. It was then routed to the concentration of drainage area EX3 with the channel configuration of the trapezoidal channel along Desert Way where it was added to runoff from drainage area EX3. Drainage areas EX3 and EX4 were then routed with the trapezoidal channel along Desert Way to the northwest property boundary where it was added to runoff from drainage areas EX1 and EX2 for the final concentration point at this location. Drainage area EX5 was not routed.

2.2.4 Existing Conditions Results

In northwest corner of the property, the final concentration point for runoff from drainage areas 1 through 4, the HEC-1 models compute a peak of 419 cfs in the 5-year event and 1354 cfs in the 100-year event. A peak of 54 cfs is generated in the 5-year event and 195 cfs in the 100-year event for drainage area 5 concentrating in the channel bordering the high school property. Table 3 shows the peak flows and times of peak computed by the existing conditions HEC-1 models.

Table 3: Existing Conditions Runoff Results

Sub Drainage area	5 Year		100 Year	
	Q _p (cfs)	T _p (hours)	Q _p (cfs)	T _p (hours)
EX1	172	13.4	579	13.3
EX2	45	12.9	228	12.9
EX3	188	13.5	515	13.4
EX4	37	12.8	139	12.8
EX5	54	12.6	195	12.6

2.3 PROPOSED CONDITIONS

The goal of the master drainage plan is to perpetuate existing drainage patterns and to mitigate any flow increase to at or below pre-development levels for the two design storms. The SCS runoff and hydrograph methods were used within the HEC-1 model to simulate the 5- and 100-year runoff from the development as described in the Washoe County Hydrologic Criteria and Drainage Design Manual. We then sized a preliminary detention basin for the southern portion of the site to mitigate the increase in runoff caused by development so that the channel bordering the high school will not experience an increase in peak flows. This detention basin design is solely for the purpose of demonstrating that mitigation of peak flows within the southern portion of Damonte Foothills is possible. The detention basin location and size may change in final design.

2.3.1 Subdrainage areas

The subdrainage areas are outlined in Figure 3, Proposed Conditions Drainage area Delineation. The offsite drainage areas correspond to the existing conditions drainage areas with additional divisions to aid in the design of drainage facilities. Onsite drainage areas were delineated according to proposed drainage facility locations and downstream routing. Please see Figure 3: Proposed Conditions Subwatershed Delineation.

Drainage area OFF1 is identical to existing conditions drainage area EX1, concentrating along the northern boundary of the site. Offsite drainage areas OFF2 through OFF4 concentrate near the northeast corner of the site. Runoff from OFF1 through OFF4 will be collected by a trapezoidal channel running along the north boundary of the site that will discharge to a culvert beneath Desert Way. Onsite drainage areas DEV1 through DEV4 will also discharge to the boundary channel. Onsite drainage area DEV5 will drain directly to the Damonte Ranch channel along Desert Way through a culvert.

Offsite drainage area OFF5 corresponds to existing conditions drainage area 3. It will be collected by a channel that will run through the middle of the site, which will also collect runoff from OFF 6 and onsite drainage areas DEV6 through DEV10.

Runoff from offsite drainage areas DEV7 and DEV8 concentrates near the southeast boundary of the site. Offsite drainage area OFF7 will flow through onsite drainage area 12. Runoff from OFF7 and DEV12 will be collected in a channel to be routed through onsite drainage areas DEV11 and DEV13 to the Damonte Ranch bordering the high school. Runoff from offsite drainage area DEV8 will flow through DEV12. Runoff from DEV12 will drain directly to the high school boundary channel.

2.3.2 Runoff Computation

The Washoe County hydrologic methodology was utilized to compute proposed runoff using the SCS loss and hydrograph methodologies. Offsite runoff coefficients were based on soil data obtained from the NRCS Southern Washoe County Soil Maps and

observed vegetation cover. Onsite drainage area coefficients were based on proposed residential density and the Southern Washoe County Soil Survey. Runoff coefficients and lag times were computed using methodology described in the Washoe County Hydrologic Criteria and Drainage Design Manual. Please see Table 4 for proposed conditions runoff parameters and Appendix A for runoff computation.

Table 4: Proposed Conditions Runoff Parameters

Sub Drainage area											
	(acres)		B	C	D	(mile)	(mile)	(ft/mile)			(hours)
OFF1	1107		13	0	1094	3.3	2.4	1178	81.8	0.09	1.21
OFF2	111		0	0	111	1.2	0.7	1934	82	0.09	0.54
OFF3	51		0	0	51	0.6	0.3	1302	82	0.09	0.33
OFF4	133		0	0	132	1.0	0.6	2195	82	0.09	0.48
OFF5	1422		21	0	1331	3.4	1.9	529	80.7	0.09	1.32
OFF6	119		0	0	119	1.0	0.5	1396	82	0.09	0.46
OFF7	60		0	0	60	0.5	0.3	1796	82	0.09	0.31
OFF8	15		0	1	15	0.3	0.1	2212	81.4	0.09	0.14
Sub Drainage area											
	(acres)	(ac/house)	B	C	D	(feet)	(ft/ft)		(%)		(hours)
DEV1	7	0.46	0	7	0	1160	0.001	80.2	8.9	0.78	0.16
DEV2	61	0.41	32	9	20	4144	0.026	77.1	11.5	0.78	0.25
DEV3	46	0.59	3	0	43	3516	0.047	83.5	11.1	0.78	0.17
DEV4	15	0	0	0	15	1694	0.062	82.0	0	0.78	0.14
DEV5	6	0.32	0	6	0	870	0.013	81.0	13.5	0.78	0.11
DEV6	3	0	1	2	0	965	0.015	72.0	0	0.78	0.11
DEV7	15	0.73	14	0	1	1945	0.054	70.1	6.8	0.78	0.17
DEV8	8	1.52	3	0	5	1371	0.077	76.6	10.2	0.78	0.07
DEV9	41	0.37	25	0	16	2340	0.056	75.5	12.0	0.78	0.11
DEV10	61	1.52	0	0	61	2585	0.162	84.0	7.3	0.78	0.07
DEV11	21	0.41	0	11	10	967	0.124	82.9	13.0	0.78	0.05
DEV12	22	1.84	0	0	22	1098	0.164	84.0	2.5	0.78	0.04
DEV13	58	0.48	1	20	37	3834	0.164	83.2	11.0	0.78	0.11

2.3.3 Stormwater Routing

The Muskingum Cunge subroutine was utilized within HEC-1 to simulate routing within the proposed conditions runoff models. In the northern portion of the site runoff from OFF4 is routed within a proposed trapezoidal channel along the eastern boundary of DEV3. Runoff from OFF 3 collects in this channel as well, but because it is such a short reach, it is not routed within HEC-1. CP4 concentrates runoff from OFF3, OFF4 and DEV 4. Runoff collecting at CP4 is routed to CP3 within a trapezoidal channel. Runoff from DEV3 and DEV4 is collected at CP3 without routing. Runoff from CP3 is then routed to CP1 in the continuation of the trapezoidal channel that discharges to the northwest corner of the property to cross beneath Desert Way in a culvert. Runoff from DEV1 and DEV2 also collects at this location.

In the center portion of the site, runoff from OFF6 is collected in a trapezoidal channel that runs through onsite drainage area DEV10. It flows to DEV8 where it co-mingles

with runoff from DEV5 and flows west in a constructed trapezoidal channel. CP8 collects this flow and runoff from DEV8 and DEV10. CP8 is routed to CP7 in the continuation of the channel where it co-mingles with runoff from DEV7 and DEV9. CP7 is then routed to CP6 where runoff from DEV6 also concentrates. This flow then crosses Desert Way in a culvert and flows within the Damonte Ranch channel to join flow from CP1 across the street from the northwest corner of the site. Runoff from onsite drainage area DEV5 crosses the street in a culvert and is routed in the Damonte Ranch channel to this corner as well. This concentration is directly comparable to existing conditions CP1.

In the southern portion of the site runoff from offsite drainage area OFF7 is routed through onsite drainage area DEV12 in a trapezoidal channel to the outlet of DEV12 (CP12). This flow is routed to CP11 in a trapezoidal channel where it joins runoff from DEV11. It is preliminarily proposed for this Master Drainage Plan that a detention basin be constructed at this location to detain this flow and mitigate the increase in peak flow that concentrates within the boundary channel along the high school. Flow exiting the detention basin would be routed to the high school channel in a trapezoidal channel. Runoff from DEV13 drains directly into the high school channel. Runoff from the small offsite drainage area OFF8 drains through DEV11 and DEV13 to co-mingle with the onsite runoff within these drainage areas and be collected within the proposed stormdrains to outlet to the proposed channels. The proposed conditions HEC-1 models were also run without detention in the southern portion of the site.

2.3.4 Proposed Conditions Results

The 5-year proposed conditions HEC-1 model computes a peak flow of 385 cfs at CP1 after the flow from the central portion of site is added. The 100-year model predicts a peak of 1274 cfs. Both of these peak flows are less than existing conditions. Although this seem counter-intuitive as the proposed conditions will increase impervious area and resulting runoff volumes, it makes sense when times to peak are considered. The developed drainage areas on the site, which are much smaller than the large offsite drainage areas OFF1 and OFF5, flush through the system faster when developed, making them less coincident with the runoff from the offsite drainage areas with the longer times of concentration and higher peak flow rates. Please see Table 5 the proposed conditions peak flow results.

In the southern portion of the site, the 5- and 100-year peak flow rates concentrating in the channel increase. In the 5-year event, the peak flow rate concentrating within the channel increases from 54 cfs in existing conditions to 73 cfs in proposed conditions. In the 100-year event the flow increases from 195 cfs in existing conditions to 248 cfs in proposed conditions. Please see Table 5 for all peak flow and times of peak results and Appendix D for the HEC-1 model output.

This increase in peak flow for the two design events will be mitigated in part by detention basins within the McCauley Ranch subdivision. Because this subdivision is still under design by TEC, the site and sizing of the detention basins are not included in this report. The channel bordering the Damonte Ranch High School and the downstream culverts

were designed to convey more than 250 cfs and according to normal depth and culvert rating curves can currently handle much higher flows (Wood Rodgers, Inc., 2005). However, the flow from the site is not the only runoff concentrating within the channel; there are small additional catchments that drain to it. The analysis for the final design of the McCauley Ranch subdivision and peak flow mitigation will insure that any increase in the 100-year peak flow to the channel will not overwhelm the conveyance capability of the channel or downstream culverts and will not increase the peak flow from the area for the two design storms.

Table 5: Proposed Conditions Runoff Results

Sub Drainage area	24-Hour		100-Year	
	Q _p (cfs)	T _p (hours)	Q _p (cfs)	T _p (hours)
OFF1	172	13.4	579	13.3
OFF2	30	12.6	108	12.6
OFF3	19	12.4	68	12.4
OFF4	38	12.5	139	12.5
OFF5	192	13.5	663	13.4
OFF6	35	12.5	129	12.5
OFF7	22	12.4	82	12.3
OFF8	7	12.2	26	12.2
DEV1	4	12.2	14	12.2
DEV2	22	12.3	86	12.3
DEV3	30	12.2	97	12.2
DEV4	8	12.2	31	12.2
DEV5	4	12.1	14	12.1
DEV6	1	12.2	5	12.1
DEV7	3	12.2	18	12.2
DEV8	6	12.1	18	12.1
DEV9	20	12.1	80	12.1
DEV10	54	12.1	176	12.1
DEV11	21	12.1	67	12.1
DEV12	21	12.1	71	12.1
DEV13	34	12.2	112	12.2

3.0 PROPOSED DRAINAGE FACILITIES

3.1 STORM DRAINS

The design of the storm drain system will be included in the phased drainage report submittals with the development plans. They will be designed according to City of Reno standards. All storm drains will discharge into proposed or existing channel. Storm drains will convey runoff from almost the entire on-site area. Half-lots that border a channel or detention basin will discharge directly into that channel or detention basin.

3.2 CHANNELS

The channel locations are shown in Figure 4 with the peak 100-year flow rates as described in the figure and Table 6. All side slopes and lining will be designed according to City of Reno standards in the final design of the subdivisions.

Table 6: Preliminary Channel Parameters

Channel	Side Slope	100-year Peak Flow (cfs)	Channel Width (ft)	Channel Depth (ft)	Channel Length (ft)
OFF5 to OFF6	0.100	129	10	3	0.8
CP8 to OFF6	0.083	687	10	3	2.2
CP8 to CP7	0.065	692	6	3	3.6
CP7 to CP6	0.15	695	6	3	5.1
OFF4 to CP4	0.052	139 to 205	5	3	1.7
CP4 to CP3	0.083	205 to 342	10	3	1.5
CP3 to CP1	0.027	342 to 584	10	3	2.7

3.3 CULVERTS

The culvert locations are shown in Figure 4. The culverts have been preliminarily designed for the northern portion of the site. Because the roadways and layout of the southern portion is very much in process, the locations and peak flows have been indicated on Figure 4 but no preliminary size has been assigned. The calculations for the culvert designs are located in appendix B.

Because of the steep slopes of the channels through much of the site, the inlets and outlets of the culverts will have to be armored.

3.4 MAINTENANCE ISSUES

The channels will need to be regularly maintained to prevent sediment accumulation that would jeopardize the function of the flood control facilities. Because there is such a relatively large off-site undeveloped area contributing to the portion of the site with the detention basin, significant sediment accumulation may compromise the basin capacity if not maintained.

4.0 CONCLUSION

The proposed Damonte Foothills development will not have negative drainage impacts on the areas surrounding it. It will decrease the amount of runoff discharging from the site in the design events in the northern portion of the site. From the southern portion, the final design of McCauley Ranch subdivision will ensure that any increase in peak flows to the channel will either be mitigated by on-site detention or will not overwhelm the capacity of the Damonte Ranch High School channel or any downstream facilities. In addition, any increase in peak flow from the southern portion of Damonte Foothills will not contribute to an overall increase in peak design flows from Damonte Ranch. Please see Table 7 for a summary of the computed runoff from the site in both existing and proposed conditions.

Table 7: Peak Flow Results

Location	Event			
	5-Year Ex	5-Year Prop	100-Year Ex	100-Year Prop
CP1	419	385	1354	1274
High School Channel	54	73	195	248

As the individual subdivision progress, the hydrology reports will be submitted to Wood Rodgers, Inc. to insure that the design conforms to the master drainage design.

References

- City of Reno, 2000. City of Reno Design Manual, Chapter II Storm Drainage. November 1st, 2000.
- Natural Resource Conservation District (Formerly Soil Conservation District), 1980. Soil Survey of Washoe County, Nevada, South Part.
- Nimbus Engineers, 1995. Southeast Truckee Meadows Flood Control Master Plan. May 1995.
- Nimbus Engineers, 2001. Application for Conditional Letter of Map Revision (CLOMR): Damonte Ranch/Double Diamond Ranch Regional Flood Control Improvements. March 2001 and Addendum September 2001.
- USACE, Hydrologic Engineering Center, HEC-1 v. 4.1, 1998.
- Washoe County, 1996. Washoe County Hydrologic Criteria and Drainage Design Manual. Prepared by WRC Nevada, December 1996.
- Wood Rodgers, Inc., 2005. Damonte Hills Boulevard Drainage Study. March 8, 2005.

Figure 1: Damonte Foothills Vicinity Map



Figure 2: Existing Conditions Subdrainage Area Delineation

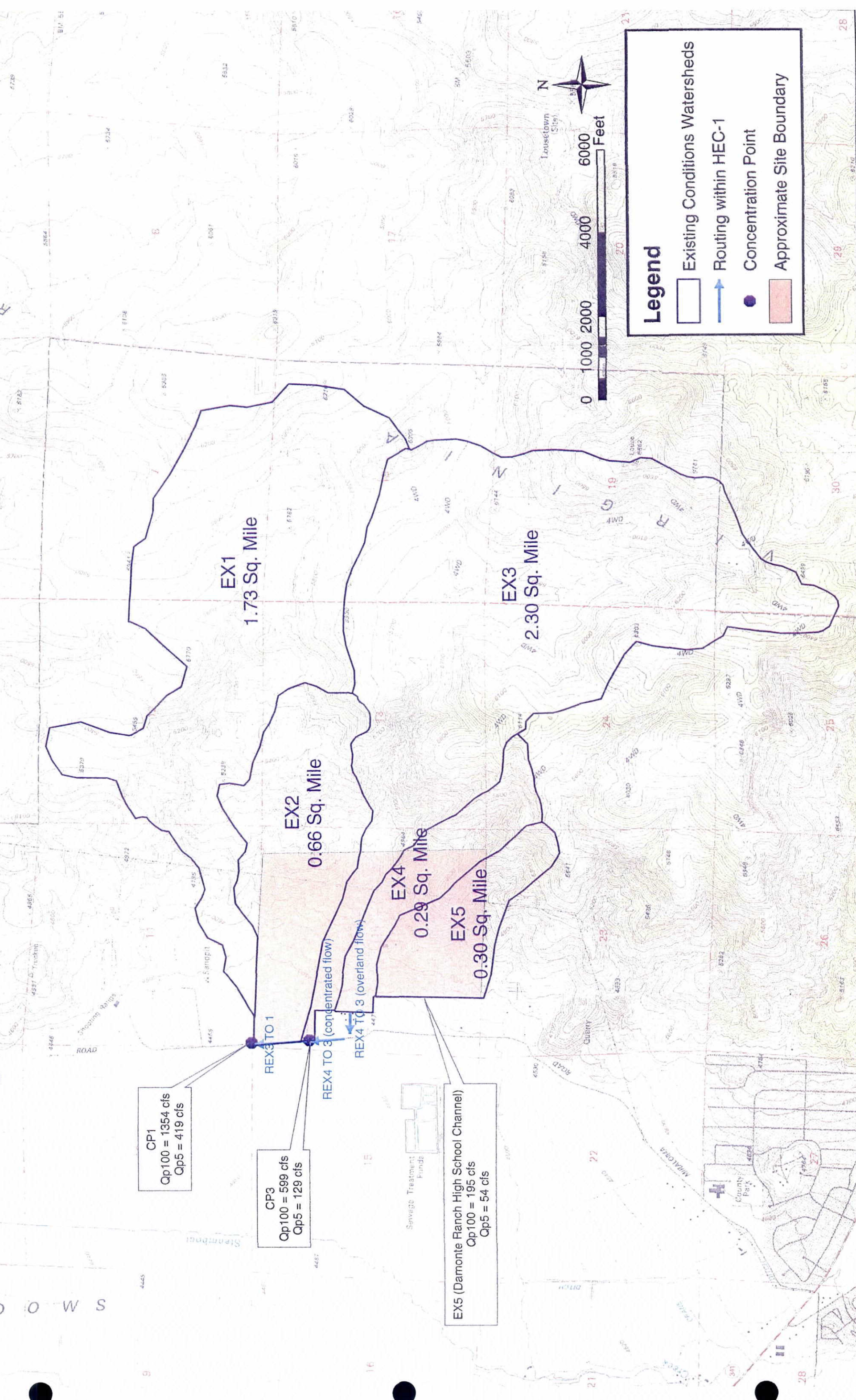


Figure 3: Proposed Conditions Subdrainage Area Delineation

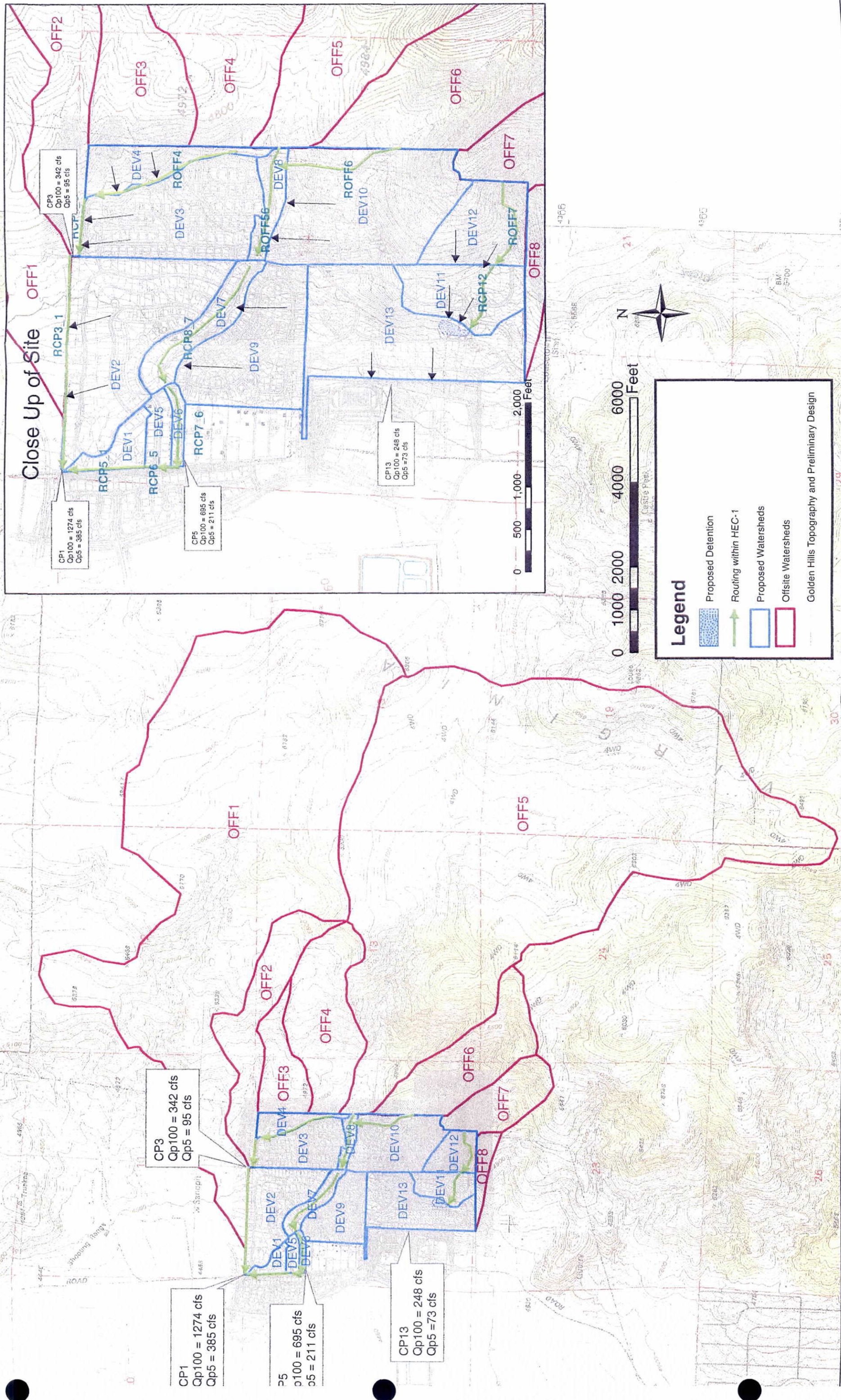
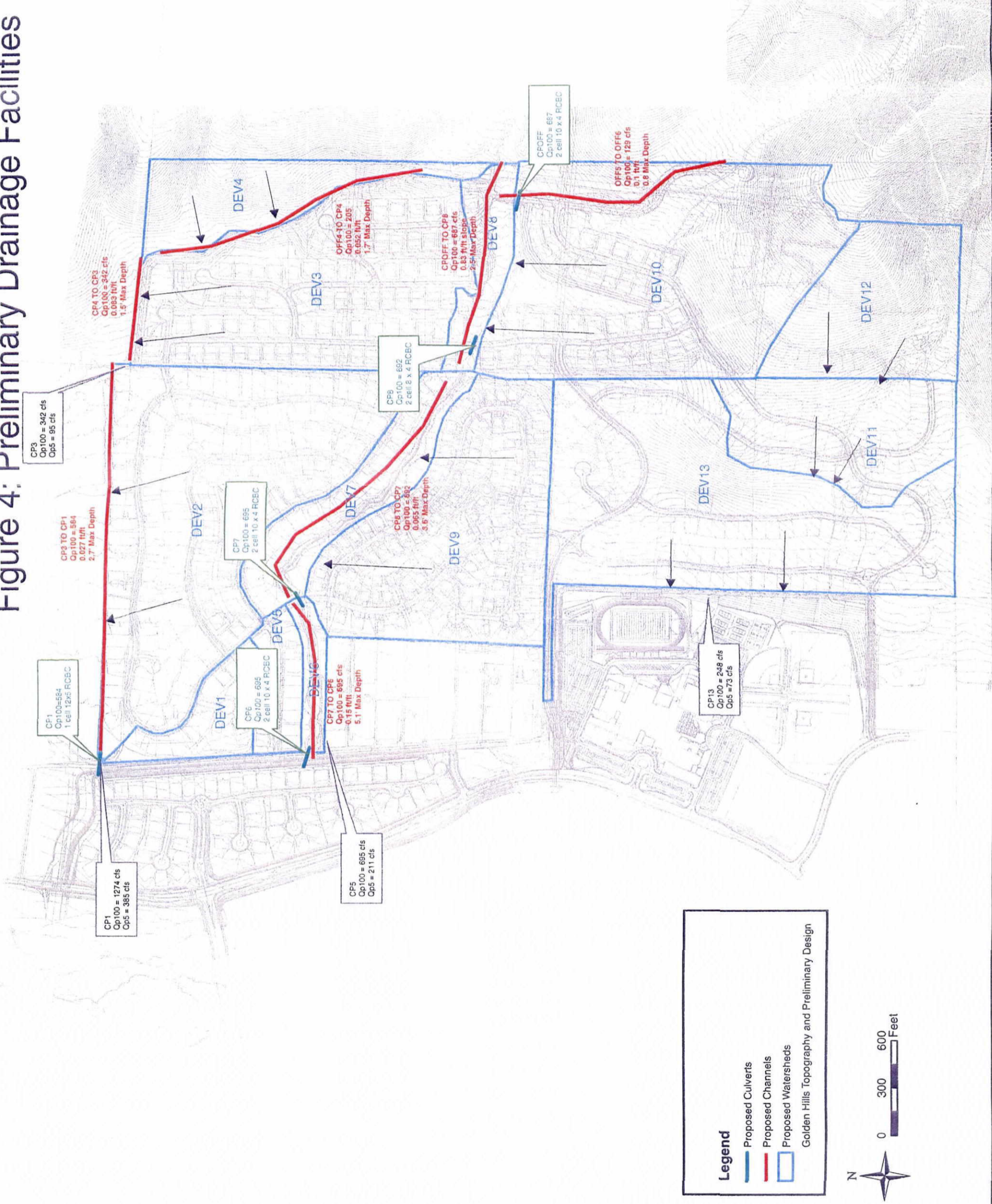


Figure 4: Preliminary Drainage Facilities





POINT PRECIPITATION FREQUENCY ESTIMATES FROM NOAA ATLAS 14



Nevada 39.433 N 119.67 W 5770 feet

from "Precipitation-Frequency Atlas of the United States" NOAA Atlas 14, Volume 1, Version 3

G.M. Bonnin, D. Todd, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland, 2003

Extracted: Fri Feb 4 2005

Precipitation Frequency Estimates (inches)																		
ARI* (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
2	0.13	0.20	0.25	0.34	0.41	0.55	0.67	0.97	1.32	1.75	2.20	2.71	3.21	3.64	4.71	5.62	6.81	7.99
5	0.18	0.27	0.34	0.45	0.56	0.72	0.84	1.20	1.68	2.25	2.86	3.56	4.25	4.81	6.18	7.37	8.92	10.45
10	0.22	0.33	0.41	0.56	0.69	0.84	0.98	1.38	1.96	2.65	3.40	4.27	5.11	5.75	7.32	8.73	10.54	12.24
25	0.28	0.43	0.54	0.72	0.89	1.04	1.16	1.60	2.31	3.21	4.17	5.28	6.33	7.07	8.88	10.60	12.73	14.55
50	0.34	0.52	0.65	0.87	1.08	1.21	1.30	1.77	2.59	3.67	4.80	6.10	7.32	8.13	10.10	12.05	14.42	16.28
100	0.41	0.62	0.78	1.04	1.29	1.39	1.48	1.93	2.87	4.14	5.47	6.99	8.39	9.26	11.38	13.55	16.17	18.00
200	0.49	0.75	0.93	1.25	1.55	1.61	1.70	2.11	3.14	4.65	6.18	7.94	9.54	10.43	12.69	15.11	17.96	19.72
500	0.62	0.95	1.18	1.59	1.97	2.04	2.12	2.33	3.50	5.35	7.19	9.31	11.17	12.09	14.50	17.24	20.42	21.98
1000	0.75	1.14	1.42	1.91	2.36	2.43	2.51	2.64	3.78	5.91	8.01	10.43	12.52	13.42	15.93	18.91	22.35	23.71

* These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval. Please refer to the documentation for more information. NOTE: Formatting forces estimates near zero to appear as zero.

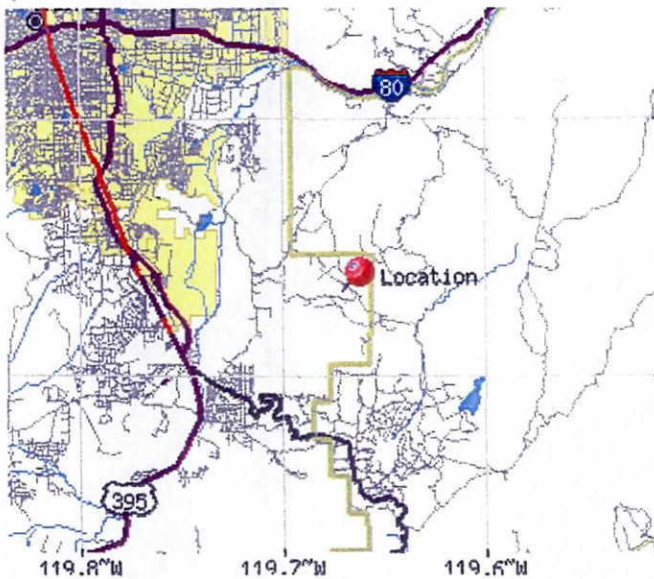
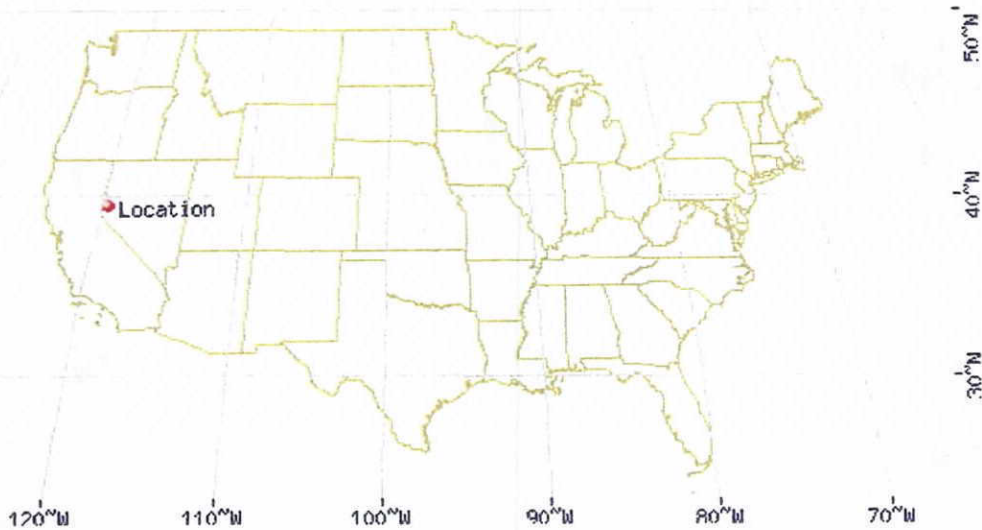
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
2	0.11	0.17	0.21	0.29	0.36	0.49	0.61	0.87	1.19	1.58	1.97	2.42	2.84	3.22	4.19	4.98	6.03	7.05
5	0.15	0.23	0.29	0.39	0.48	0.62	0.76	1.07	1.50	2.02	2.55	3.17	3.74	4.24	5.48	6.50	7.88	9.20
10	0.19	0.28	0.35	0.47	0.58	0.73	0.86	1.22	1.73	2.36	3.01	3.79	4.48	5.04	6.46	7.66	9.25	10.74
25	0.23	0.36	0.44	0.59	0.74	0.87	1.00	1.39	2.00	2.83	3.65	4.63	5.49	6.13	7.76	9.21	11.11	12.71
50	0.27	0.41	0.51	0.69	0.85	0.98	1.11	1.51	2.21	3.18	4.17	5.31	6.29	7.00	8.76	10.40	12.50	14.15
100	0.31	0.48	0.59	0.80	0.99	1.10	1.24	1.63	2.41	3.54	4.69	6.01	7.13	7.88	9.79	11.61	13.92	15.55
200	0.36	0.55	0.68	0.91	1.13	1.23	1.39	1.74	2.58	3.89	5.23	6.73	8.00	8.78	10.79	12.81	15.33	16.91
500	0.42	0.65	0.80	1.08	1.34	1.48	1.68	1.87	2.77	4.35	5.96	7.72	9.18	9.98	12.13	14.39	17.19	18.68
1000	0.48	0.73	0.91	1.23	1.52	1.70	1.93	2.10	2.92	4.70	6.52	8.50	10.13	10.90	13.14	15.59	18.59	19.96

* The lower bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are less than.

** These precipitation frequency estimates are based on a partial duration maxima series. ARI is the Average Recurrence Interval.

Please refer to the [documentation](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

Maps -



These maps were produced using a direct map request from the U.S. Census Bureau Mapping and Cartographic Resources [Tiger Map Server](#).

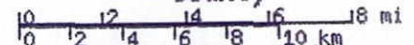
Please read [disclaimer](#) for more information.

LEGEND

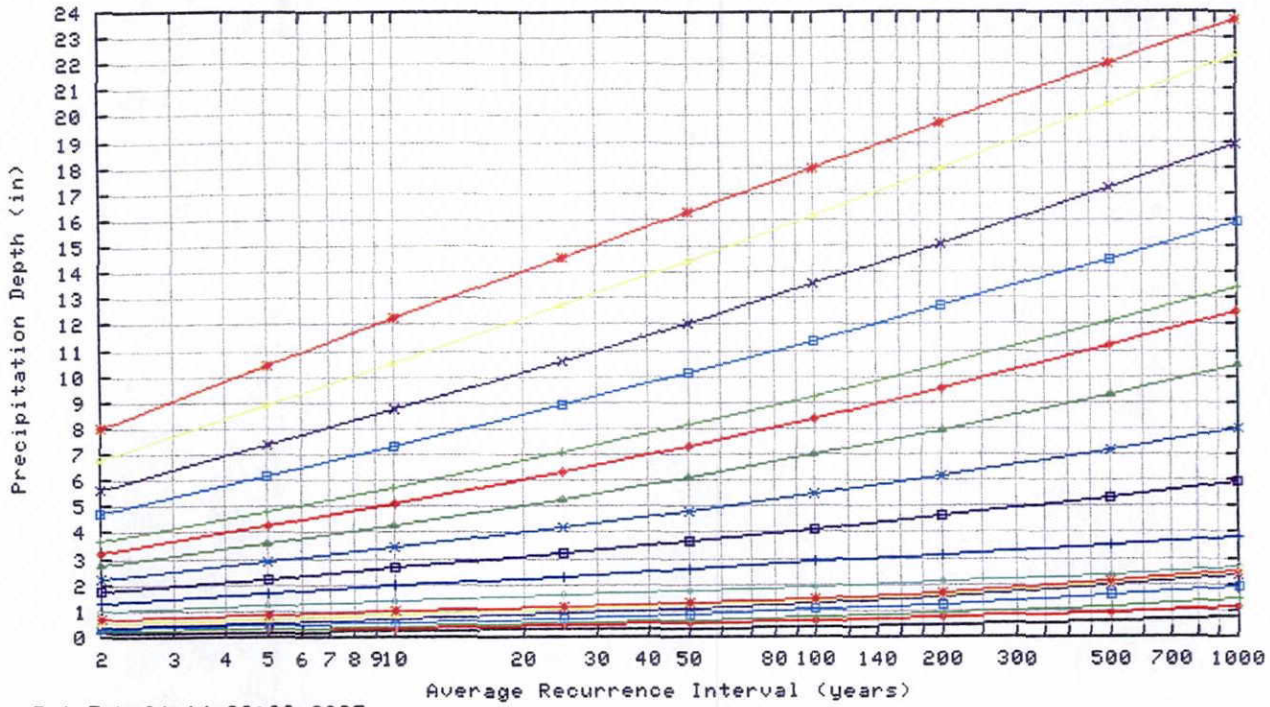
- State
- County
- Indian Resv
- Lake/Pond/Ocean
- Street
- Expressway
- Highway
- Connector
- Stream
- Military Area
- National Park
- Other Park
- City
- County

Scale 1:228583

*average--true scale depends on monitor resolution



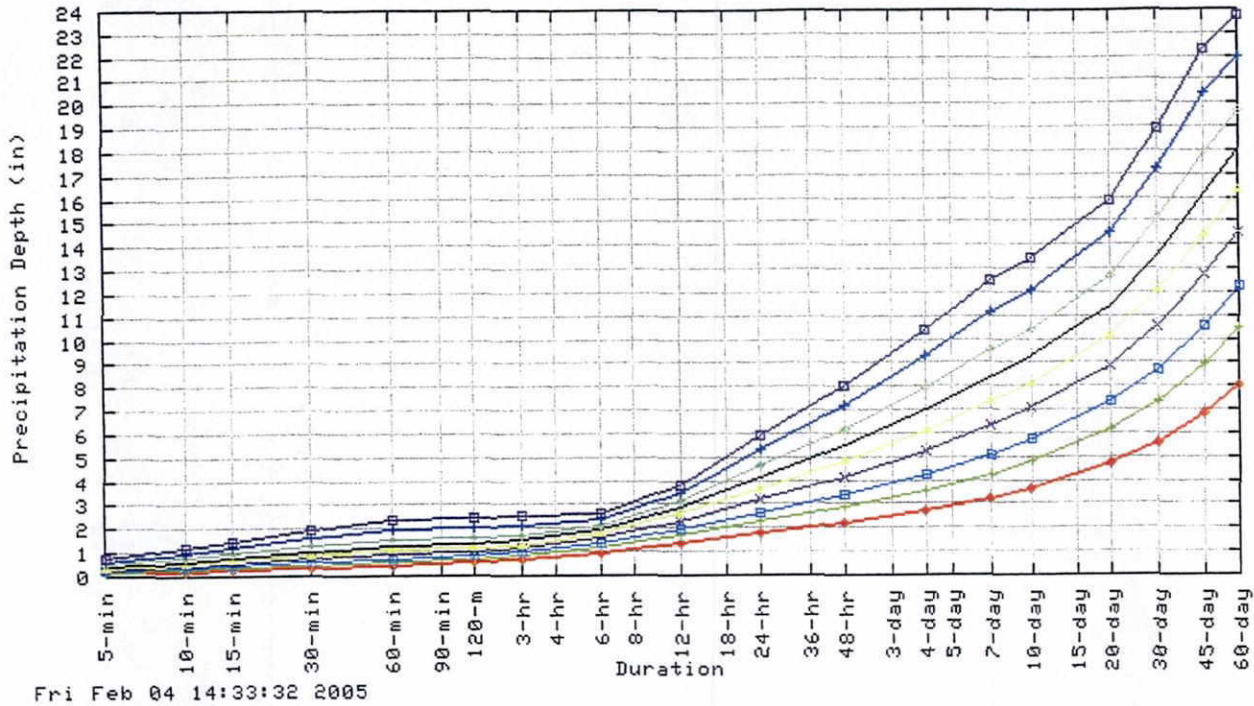
Partial duration based Point Precipitation Frequency Estimates Version: 3
 39.433 N 119.67 W 5770 ft



Fri Feb 04 14:33:32 2005

Duration			
5-min	5-min	48-hr	30-day
10-min	3-hr	4-day	45-day
15-min	6-hr	7-day	60-day
30-min	12-hr	10-day	
60-min	24-hr	20-day	

Partial duration based Point Precipitation Frequency Estimates Version: 3
39.433 N 119.67 W 5770 ft



Average Recurrence Interval (years)	
1 in 2	+
1 in 5	o
1 in 10	x
1 to 25	*
1 in 100	—
1 in 200	+
1 in 500	x
1 in 1000	o

Confidence Limits -

* Upper bound of the 90% confidence interval Precipitation Frequency Estimates (inches)																		
ARI** (years)	5 min	10 min	15 min	30 min	60 min	120 min	3 hr	6 hr	12 hr	24 hr	48 hr	4 day	7 day	10 day	20 day	30 day	45 day	60 day
2	0.15	0.24	0.29	0.39	0.49	0.64	0.76	1.09	1.48	1.95	2.48	3.05	3.66	4.16	5.34	6.39	7.69	9.04
5	0.21	0.32	0.40	0.54	0.66	0.82	0.95	1.35	1.89	2.50	3.22	4.03	4.87	5.50	7.01	8.39	10.10	11.81
10	0.26	0.39	0.49	0.66	0.81	0.98	1.11	1.55	2.20	2.95	3.83	4.83	5.85	6.58	8.33	9.96	11.94	13.83
25	0.34	0.52	0.64	0.86	1.06	1.22	1.33	1.82	2.64	3.60	4.72	5.98	7.26	8.11	10.13	12.10	14.44	16.48
50	0.41	0.63	0.78	1.05	1.30	1.44	1.52	2.02	2.98	4.13	5.45	6.92	8.42	9.35	11.55	13.82	16.41	18.50
100	0.50	0.77	0.95	1.28	1.58	1.71	1.79	2.24	3.35	4.72	6.25	7.96	9.67	10.66	13.04	15.58	18.45	20.54
200	0.62	0.94	1.17	1.57	1.95	2.02	2.10	2.47	3.72	5.34	7.12	9.09	11.04	12.08	14.61	17.45	20.60	22.58
500	0.82	1.25	1.55	2.08	2.58	2.66	2.74	3.03	4.27	6.25	8.39	10.76	13.06	14.12	16.86	20.06	23.58	25.36
1000	1.01	1.54	1.91	2.58	3.19	3.27	3.35	3.61	4.68	7.01	9.47	12.17	14.76	15.80	18.65	22.18	26.03	27.48

* The upper bound of the confidence interval at 90% confidence level is the value which 5% of the simulated quantile values for a given frequency are greater than.
 ** These precipitation frequency estimates are based on a partial duration series. ARI is the Average Recurrence Interval.
 Please refer to the [documentation](#) for more information. NOTE: Formatting prevents estimates near zero to appear as zero.

* Lower bound of the 90% confidence interval Precipitation Frequency Estimates (inches)																			

Other Maps/Photographs -

View USGS digital orthophoto quadrangle (DOQ) covering this location from TerraServer; **USGS Aerial Photograph** may also be available from this site. A DOQ is a computer-generated image of an aerial photograph in which image displacement caused by terrain relief and camera tilts has been removed. It combines the image characteristics of a photograph with the geometric qualities of a map. Visit the [USGS](#) for more information.

Watershed/Stream Flow Information -

Find the **Watershed** for this location using the U.S. Environmental Protection Agency's site.

Climate Data Sources -

Precipitation frequency results are based on data from a variety of sources, but largely NCDC. The following links provide general information about observing sites in the area, regardless of if their data was used in this study. For detailed information about the stations used in this study, please refer to our documentation.

Using the **National Climatic Data Center's (NCDC)** station search engine, locate other climate stations within:

7287711ES ...OR... **0601E** of this location (39.433/-119.67). Digital ASCII data can be obtained directly from [NCDC](#).

Find **Natural Resources Conservation Service (NRCS) SNOTEL (SNOWpack TELEmetry)** stations by visiting the **Western Regional Climate Center's state-specific SNOTEL station maps**.

Hydrometeorological Design Studies Center
DOC/NOAA/National Weather Service
1325 East-West Highway
Silver Spring, MD 20910
(301) 713-1669
Questions?: HDSC_Questions@noaa.gov

[Disclaimer](#)

Time of Concentration Worksheet
 Golden Hills Proposed Watersheds
 Calculated by: Wood Rodgers, Inc

Sub-basin Data		Initial/Overland Time		Travel Time			Tc		Tc Urbanized Basins Check		Final Tc		Lag Time
No.	Area	Length (ft)	Slope (%)	Ti (min) ¹	Length (ft)	Slope (%)	Vel. (fps) ²	Tl (min)	(Ti+Tl)	Total Length (ft)	Tc ³	(min)	(hrs) (0.6*Tc)
1	0.0115	100	1	5.8	1060	0.086	0.6	30.1	35.9	1160	16.4	16.4	0.16
2	0.0957	100	2.63	4.2	4044	2.63	3.2	20.8	25.0	4144	33.0	25.0	0.25
3	0.0724	100	4.69	3.5	3416	4.69	4.3	13.1	16.6	3516	29.5	16.6	0.17
4	0.0233	100	6.2	3.2	1594	6.2	2.5	10.7	13.8	1694	19.4	13.8	0.14
5	0.0091	100	1.26	5.3	770	1.26	2.2	5.7	11.1	870	14.8	11.1	0.11
6	0.0053	100	1.45	5.1	865	1.45	2.4	6.0	11.1	965	15.4	11.1	0.11
7	0.0227	100	5.4	3.3	1845	5.4	2.3	13.2	16.5	1945	20.8	16.5	0.17
8	0.0118	100	7.66	2.9	1271	7.66	5.5	3.8	6.8	1371	17.6	6.8	0.07
9	0.0638	100	5.55	3.3	2240	5.55	4.7	7.9	11.2	2340	23.0	11.2	0.11
10	0.0949	100	16.2	2.3	2485	16.2	8.0	5.1	7.4	2585	24.4	7.4	0.07
11	0.0034	100	12.4	2.5	867	12.4	7.0	2.1	4.6	967	15.4	4.6	0.05
12	0.0346	100	16.4	2.3	998	16.4	8.1	2.1	4.3	1098	16.1	4.3	0.04
13	0.0911	100	3.65	3.8	3734	3.65	8.1	7.7	11.4	3834	31.3	11.4	0.11

¹ Ti=1.8 (1.1-R)^{1/2} L^{1/2}/S^{1/3} Assume R=.78 for all urban areas

² velocity on paved surfaces = 2*slope^{.42}; velocity on open space= slope^{.1/2}

³ Tc=(L/180)+10

Existing Conditions Soil and CN Determination
Vegetation Cover Assumed Shrub/Brush (except for burned area in EX5)

Watershed				Soil Polygon				Composite	
ID	Area (sq feet)	area_sqmil	MUSYM	mname	Area (sq feet)	Hydro	CN	Soil %	CN
1	4479625.06	1.72959	482	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES	53716.61	B	61	1.2%	81.75
1	4479625.06	1.72959	531	SAGOUSPE FINE SANDY LOAM	153.10	C	73	0.0%	
1	4479625.06	1.72959	585	BARNARD-TROSI ASSOCIATION	4132683.35	D	82	92.3%	
1	4479625.06	1.72959	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	293071.99	D		6.5%	
2	1715318.06	0.66229	482	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES	26148.01	B	61	1.5%	74.64
2	1715318.06	0.66229	971	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES	64585.59	B	61	3.8%	
2	1715318.06	0.66229	482	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES	55342.74	B	61	3.2%	
2	1715318.06	0.66229	531	SAGOUSPE FINE SANDY LOAM	31428.86	C	73	1.8%	
2	1715318.06	0.66229	911	VAMP SILT LOAM, STRONGLY SALINE-ALKALI	7202.17	C	73	0.4%	
2	1715318.06	0.66229	420	GODECKE LOAMY SAND	49773.04	C	73	2.9%	
2	1715318.06	0.66229	585	BARNARD-TROSI ASSOCIATION	1136934.09	D	82	66.3%	
2	1715318.06	0.66229	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	343903.56	D	82	20.0%	
3	5951392.32	2.29785	960	KAYO STONY SANDY LOAM, 2 TO 4 PERCENT SLOPES	367666.34	B	61	6.2%	80.27
3	5951392.32	2.29785	971	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES	25706.90	B	61	0.4%	
3	5951392.32	2.29785	482	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES	89113.81	B	61	1.5%	
3	5951392.32	2.29785	911	VAMP SILT LOAM, STRONGLY SALINE-ALKALI	6330.99	C	73	0.1%	
3	5951392.32	2.29785	420	GODECKE LOAMY SAND	9777.01	C	73	0.2%	
3	5951392.32	2.29785	585	BARNARD-TROSI ASSOCIATION	1604949.08	D	82	27.0%	
3	5951392.32	2.29785	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	3822387.92	D	82	64.2%	
3	5951392.32	2.29785	1520	DUCCO-SMALLCONE-CAGLE ASSOCIATION	25460.28	D	82	0.4%	
4	755071.91	0.29153	971	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES	16413.61	B	61	2.2%	80.54
4	755071.91	0.29153	482	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES	36250.09	B	61	4.8%	
4	755071.91	0.29153	585	BARNARD-TROSI ASSOCIATION	203694.86	D	82	27.0%	
4	755071.91	0.29153	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	498713.94	D	82	66.0%	
5	782130.19	0.30198	971	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES	393.11	B	62*	0.1%	82.06
5	782130.19	0.30198	252	CASSIRO GRAVELLY SANDY LOAM, 8 TO 15 PERCENT SLOPES	128194.97	C	75*	16.4%	
5	782130.19	0.30198	585	BARNARD-TROSI ASSOCIATION	317032.17	D	85*	40.5%	
5	782130.19	0.30198	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	336509.93	D	82	43.0%	

* Burned area - assumed mixed grass shrub

Offsite Watershed Soil and CN Calculations
 Assuming vegetation cover is shrub/brush

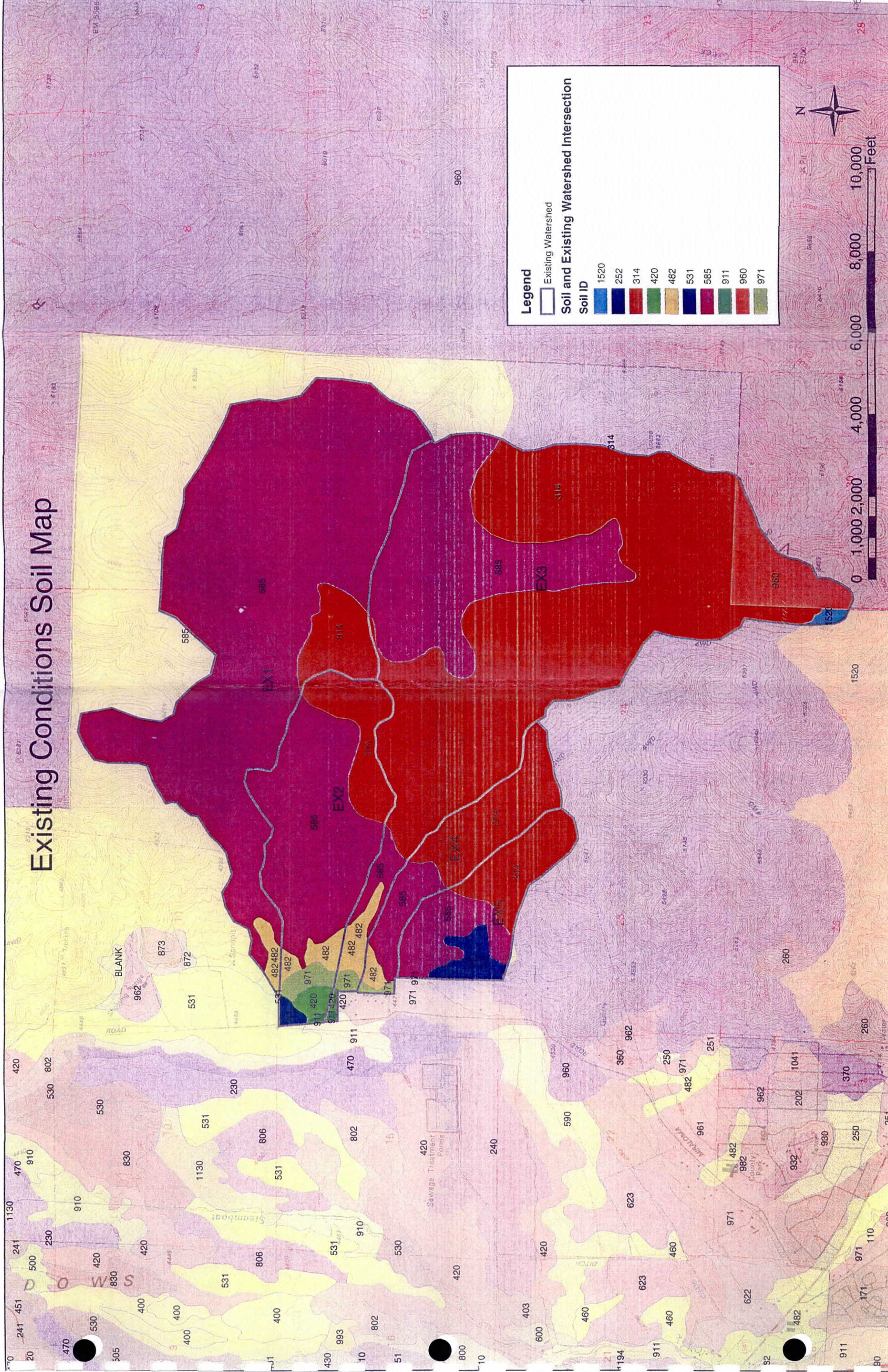
ID	Watershed				Soil Polygon										Composite CN
	Area (sq feet)	area_mile	Length	Lc	Fall	Slope	AREA_AC	Area (sq mile)	MUSYM	inunama	Hydro	CN	Soil %		
1	4479625.06	1.72959	17152.00	12490.00	3825	1177.47	1106.93	53716.61	482	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES	B	61	1.20%	81.75	
1	4479625.06	1.72959	17152.00	12490.00	3825	1177.47	1106.93	153.10	531	SAGOUSPE FINE SANDY LOAM	C	73	0.00%		
1	4479625.06	1.72959	17152.00	12490.00	3825	1177.47	1106.93	4132683.36	585	BARNARD-TROSI ASSOCIATION	D	82	92.26%	82.00	
1	4479625.06	1.72959	17152.00	12490.00	3825	1177.47	1106.93	293071.99	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	6.54%		
2	448661.98	0.17323	0.00	0.00	0	0.00	110.87	360529.36	585	BARNARD-TROSI ASSOCIATION	D	82	80.36%	82.00	
2	448661.98	0.17323	0.00	0.00	0	0.00	110.87	88132.62	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	19.64%		
3	207170.48	0.07999	3245.00	1355.00	800	1301.00	51.19	207170.48	585	BARNARD-TROSI ASSOCIATION	D	82	100.00%	82.00	
4	536054.38	0.20697	5292.00	3288.00	2200	2195.00	132.46	281475.95	585	BARNARD-TROSI ASSOCIATION	D	82	52.51%		
4	536054.38	0.20697	5292.00	3288.00	2200	2195.00	132.46	254578.43	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	47.49%		
5	5752978.79	2.22124	18155.00	10100.00	189	529.00	1421.58	368071.88	960	KAYO STONY SANDY LOAM, 2 TO 4 PERCENT SLOPES	B	61	6.36%	80.66	
5	5752978.79	2.22124	18155.00	10100.00	189	529.00	1421.58	1536451.92	585	BARNARD-TROSI ASSOCIATION	D	82	26.74%		
5	5752978.79	2.22124	18155.00	10100.00	189	529.00	1421.58	3823013.29	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	66.45%		
5	5752978.79	2.22124	18155.00	10100.00	189	529.00	1421.58	25441.71	1520	DUCO-SMALL CONE-CAGLE ASSOCIATION	D	82	0.44%		
6	481616.87	0.18595	5120.00	2392.00	1354	1396.31	119.01	9350.91	585	BARNARD-TROSI ASSOCIATION	D	82	1.94%	82.00	
6	481616.87	0.18595	5120.00	2392.00	1354	1396.31	119.01	472159.50	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	98.04%		
6	481616.87	0.18595	5120.00	2392.00	1354	1396.31	119.01	106.46	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	0.02%		
7	241217.79	0.09313	2704.00	1510.00	920	1796.45	59.61	24111.33	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	99.96%	82.00	
7	241217.79	0.09313	2704.00	1510.00	920	1796.45	59.61	106.46	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	0.04%		
8	59107.54	0.02282	1528.00	751.00	640	2211.52	14.61	1885.33	252	CASSIRO GRAVELLY SANDY LOAM, 8 TO 15 PERCENT SLOPES	C	73	3.19%	81.71	
8	59107.54	0.02282	1528.00	751.00	640	2211.52	14.61	15194.95	585	BARNARD-TROSI ASSOCIATION	D	82	25.71%		
8	59107.54	0.02282	1528.00	751.00	640	2211.52	14.61	42027.26	314	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION	D	82	71.10%		

Proposed Conditions Soil Hydro Group and CN Calculation
 Taken from GIS database analysis

id	Area (sq feet)		Area (ACRE)		Watershed		Slope		Houses		acre/house		MUSTM		Hydro Grp		Name		Soil Polygon		Soil area		Soil %		Composite		Impervious area			
	Area	Ln	Area	Ln	area	Ln	Slope	Houses	acre/house	MUSTM	Hydro Grp	name	Soil Polygon	Soil area	Soil %	CN	CN	Soil %	CN	Soil %	CN	Soil %	CN	Soil %	CN	Soil %	CN	Soil %	CN	
1	320235.91	7.35	0.01149	1160	10	16	0.459	631	C	SAGOUSE FINE SANDY LOAM		109584.78	34.22%	80.20	80.20	28440	8.88%													
1	320235.91	7.35	0.01149	1160	10	16	0.459	631	C	VAMP SILT LOAM, STRONGLY SALINE-ALKALI		31976.32	9.93%	80.20	80.20															
1	320235.91	7.35	0.01149	1160	10	16	0.459	631	C	GODECKE LOAMY SAND		178674.82	65.79%	80.20	80.20															
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	B	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES		276840.65	10.45%	71.13	71.13	305940	11.47%													
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		490988.97	18.40%	71.13	71.13															
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	B	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES		640365.19	24.01%	71.13	71.13															
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	C	SAGOUSE FINE SANDY LOAM		201472.36	7.55%	80.56	80.56															
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	C	GODECKE LOAMY SAND		181752.79	6.81%	80.56	80.56															
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	D	BARNARD-TROSI ASSOCIATION		874160.04	32.77%	85.13	85.13															
2	2667530.00	61.24	0.09568	4144	109	161	0.406	482	D	BARNARD-TROSI ASSOCIATION		189545.28	93.64%	84.43	84.43	235400	11.17%													
3	2017845.54	46.32	0.07238	3516	165	79	0.586	585	D	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES		128400.25	6.36%	69.66	69.66															
3	2017845.54	46.32	0.07238	3516	165	79	0.586	585	B	BARNARD-TROSI ASSOCIATION		849339.00	100.00%	82.00	82.00	0	0.00%													
4	649338.99	14.91	0.02329	1894	105	0		585	D	BARNARD-TROSI ASSOCIATION																				
5	254007.99	5.83	0.00911	870	11	18	0.324	971	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		5685.63	2.24%	72.33	72.33	34400	13.54%													
5	254007.99	5.83	0.00911	870	11	18	0.324	971	C	VAMP SILT LOAM, STRONGLY SALINE-ALKALI		64127.67	25.25%	81.22	81.22															
5	254007.99	5.83	0.00911	870	11	18	0.324	971	C	GODECKE LOAMY SAND		184194.69	72.52%	81.22	81.22															
6	147250.43	3.38	0.00528	965	14	0		971	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		24331.43	16.52%	62.00	62.00	0	0.00%													
6	147250.43	3.38	0.00528	965	14	0		971	C	VAMP SILT LOAM, STRONGLY SALINE-ALKALI		35233.32	23.93%	74.00	74.00															
6	147250.43	3.38	0.00528	965	14	0		971	C	GODECKE LOAMY SAND		87685.68	59.55%	74.00	74.00															
7	633367.26	14.54	0.02272	1945	105	20	0.727	971	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		159412.72	25.17%	69.09	69.09	43200	6.82%													
7	633367.26	14.54	0.02272	1945	105	20	0.727	971	B	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES		439000.81	68.36%	69.09	69.09															
7	633367.26	14.54	0.02272	1945	105	20	0.727	971	C	GODECKE LOAMY SAND		581.96	0.09%	79.55	79.55															
7	633367.26	14.54	0.02272	1945	105	20	0.727	971	D	BARNARD-TROSI ASSOCIATION		40371.67	6.37%	84.55	84.55															
8	330184.94	7.59	0.01164	1371	105	5	1.516	585	D	BARNARD-TROSI ASSOCIATION		209137.71	63.34%	85.00	85.00	33940	10.25%													
8	330184.94	7.59	0.01164	1371	105	5	1.516	585	B	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES		121057.23	36.68%	62.00	62.00															
8	330184.94	7.59	0.01164	1371	105	5	1.516	585	D	BARNARD-TROSI ASSOCIATION																				
9	177777.53	40.81	0.06377	2340	130	111	0.368	971	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		466710.59	26.25%	69.58	69.58	213120	11.99%													
9	177777.53	40.81	0.06377	2340	130	111	0.368	971	B	HOLBROOK COBBLY LOAMY SAND, 2 TO 8 PERCENT SLOPES		621369.56	34.95%	69.58	69.58															
9	177777.53	40.81	0.06377	2340	130	111	0.368	971	C	GODECKE LOAMY SAND		5268.69	0.30%	80.79	80.79															
9	177777.53	40.81	0.06377	2340	130	111	0.368	971	D	BARNARD-TROSI ASSOCIATION		684428.74	38.50%	84.79	84.79															
10	2643288.01	60.73	0.09489	2585	420	40	1.518	585	D	BARNARD-TROSI ASSOCIATION		2218469.69	83.79%	84.00	84.00	193200	7.30%													
10	2643288.01	60.73	0.09489	2585	420	40	1.518	585	D	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION		428616.33	16.21%	84.00	84.00															
11	932651.16	21.47	0.00335	3834	140	52	0.412	585	C	CASSIRO GRAVELLY SANDY LOAM, 8 TO 15 PERCENT SLOPES		492386.54	52.79%	80.53	80.53	121520	13.03%													
11	932651.16	21.47	0.00335	3834	140	52	0.412	585	D	BARNARD-TROSI ASSOCIATION		438107.76	46.97%	85.52	85.52															
11	932651.16	21.47	0.00335	3834	140	52	0.412	585	D	BARNARD-TROSI ASSOCIATION		397.42	0.04%	85.52	85.52															
11	932651.16	21.47	0.00335	3834	140	52	0.412	585	D	BARNARD-TROSI ASSOCIATION		1759.43	0.19%	85.52	85.52															
12	963871.02	22.13	0.03457	1098	180	12	1.844	585	D	BARNARD-TROSI ASSOCIATION		541485.28	56.18%	84.00	84.00	24000	2.49%													
12	963871.02	22.13	0.03457	1098	180	12	1.844	585	D	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION		422375.74	43.82%	84.00	84.00															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		37055.20	1.46%	70.26	70.26	280560	11.05%													
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	B	ALADSHI SANDY LOAM, 2 TO 4 PERCENT SLOPES		479.10	0.02%	70.26	70.26															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	C	GODECKE LOAMY SAND		292.69	0.01%	80.13	80.13															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	C	CASSIRO GRAVELLY SANDY LOAM, 8 TO 15 PERCENT SLOPES		879892.44	34.64%	80.13	80.13															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	D	BARNARD-TROSI ASSOCIATION		1619355.80	63.72%	85.13	85.13															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	D	RISLEY-XMAN-ROCK OUTCROP ASSOCIATION		448.58	0.02%	85.13	85.13															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	D	BARNARD-TROSI ASSOCIATION		1410.00	0.06%	85.13	85.13															
13	2539977.02	58.31	0.00911	3834	140	122	0.478	971	D	BARNARD-TROSI ASSOCIATION		2040.22	0.08%	85.13	85.13															

CN is based on average lot size in subwatershed (# of houses/area) weighted with soil type

Existing Conditions Soil Map

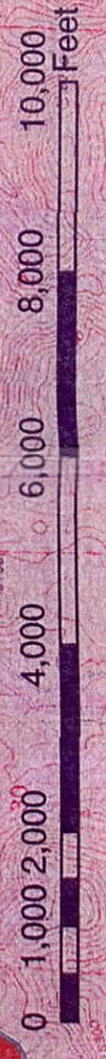


Legend

- Existing Watershed
- Soil and Existing Watershed Intersection

Soil ID

1520	252	314	420	482	531	585	911	960	971
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Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	OFF6 TO OFF5
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Channel Slope	100000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft
Discharge	129.00 cfs

Results

Depth	0.84 ft
Flow Area	10.6 ft ²
Wetted Perim	15.33 ft
Top Width	15.06 ft
Critical Depth	1.48 ft
Critical Slope	0.013012 ft/ft
Velocity	12.22 ft/s
Velocity Head	2.32 ft
Specific Energ	3.16 ft
Froude Numb	2.57
Flow Type	Supercritical

Worksheet

Worksheet for Trapezoidal Channel

Project Description

Worksheet	CPOFF to CP8
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Channel Slope	083000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft
Discharge	687.00 cfs

Results

Depth	2.19 ft
Flow Area	36.4 ft ²
Wetted Perim	23.87 ft
Top Width	23.16 ft
Critical Depth	3.69 ft
Critical Slope	0.010256 ft/ft
Velocity	18.89 ft/s
Velocity Head	5.55 ft
Specific Energ	7.74 ft
Froude Numb	2.66
Flow Type	Supercritical

Worksheet

Worksheet for Irregular Channel

Project Description

Worksheet	CP8 TO CP7
Flow Element	Irregular Chan
Method	Manning's For
Solve For	Channel Depth

Input Data

Channel Slope	0.065000 ft/ft
Discharge	692.00 cfs

Options

Current Roughness Method	used Lotter's Method
Open Channel Weighting	used Lotter's Method
Closed Channel Weighting	Horton's Method

Results

Mannings Coefficient	0.030
Water Surface Elev	3.60 ft
Elevation Range	3.00 to 7.00
Flow Area	35.3 ft ²
Wetted Perimeter	18.31 ft
Top Width	15.62 ft
Actual Depth	3.60 ft
Critical Elevation	5.41 ft
Critical Slope	0.010905 ft/ft
Velocity	19.58 ft/s
Velocity Head	5.96 ft
Specific Energy	9.56 ft
Froude Number	2.30
Flow Type	Supercritical

Roughness Segments

Start Station	End Station	Mannings Coefficient
0+00	0+36	0.030

Natural Channel Points

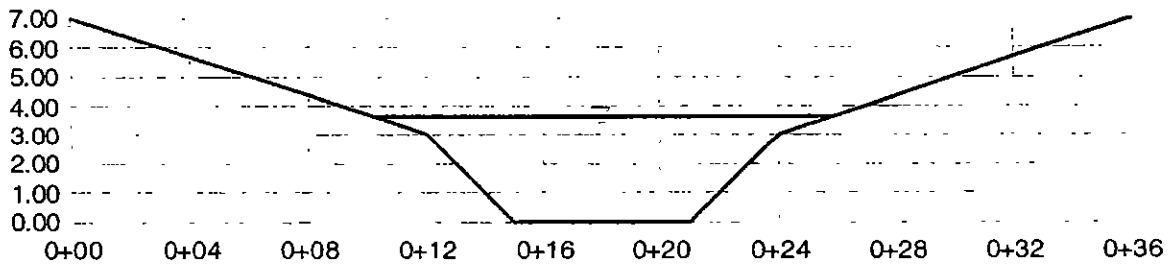
Station (ft)	Elevation (ft)
0+00	7.00
0+12	3.00
0+15	0.00
0+21	0.00
0+24	3.00
0+36	7.00

Cross Section

Cross Section for Irregular Channel

Project Description	
Worksheet	CP8 TO CP7
Flow Element	Irregular Chan
Method	Manning's Forr
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.030
Channel Slope	0.065000 ft/ft
Water Surface Elev	3.60 ft
Elevation Range	.00 to 7.00
Discharge	692.00 cfs



V:1
H:1
NTS

Worksheet

Worksheet for Irregular Channel

Project Description

Worksheet	CP7 TO CP6
Flow Element	Irregular Chan
Method	Manning's Forr
Solve For	Channel Depth

Input Data

Channel Sk	015000 ft/ft
Discharge	695.00 cfs

Options

Current Roughness Method	ved Lotter's Method
Open Channel Weighting	ved Lotter's Method
Closed Channel Weighting	Horton's Method

Results

Mannings Coefficient	0.030
Water Surface Elev	5.08 ft
Elevation Range	3.00 to 7.00
Flow Area	64.9 ft ²
Wetted Perimeter	27.62 ft
Top Width	24.46 ft
Actual Depth	5.08 ft
Critical Elevation	5.42 ft
Critical Slope	0.010899 ft/ft
Velocity	10.72 ft/s
Velocity Head	1.78 ft
Specific Energy	6.86 ft
Froude Number	1.16
Flow Type	Supercritical

Roughness Segments

Start Station	End Station	Mannings Coefficient
0+00	0+36	0.030

Natural Channel Points

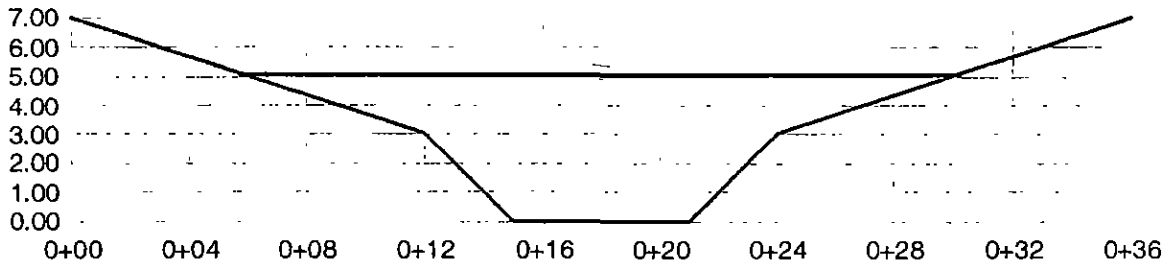
Station (ft)	Elevation (ft)
0+00	7.00
0+12	3.00
0+15	0.00
0+21	0.00
0+24	3.00
0+36	7.00

Cross Section

Cross Section for Irregular Channel

Project Description	
Worksheet	CP7 TO CP6
Flow Element	Irregular Chanl
Method	Manning's Forr
Solve For	Channel Depth

Section Data	
Mannings Coefficient	0.030
Channel Slope	0.015000 ft/ft
Water Surface Elev	5.08 ft
Elevation Range	.00 to 7.00
Discharge	695.00 cfs



V:1
H:1
NTS

Table Rating Table for Trapezoidal Channel

Project Description	
Worksheet	CP3 TO CP1
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Input Data	
Mannings Coeffic	0.030
Channel Slope	027000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft

Attribute	Minimum	Maximum	Increment
Discharge (cfs)	342.00	584.00	10.00

Discharge (cfs)	Depth (ft)	Velocity (ft/s)	Flow Area (ft ²)	Wetted Perimeter (ft)	Top Width (ft)
342.00	2.04	10.37	33.0	22.93	22.27
352.00	2.08	10.45	33.7	23.12	22.45
362.00	2.11	10.54	34.4	23.32	22.63
372.00	2.14	10.62	35.0	23.50	22.81
382.00	2.16	10.70	35.7	23.69	22.99
392.00	2.19	10.78	36.4	23.87	23.16
402.00	2.22	10.85	37.0	24.06	23.33
412.00	2.25	10.93	37.7	24.23	23.50
422.00	2.28	11.00	38.4	24.41	23.67
432.00	2.31	11.07	39.0	24.58	23.84
442.00	2.33	11.14	39.7	24.76	24.00
452.00	2.36	11.21	40.3	24.93	24.16
462.00	2.39	11.28	41.0	25.09	24.32
472.00	2.41	11.35	41.6	25.26	24.48
482.00	2.44	11.41	42.2	25.42	24.63
492.00	2.46	11.48	42.9	25.58	24.79
502.00	2.49	11.54	43.5	25.75	24.94
512.00	2.51	11.61	44.1	25.90	25.09
522.00	2.54	11.67	44.7	26.06	25.23
532.00	2.56	11.73	45.4	26.21	25.38
542.00	2.59	11.79	46.0	26.37	25.53
552.00	2.61	11.85	46.6	26.52	25.67
562.00	2.64	11.91	47.2	26.67	25.81
572.00	2.66	11.97	47.8	26.82	25.95
582.00	2.68	12.02	48.4	26.97	26.09

Table Rating Table for Trapezoidal Channel

Project Description

Worksheet	OFF4 TO CP4
Flow Element	Trapezoidal Cha
Method	Manning's Formu
Solve For	Channel Depth

Input Data

Mannings Coeffic	0.030
Channel Slope	052000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	5.00 ft

Attribute	Minimum	Maximum	Increment
Discharge (cfs)	139.00	205.00	10.00

Discharge (cfs)	Depth (ft)	Velocity (ft/s)	Flow Area (ft ²)	Wetted Perimeter (ft)	Top Width (ft)
139.00	1.40	10.77	12.9	13.87	13.41
149.00	1.45	10.97	13.6	14.18	13.71
159.00	1.50	11.17	14.2	14.48	13.99
169.00	1.54	11.35	14.9	14.77	14.27
179.00	1.59	11.53	15.5	15.05	14.54
189.00	1.63	11.70	16.2	15.32	14.79
199.00	1.67	11.86	16.8	15.59	15.04

Table Rating Table for Trapezoidal Channel

Project Description	
Worksheet	CP4 TO CP3
Flow Element	Trapezoidal Cha
Method	Manning's Form
Solve For	Channel Depth

Input Data	
Mannings Coeffic	0.030
Channel Slope	083000 ft/ft
Left Side Slope	3.00 H : V
Right Side Slope	3.00 H : V
Bottom Width	10.00 ft

Attribute	Minimum	Maximum	Increment
Discharge (cfs)	205.00	342.00	10.00

Discharge (cfs)	Depth (ft)	Velocity (ft/s)	Flow Area (ft ²)	Wetted Perimeter (ft)	Top Width (ft)
205.00	1.15	13.26	15.5	17.27	16.90
215.00	1.18	13.45	16.0	17.47	17.08
225.00	1.21	13.64	16.5	17.65	17.26
235.00	1.24	13.82	17.0	17.84	17.44
245.00	1.27	14.00	17.5	18.02	17.61
255.00	1.30	14.16	18.0	18.20	17.78
265.00	1.32	14.33	18.5	18.37	17.94
275.00	1.35	14.49	19.0	18.54	18.10
285.00	1.38	14.65	19.5	18.71	18.26
295.00	1.40	14.80	19.9	18.87	18.42
305.00	1.43	14.95	20.4	19.03	18.57
315.00	1.45	15.09	20.9	19.19	18.72
325.00	1.48	15.23	21.3	19.35	18.87
335.00	1.50	15.37	21.8	19.50	19.02

Culvert Calculator Report

CP7

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	4,474.00 ft	Headwater Depth/Height	1.46
Computed Headwater Elev.	4,473.36 ft	Discharge	695.00 cfs
Inlet Control HW Elev.	4,472.93 ft	Tailwater Elevation	4,467.00 ft
Outlet Control HW Elev.	4,473.36 ft	Control Type	Entrance Control
Grades			
Upstream Invert	4,467.50 ft	Downstream Invert	4,465.30 ft
Length	110.00 ft	Constructed Slope	0.020000 ft/ft
Hydraulic Profile			
Profile	S2	Depth, Downstream	2.13 ft
Slope Type	Steep	Normal Depth	1.79 ft
Flow Regime	Supercritical	Critical Depth	3.35 ft
Velocity Downstream	16.35 ft/s	Critical Slope	0.003261 ft/ft
Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		
Outlet Control Properties			
Outlet Control HW Elev.	4,473.36 ft	Upstream Velocity Head	1.67 ft
Ke	0.50	Entrance Loss	0.84 ft
Inlet Control Properties			
Inlet Control HW Elev.	4,472.93 ft	Flow Control	Submerged
Inlet Type: 10 - 45° skewed headwall		Area Full	80.0 ft²
K	0.49800	HDS 5 Chart	11
M	0.66700	HDS 5 Scale	4
C	0.03270	Equation Form	2
Y	0.75000		

Culvert Calculator Report CP5

Ive For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	4,463.00 ft	Headwater Depth/Height	1.63
Computed Headwater Elev.	4,462.50 ft	Discharge	695.00 cfs
Inlet Control HW Elev.	4,461.44 ft	Tailwater Elevation	4,457.00 ft
Outlet Control HW Elev.	4,462.50 ft	Control Type	Outlet Control

Grades

Upstream Invert	4,456.00 ft	Downstream Invert	4,455.00 ft
Length	80.00 ft	Constructed Slope	0.012500 ft/ft

Hydraulic Profile

Profile	CompositeM2PressureProfile	Depth, Downstream	3.35 ft
Slope Type	Mild	Normal Depth	N/A ft
Flow Regime	Subcritical	Critical Depth	3.35 ft
Velocity Downstream	10.38 ft/s	Critical Slope	0.023634 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.035
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties

Outlet Control HW Elev.	4,462.50 ft	Upstream Velocity Head	1.17 ft
Ke	0.50	Entrance Loss	0.59 ft

Inlet Control Properties

Inlet Control HW Elev.	4,461.44 ft	Flow Control	Submerged
Inlet Type	10 - 45° skewed headwall	Area Full	80.0 ft ²
K	0.49800	HDS 5 Chart	11
M	0.66700	HDS 5 Scale	4
C	0.03270	Equation Form	2
Y	0.75000		

Culvert Calculator Report CP1

olve For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	4,461.00 ft	Headwater Depth/Height	1.40
Computed Headwater Elev:	4,460.56 ft	Discharge	584.00 cfs
Inlet Control HW Elev.	4,460.56 ft	Tailwater Elevation	4,453.00 ft
Outlet Control HW Elev.	4,460.25 ft	Control Type	Inlet Control

Grades

Upstream Invert	4,453.54 ft	Downstream Invert	4,451.34 ft
Length	110.00 ft	Constructed Slope	0.020000 ft/ft

Hydraulic Profile

Profile	S2	Depth, Downstream	2.74 ft
Slope Type	Steep	Normal Depth	2.19 ft
Flow Regime	Supercritical	Critical Depth	4.19 ft
Velocity Downstream	17.79 ft/s	Critical Slope	0.003095 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	12.00 ft
Section Size	12 x 5 ft	Rise	5.00 ft
Number Sections	1		

Outlet Control Properties

Outlet Control HW Elev.	4,460.25 ft	Upstream Velocity Head	2.10 ft
Ke	0.20	Entrance Loss	0.42 ft

Inlet Control Properties

Inlet Control HW Elev.	4,460.56 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	60.0 ft²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

Culvert Calculator Report

CPOFF

Ive For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	4,690.00 ft	Headwater Depth/Height	1.45
Computed Headwater Elev:	4,689.81 ft	Discharge	687.00 cfs
Inlet Control HW Elev.	4,689.34 ft	Tailwater Elevation	4,685.00 ft
Outlet Control HW Elev.	4,689.81 ft	Control Type	Entrance Control

Grades

Upstream Invert	4,684.00 ft	Downstream Invert	4,680.00 ft
Length	120.00 ft	Constructed Slope	0.033333 ft/ft

Hydraulic Profile

Profile CompositePressureProfileS1S2		Depth, Downstream	5.00 ft
Slope Type	N/A	Normal Depth	1.50 ft
Flow Regime	N/A	Critical Depth	3.32 ft
Velocity Downstream	8.59 ft/s	Critical Slope	0.003256 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	10.00 ft
Section Size	10 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties

Outlet Control HW Elev.	4,689.81 ft	Upstream Velocity Head	1.66 ft
Ke	0.50	Entrance Loss	0.83 ft

Inlet Control Properties

Inlet Control HW Elev.	4,689.34 ft	Flow Control	Submerged
Inlet Details; 10 - 45° skewed headwall		Area Full	80.0 ft²
K	0.49800	HDS 5 Chart	11
M	0.66700	HDS 5 Scale	4
C	0.03270	Equation Form	2
Y	0.75000		

Culvert Calculator Report CP8

olve For: Headwater Elevation

Culvert Summary

Allowable HW Elevation	4,601.20 ft	Headwater Depth/Height	1.70
Computed Headwater Elev.	4,600.79 ft	Discharge	692.00 cfs
Inlet Control HW Elev.	4,600.79 ft	Tailwater Elevation	4,595.00 ft
Outlet Control HW Elev.	4,600.78 ft	Control Type	Inlet Control

Grades

Upstream Invert	4,594.00 ft	Downstream Invert	4,592.00 ft
Length	120.00 ft	Constructed Slope	0.016667 ft/ft

Hydraulic Profile

Profile	S2	Depth, Downstream	2.64 ft
Slope Type	Steep	Normal Depth	2.28 ft
Flow Regime	Supercritical	Critical Depth	3.87 ft
Velocity Downstream	16.37 ft/s	Critical Slope	0.003868 ft/ft

Section

Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 4 ft	Rise	4.00 ft
Number Sections	2		

Outlet Control Properties

Outlet Control HW Elev.	4,600.78 ft	Upstream Velocity Head	1.94 ft
Ke	0.50	Entrance Loss	0.97 ft

Inlet Control Properties

Inlet Control HW Elev.	4,600.79 ft	Flow Control	Submerged
Inlet Type	16' type; 10 - 45° skewed headwall	Area Full	64.0 ft²
K	0.49800	HDS 5 Chart	11
M	0.66700	HDS 5 Scale	4
C	0.03270	Equation Form	2
Y	0.75000		

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 17MAR05 TIME 14:40:36 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS-WRITE STAGE FREQUENCY, DSS-READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR. 5-YEAR EVENT
2 ID GENERATED 2/2005 BY WOOD RODGERS INC
3 ID -----
*
4 IT 2 17MAR78 0200 19MAR78 0200
5 IN 1
6 IO 3
*
7 KK EX1 RUNOFF FROM EXISTING AREA 1
8 BA 1.7296
9 PH 0.18 0.34 0.56 0.72 0.84 1.20 1.68 2.25
10 LS 0 81.8
11 UD 1.21
*
12 KK EX2 RUNOFF FROM EXISTING AREA 2
13 BA 0.6623
14 LS 0 74.6
15 UD 0.80
*
16 KK EX3 RUNOFF FROM EXISTING AREA 3
17 BA 2.2979
18 LS 0 80.27
19 UD 1.36
*
20 KK EX4 RUNOFF FROM EXISTING AREA 4
21 BA 0.2915
22 LS 0 80.5
23 UD 0.735
*
24 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
* IN OVERLAND SHALLOW FLOW
25 RD 618 0.014 0.04 TRAP 100 0.33
*
26 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
27 RD 850 0.009 0.03 TRAP 10 0.33
*
28 KK CP3 CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
29 HC 2
*
30 KK REX3_1 ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
31 RD 914 0.003 0.03 TRAP 10 0.33
*

```

1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
32 KK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

```



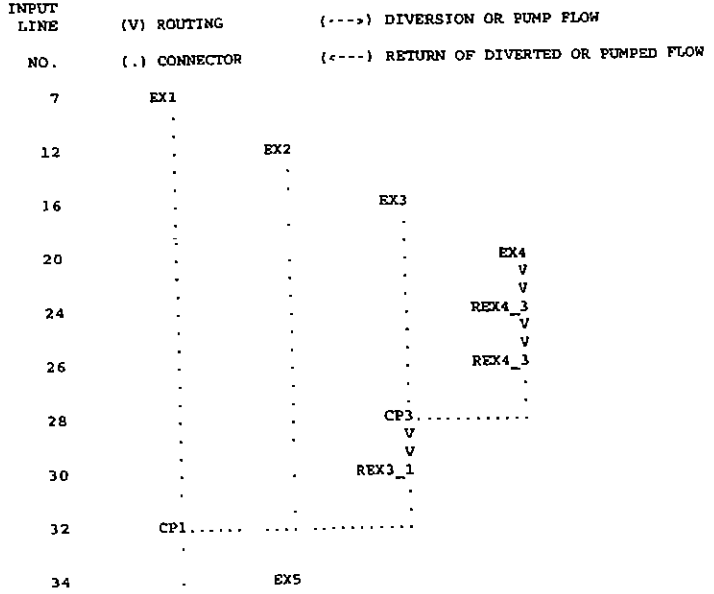
```

* CORNER OF SITE
33 HC 3
*
34 KK EX5 RUNOFF FROM OFFSITE AREA 5
35 BA 0.3020
36 LS 0 80.5
37 UD 0.51
*
38 ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4 1 *
* RUN DATE 17MAR05 TIME 14:40:36 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 5-YEAR EVENT
GENERATED 2/2005 BY WOOD RODGERS INC

```

6 10 OUTPUT CONTROL VARIABLES
      IPRNT 3 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
     NMIN 2 MINUTES IN COMPUTATION INTERVAL
     IDATE 17MAR78 STARTING DATE
     ITIME 0200 STARTING TIME
     NO 1441 NUMBER OF HYDROGRAPH ORDINATES
     NDDATE 19MAR78 ENDING DATE
     NDTIME 0200 ENDING TIME
     ICENT 19 CENTURY MARK

     COMPUTATION INTERVAL .03 HOURS
     TOTAL TIME BASE 48.00 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

```

*****
*           *
7 KK      EX1      *   RUNOFF FROM EXISTING AREA 1
*           *
*****

```

SUBBASIN RUNOFF DATA

```

8 BA      SUBBASIN CHARACTERISTICS
          TAREA      1.73  SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH      DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          HYDRO-35      TP-40      TP-49
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          18      .34      .56      .72      .84      1.20      1.68      2.25      .00      .00      .00      .00

          STORM AREA = 1.73

```

```

10 LS     SCS LOSS RATE
          STRL      .44  INITIAL ABSTRACTION
          CRVNBR    81.80  CURVE NUMBER
          RTIMP     .00  PERCENT IMPERVIOUS AREA

```

```

11 UD     SCS DIMENSIONLESS UNITGRAPH
          TLAG     1.21  LAG

```

UNIT HYDROGRAPH
183 END-OF-PERIOD ORDINATES

6.	11.	17	25	38.	50.	63.	79.	95.	112.
129.	151.	173.	195.	219.	249.	279.	308.	341.	376.
412.	447.	477.	506.	536.	563.	584.	604.	624.	640.
651.	662.	673.	676.	678.	680.	681.	679.	677.	675.
669.	657.	646.	635.	623.	610.	597.	583.	569.	554.
539.	522.	504.	485.	467.	445.	423.	401.	379.	361.
342.	324.	308.	295.	282.	269.	257.	246.	235.	224.
215.	206.	196.	188.	181.	174.	168.	161.	154.	147.
141.	135.	130.	124.	119.	113.	107.	102.	98.	94.
90.	87.	83.	79.	75.	72.	69.	66.	64.	61.
58.	55.	53.	50.	48.	46.	44.	42.	40.	38.
37.	35.	34.	32.	31.	30.	28.	27.	26.	25.
24.	23.	22.	21.	20.	19.	18.	18.	17.	16.
15.	15.	14.	13.	13.	12.	12.	11.	11.	10.
10.	9.	9.	9.	8.	8.	8.	7.	7.	7.
7.	6.	6.	6.	6.	6.	5.	5.	5.	5.
4.	4.	4.	4.	4.	3.	3.	3.	3.	3.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1.	0.	0.							

HYDROGRAPH AT STATION EX1

```

TOTAL RAINFALL = 2.24, TOTAL LOSS = 1.44, TOTAL EXCESS = .80

PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 172.         13.37          (CFS)
                    (INCHES)      .514      .805      .805      .805
                    (AC-FT)       47.       74.       74.       74.

CUMULATIVE AREA = 1.73 SQ MI

```

```

*****
*           *
12 KK     EX2      *   RUNOFF FROM EXISTING AREA 2
*           *
*****

```

SUBBASIN RUNOFF DATA

```

13 BA     SUBBASIN CHARACTERISTICS
          TAREA     .66  SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH      DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          HYDRO-35      TP-40      TP-49
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          18      .34      .56      .72      .84      1.20      1.68      2.25      .00      .00      .00      .00

          STORM AREA = .66

```

14 LS SCS LOSS RATE
 STRTL .68 INITIAL ABSTRACTION
 CRVNR 74.60 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

15 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .80 LAG

UNIT HYDROGRAPH
 122 END-OF-PERIOD ORDINATES

5.	10.	18.	29.	41.	55.	69.	87.	106.	127.
152.	178.	207.	237.	266.	292.	317.	336.	354.	368.
378.	387.	389.	391.	391.	389.	387.	378.	368.	358.
346.	335.	322.	309.	294.	278.	262.	242.	223.	207.
191.	176.	165.	154.	144.	135.	126.	118.	110.	104.
98.	92.	86.	81.	76.	71.	66.	61.	57.	54.
51.	47.	44.	41.	39.	36.	34.	32.	29.	28.
26.	24.	22.	21.	20.	19.	17.	16.	15.	14.
13.	13.	12.	11.	10.	10.	9.	8.	8.	7.
7.	6.	6.	6.	5.	5.	5.	4.	4.	4.
4.	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	1.	1.	1.	1.	1.	1.	0.
0.	0.								

HYDROGRAPH AT STATION EX2

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.75, TOTAL EXCESS = .49

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
45.	12 93	23	9.	4.	4.	
		(INCHES)	.317	.494	.494	.494
		(AC-FT)	11.	17.	17.	17.

CUMULATIVE AREA = .66 SQ MI

.....

16 KK EX3 RUNOFF FROM EXISTING AREA 3

SUBBASIN RUNOFF DATA

17 BA SUBBASIN CHARACTERISTICS
 TAREA 2.30 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = 2.30

18 LS SCS LOSS RATE
 STRTL .49 INITIAL ABSTRACTION
 CRVNR 80.27 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

19 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.36 LAG

UNIT HYDROGRAPH
 206 END-OF-PERIOD ORDINATES

6.	12.	18.	23.	36.	50.	63.	77.	94.	111.
129.	146.	167.	191.	214.	238.	265.	296.	327.	359.
392.	429.	466.	503.	539.	570.	601.	633.	663.	685.
706.	728.	749.	761.	773.	785.	796.	800.	802.	804.
806.	805.	803.	801.	799.	792.	780.	768.	756.	744.
730.	716.	703.	689.	673.	657.	642.	625.	606.	586.
567.	547.	524.	500.	477.	453.	434.	414.	395.	375.
360.	346.	333.	319.	307.	295.	283.	272.	261.	251.
241.	232.	223.	216.	209.	202.	194.	187.	180.	173.
166.	160.	154.	149.	143.	137.	131.	125.	119.	115.
111.	107.	103.	99.	96.	92.	88.	84.	82.	79.
76.	73.	70.	67.	64.	61.	59.	57.	55.	53.
51.	48.	46.	44.	43.	41.	40.	38.	37.	35.
34.	32.	31.	30.	29.	28.	27.	26.	25.	24.
23.	22.	21.	21.	20.	19.	18.	17.	17.	16.

16.	15.	14.	14.	13.	13.	12	12.	11.	11.
11	10.	10.	9.	9.	9.	8.	8.	8.	8.
8.	7.	7.	7.	7.	6.	6.	6.	6.	5.
5.	5.	5.	4.	4.	4.	4.	4.	3.	3.
3.	3.	3.	2.	2.	2.	2.	2.	1.	1
1.	1.	1.	0.	0.	0				

*** *** *** *** ***

HYDROGRAPH AT STATION EX3

TOTAL RAINFALL = 2.24, TOTAL LOSS = 1.51, TOTAL EXCESS = .73

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
188.	13.53	114.	45.	23.	23.
		(INCHES) .460	.729	.729	.729
		(AC-FT) 56.	89.	89.	89.

CUMULATIVE AREA = 2.30 SQ MI

.....

 20 KK * EX4 * RUNOFF FROM EXISTING AREA 4

SUBBASIN RUNOFF DATA

21 BA SUBBASIN CHARACTERISTICS
 TAREA .29 SUBBASIN AREA

PRECIPITATION DATA

9 PH	DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM										
	HYDRO-35	TP-40	TP-49								
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = .29

22 LS SCS LOSS RATE
 STRTL .48 INITIAL ABSTRACTION
 CRVNR 80.50 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

23 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .74 LAG

UNIT HYDROGRAPH
 112 END-OF-PERIOD ORDINATES

2.	5.	10.	16.	22.	30.	38.	48.	58.	71.
84.	99.	115.	130.	143.	156.	165.	174.	179.	184.
186.	187.	187.	186.	184.	180.	175.	169.	163.	157.
150	143.	134.	126.	116.	106.	97.	89.	82.	76.
71.	66.	61.	57.	53.	50.	47.	44.	41.	38.
35.	33.	30.	28.	26.	24.	23.	21.	20.	18.
17.	16.	15.	14.	13.	12.	11.	10.	9.	9.
8.	8.	7.	7.	6.	6.	5.	5.	5.	4.
4.	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.								

*** *** *** *** ***

HYDROGRAPH AT STATION EX4

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.51, TOTAL EXCESS = .74

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
17.	12.83	15.	6.	3.	3.
		(INCHES) .487	.744	.744	.744
		(AC-FT) 8.	12.	12.	12.

CUMULATIVE AREA = .29 SQ MI

.....

```

*****
*
24 KK * REX4_3 * ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
*
*****

```

HYDROGRAPH ROUTING DATA

```

25 RD MUSKINGUM-CUNGE CHANNEL ROUTING
      L 618. CHANNEL LENGTH
      S .0140 SLOPE
      N .040 CHANNEL ROUGHNESS COEFFICIENT
      CA .00 CONTRIBUTING AREA
      SHAPE TRAP CHANNEL SHAPE
      WD 100.00 BOTTOM WIDTH OR DIAMETER
      Z .33 SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	.22	1.64	2.00	123.60	36.52	774.00	74	2.05

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.22	1.64	2.00	36.52	774.00	.74
------	-----	------	------	-------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .2335E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION REX4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
37.	12.90	15.	6.	3.	3.
		(INCHES) .487	.744	.744	.744
		(AC-FT) 8.	12.	12.	12.

CUMULATIVE AREA = .29 SQ MI

```

*****
*
26 KK * REX4_3 * ROUTE RUNOFF FROM EXISTING AREA 4 TO CP1 IN DESERT WAY TRAP CHANNEL
*
*****

```

HYDROGRAPH ROUTING DATA

```

27 RD MUSKINGUM-CUNGE CHANNEL ROUTING
      L 850. CHANNEL LENGTH
      S .0090 SLOPE
      N .030 CHANNEL ROUGHNESS COEFFICIENT
      CA .00 CONTRIBUTING AREA
      SHAPE TRAP CHANNEL SHAPE
      WD 10.00 BOTTOM WIDTH OR DIAMETER
      Z .33 SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	1.25	1.50	2.00	283.33	36.52	776.00	74	4.56

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.25	1.50	2.00	36.52	776.00	.74
------	------	------	------	-------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .8896E-03 PERCENT ERROR= .0

HYDROGRAPH AT STATION REX4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
37.	12.93	15.	6.	3.	3.
	(INCHES)	.487	.744	.744	.744
	(AC-FT)	8.	12.	12.	12.
CUMULATIVE AREA =		.29 SQ MI			

28 KK *****
 * CP3 * CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
 * *

29 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
212.	13.47	129.	51.	25.	25.
	(INCHES)	.463	.730	.730	.730
	(AC-FT)	64.	101.	101.	101.
CUMULATIVE AREA =		2.59 SQ MI			

30 KK *****
 * REX3_1 * ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
 * *

HYDROGRAPH ROUTING DATA

31 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	514.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	.33	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	.72	1.50	2.00	457.00	211.94	810.00	5.67	

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.72	1.50	2.00	211.94	810.00	.73	
------	-----	------	------	--------	--------	-----	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= 1009E+03 EXCESS= .0000E+00 OUTFLOW= .1009E+03 BASIN STORAGE= .1381E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION REX3_1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR

(CFS)
 212. 13.50 129. 51. 25. 25.
 (INCHES) .463 730 .730 .730
 (AC-FT) 64. 101. 101. 101.
 CUMULATIVE AREA = 2.59 SQ MI

.....

 32 KK * * * * *
 * * * * * CPI * * * * *
 * * * * * FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST
 * * * * *

33 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CPI
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 + 419. 13.33 (CFS) 247. 97. 49. 49.
 (INCHES) .461 .725 .725 .725
 (AC-FT) 122. 193 193. 193.
 CUMULATIVE AREA = 4.98 SQ MI

.....

 34 KK * * * * *
 * * * * * EX5 * * * * *
 * * * * * RUNOFF FROM OFFSITE AREA 5
 * * * * *

SUBBASIN RUNOFF DATA

35 BA SUBBASIN CHARACTERISTICS
 TAREA .30 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00
 STORM AREA = .30

36 LS SCS LOSS RATE
 SRTTL .48 INITIAL ABSTRACTION
 CRVNR 80.50 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

37 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .51 LAG

UNIT HYDROGRAPH
 78 END-OF-PERIOD ORDINATES
 5. 13. 26. 41. 58. 79. 105. 134. 167. 197.
 225. 245. 261. 272. 276. 277. 275. 268. 257. 245.
 232. 218. 201. 182. 161. 143. 126. 113. 102. 92.
 83. 75. 69. 62. 56. 51. 46. 40. 37. 33.
 30. 27. 25. 22. 20. 18. 16. 14. 13. 12.
 11. 10. 9. 8. 7. 6. 6. 5. 5. 4.
 4. 3. 3. 3. 3. 2. 2. 2. 2. 2.
 1. 1. 1. 1. 1. 1. 0. 0. 0.

*** **

HYDROGRAPH AT STATION EX5

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.51, TOTAL EXCESS = .74

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 + (CFS)

+ 48. 12.57
 (INCHES) 16. 6. 3. 3.
 (AC-FT) 490 .744 744 744
 8. 12. 12. 12.

CUMULATIVE AREA = .30 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	EX1	172.	13.37	96.	37.	19.	1.73		
HYDROGRAPH AT	EX2	45	12.93	23.	9.	4.	.66		
HYDROGRAPH AT	EX3	188	13.53	114.	45.	23.	2.30		
HYDROGRAPH AT	EX4	37.	12.83	15.	6.	3.	.29		
ROUTED TO	REX4_3	37.	12.90	15.	6.	3.	.29		
ROUTED TO	REX4_3	37.	12.93	15	6.	3.	.29		
2 COMBINED AT	CP3	212.	13.47	129.	51.	25.	2.59		
ROUTED TO	REX3_1	212.	13.50	129.	51.	25.	2.59		
3 COMBINED AT	CP1	419.	13.33	247.	97	49.	4.98		
HYDROGRAPH AT	EX5	48.	12.57	16.	6.	3	.30		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
REX4_3	MANE	2.00	36.52	774.00	.74	2.00	36.52	774.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .2335E-02 PERCENT ERROR= .0									
REX4_3	MANE	2.00	36.52	776.00	.74	2.00	36.52	776.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .8896E-03 PERCENT ERROR= .0									
REX3_1	MANE	2.00	211.94	810.00	.73	2.00	211.94	810.00	.73
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1009E+03 EXCESS= .0000E+00 OUTFLOW= .1009E+03 BASIN STORAGE= .1381E-02 PERCENT ERROR= .0									

*** NORMAL END OF HEC-1 ***


```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 17MAR05 TIME 14 40:28 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

```

X X XXXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXX X
X X X X X
X X X X X
X X XXXXXXX XXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION, KINEMATIC WAVE, NEW FINITE DIFFERENCE ALGORITHM.

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 100-YEAR EVENT
2 ID GENERATED 2/2005 BY WOOD RODGERS INC
3 ID *****
*
4 IT 2 17MAR78 0200 19MAR78 0200
5 IN 1
6 IO 3
*
7 KK EX1 RUNOFF FROM EXISTING AREA 1
8 BA 1.7296
9 PH 0.41 0.78 1.29 1.39 1.48 1.93 2.87 4.14
10 LS 0 81.9
11 UD 1.21
*
12 KK EX2 RUNOFF FROM EXISTING AREA 2
13 BA 0.6623
14 PH 0.41 0.78 1.29 1.39 1.48 1.93 2.87 4.14
15 LS 0 74.6
16 UD 0.80
*
17 KK EX3 RUNOFF FROM EXISTING AREA 3
18 BA 2.2979
19 UD 1.36
*
20 KK EX4 RUNOFF FROM EXISTING AREA 4
21 BA 0.2915
22 LS 0 80.5
23 UD 0.735
*
24 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
* IN OVERLAND SHALLOW FLOW
25 RD 618 0.014 0.04 TRAP 100 0.33
*
26 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
27 RD 850 0.009 0.03 TRAP 10 0.33
*
28 KK CP3 CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
29 HC 2
*
30 KK REX3_1 ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
31 RD 914 0.003 0.03 TRAP 10 0.33
*

```

1

HEC-1 INPUT

PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
32 KK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

```

```

      *          CORNER OF SITE
33      HC          3
      *
34      KK          EX5  RUNOFF FROM OFFSITE AREA 5
35      BA          0.3020
36      LS          0      80.5
37      UD          0.51
      *
38      ZZ

```

1

SCHMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7      EX1
      .
12     .          EX2
      .
17     .          .          EX3
      .
20     .          .          .          EX4
      .          .          .          V
      .          .          .          V
24     .          .          .          REX4_3
      .          .          .          V
26     .          .          .          REX4_3
      .
28     .          .          .          CP3
      .          .          .          V
30     .          .          .          REX3_1
      .
32     .          .          .          CP1
      .
34     .          .          .          EX5

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998 *
*   VERSION 4.1 *
* RUN DATE 17MAR05 TIME 14:40:28 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 100-YEAR EVENT
 GENERATED 2/2005 BY WOOD RODGERS INC

```

6 IO      OUTPUT CONTROL VARIABLES
          IPRNT      3      PRINT CONTROL
          IPLOT      0      PLOT CONTROL
          QSCAL      0.    HYDROGRAPH PLOT SCALE

```

```

IT        HYDROGRAPH TIME DATA
          NMIN      2      MINUTES IN COMPUTATION INTERVAL
          IDATE     17MAR78 STARTING DATE
          ITIME     0200   STARTING TIME
          NQ        1441   NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    19MAR78 ENDING DATE
          NDTIME    0200   ENDING TIME
          ICENT     19     CENTURY MARK

```

```

          COMPUTATION INTERVAL .03 HOURS
          TOTAL TIME BASE      48.00 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME    ACRE-FEET
SURFACE AREA      ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

*****
*
*       EX1       *
*       *         *
*       *         *
*       *         *
*       *         *
*****
7 KK          RUNOFF FROM EXISTING AREA 1

```

SUBBASIN RUNOFF DATA

```

8 BA          SUBBASIN CHARACTERISTICS
              TAREA      1.73  SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH          DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
              HYDRO-35      TP-40      TP-49
              5-MIN 15-MIN 60-MIN  2-HR  3-HR  6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
              .41   .78   1.29   1.39  1.48  1.93  2.87  4.14   .00   .00   .00   .00
              STORM AREA = 1.73

```

```

10 LS        SCS LOSS RATE
              STR1L      .44  INITIAL ABSTRACTION
              CRVNR      81.80 CURVE NUMBER
              RTIMP      .00  PERCENT IMPERVIOUS AREA

```

```

11 UD        SCS DIMENSIONLESS UNITGRAPH
              TLAG      1.21  LAG

```

UNIT HYDROGRAPH
183 END-OF-PERIOD ORDINATES

6	11.	17.	25.	38.	50.	63.	79.	95.	112.
129.	151.	173.	195.	219.	249.	279.	308.	341.	376.
412.	447.	477.	506.	536.	563.	584.	604.	624.	640.
651.	662.	673.	676.	678.	680.	681.	679.	677.	675.
669.	657.	646.	635.	623.	610.	597.	583.	569.	554.
539.	522.	504.	485.	467.	445.	423.	401.	379.	361.
342.	324.	308.	295.	282.	269.	257.	246.	235.	224.
215.	206.	196.	188.	181.	174.	168.	161.	154.	147.
141.	135.	130.	124.	119.	113.	107.	102.	98.	94.
90.	87.	83.	79.	75.	72.	69.	66.	64.	61.
58.	55.	53.	50.	48.	46.	44.	42.	40.	38.
37.	35.	34.	32.	31.	30.	28.	27.	26.	25.
24.	23.	22.	21.	20.	19.	18.	18.	17.	16.
15.	15.	14.	13.	13.	12.	12.	11.	11.	10.
10.	9.	9.	9.	8.	8.	8.	7.	7.	7.
7.	6.	6.	6.	6.	6.	5.	5.	5.	5.
4.	4.	4.	4.	4.	3.	3.	3.	3.	3.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1.	0.	0.							

HYDROGRAPH AT STATION EX1

TOTAL RAINFALL = 4.13, TOTAL LOSS = 1.83, TOTAL EXCESS = 2.30

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR	
+						
+	579.	13.27	250.	107.	53.	53.
		(INCHES)	1.344	2.298	2.298	2.298
		(AC-FT)	124.	212.	212.	212.

CUMULATIVE AREA = 1.73 SQ MI

```

*****
*
*       EX2       *
*       *         *
*       *         *
*       *         *
*       *         *
*****
12 KK          RUNOFF FROM EXISTING AREA 2

```

SUBBASIN RUNOFF DATA

```

13 BA          SUBBASIN CHARACTERISTICS
              TAREA      .66  SUBBASIN AREA

```

PRECIPITATION DATA

```

14 PH          DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
              HYDRO-35      TP-40      TP-49
              5-MIN 15-MIN 60-MIN  2-HR  3-HR  6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
              .41   .78   1.29   1.39  1.48  1.93  2.87  4.14   .00   .00   .00   .00
              STORM AREA = .66

```

15 LS SCS LOSS RATE
 STRTL .68 INITIAL ABSTRACTION
 CRVNR 74.60 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

16 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .80 LAG

UNIT HYDROGRAPH
 122 END-OF-PERIOD ORDINATES

5.	10.	18.	29.	41.	55.	69.	87.	106.	127.
152.	178.	207.	237.	266.	292.	317.	336.	354.	368.
378.	387.	389.	391.	391.	389.	387.	378.	368.	358.
346.	335.	322.	309.	294.	278.	262.	242.	223.	207.
191.	176.	165.	154.	144.	135.	126.	118.	110.	104.
98.	92.	86.	81.	76.	71.	66.	61.	57.	54.
51.	47.	44.	41.	39.	36.	34.	32.	29.	28.
26.	24.	22.	21.	20.	19.	17.	16.	15.	14.
13.	13.	12.	11.	10.	10.	9.	8.	8.	7.
7.	6.	6.	6.	5.	5.	5.	4.	4.	4.
4.	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	1.	1.	1.	1.	1.	1.	0.
0.	0.								

*** **

HYDROGRAPH AT STATION EX2

TOTAL RAINFALL = 4.14, TOTAL LOSS = 2.40, TOTAL EXCESS = 1.74

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
228.	12.87	76.	31.	15.	15.	
		(INCHES)	1.060	1.740	1.740	1.740
		(AC-FT)	37.	61.	61.	61.

CUMULATIVE AREA = .66 SQ MI

.....

17 KK EX3 RUNOFF FROM EXISTING AREA J

SUBBASIN RUNOFF DATA

18 BA SUBBASIN CHARACTERISTICS
 TAREA 2.30 SUBBASIN AREA

PRECIPITATION DATA

14 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = 2.30

15 LS SCS LOSS RATE
 STRTL .68 INITIAL ABSTRACTION
 CRVNR 74.60 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

19 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.36 LAG

UNIT HYDROGRAPH
 206 END-OF-PERIOD ORDINATES

6.	12.	18.	23.	36.	50.	63.	77.	94.	111.
129.	146.	167.	191.	214.	238.	265.	296.	327.	359.
392.	429.	466.	503.	539.	570.	601.	633.	663.	685.
706.	728.	749.	761.	773.	785.	796.	800.	802.	804.
806.	805.	803.	801.	799.	792.	780.	768.	756.	744.
730.	716.	703.	689.	673.	657.	642.	625.	606.	586.
567.	547.	524.	500.	477.	453.	434.	414.	395.	375.
360.	346.	333.	319.	307.	295.	283.	272.	261.	251.
241.	232.	223.	216.	209.	202.	194.	187.	180.	173.
166.	160.	154.	149.	143.	137.	131.	125.	119.	115.
111.	107.	103.	99.	96.	92.	88.	84.	82.	79.
76.	73.	70.	67.	64.	61.	59.	57.	55.	53.
51.	48.	46.	44.	43.	41.	40.	38.	37.	35.
34.	32.	31.	30.	29.	28.	27.	26.	25.	24.
23.	22.	21.	21.	20.	19.	18.	17.	17.	16.

16.	15.	14.	14.	11.	13.	12.	12	11.	11.
11.	10.	10.	9	9.	9.	8.	8.	8.	8.
8.	7.	7	7.	7.	6.	6.	6.	6.	5.
5.	5.	5.	4	4.	4.	4.	4.	3.	3.
3.	3.	3.	2.	2.	2.	2.	2.	1.	1.
1.	1.	1.	0.	0.	0.				

*** *** *** *** ***

HYDROGRAPH AT STATION EK3

TOTAL RAINFALL = 4.13, TOTAL LOSS = 2.39, TOTAL EXCESS = 1.73

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
515.	13.43	(CFS)			
		252	107.	54.	54.
		(INCHES)	1.018	1.734	1.734
		(AC-FT)	125.	212.	212.

CUMULATIVE AREA = 2.30 SQ MI

.....

```

*****
*           *
*   EK4   *   RUNOFF FROM EXISTING AREA 4
*           *
*****

```

SUBBASIN RUNOFF DATA

21 BA SUBBASIN CHARACTERISTICS
TAREA .29 SUBBASIN AREA

PRECIPITATION DATA

14 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	00	00	.00

STORM AREA = .29

22 LS SCS LOSS RATE
STRTL .48 INITIAL ABSTRACTION
CRVNR 80.50 CURVE NUMBER
RTIMP 00 PERCENT IMPERVIOUS AREA

23 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 74 LAG

UNIT HYDROGRAPH
112 END-OF-PERIOD ORDINATES

2.	5.	10.	16.	22.	30.	38.	48.	58.	71.
84.	99.	115.	130.	143.	156.	165.	174.	179.	184.
186.	187.	187.	186.	184.	180.	175.	169.	163.	157.
150.	143.	134.	126.	116.	106.	97.	89.	82.	76.
71.	66.	61.	57.	53.	50.	47.	44.	41.	38.
35.	33.	30.	28.	26.	24.	23.	21.	20.	18.
17.	16.	15.	14.	13.	12.	11.	10.	9.	9.
8.	8.	7.	7.	6.	6.	5.	5.	5.	4.
4.	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0.								

*** *** *** *** ***

HYDROGRAPH AT STATION EK4

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.94, TOTAL EXCESS = 2.20

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
138.	12.80	(CFS)			
		41.	17.	9.	9.
		(INCHES)	1.322	2.197	2.197
		(AC-FT)	21.	34.	34.

CUMULATIVE AREA = 29 SQ MI

.....

```

*****
*
* 24 KK      * REX4_3 *      ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
*
*****

```

HYDROGRAPH ROUTING DATA

```

25 RD      MUSKINGUM-CUNGE CHANNEL ROUTING
           L      618.  CHANNEL LENGTH
           S      .0140 SLOPE
           N      .048  CHANNEL ROUGHNESS COEFFICIENT
           CA     .00  CONTRIBUTING AREA
           SHAPE  TRAP  CHANNEL SHAPE
           WD     100.00 BOTTOM WIDTH OR DIAMETER
           Z      .33  SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)					
MAIN	.22	1.64	2.00	206.00	137.53	770.00	2.20	3.45

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.22	1.64	2.00		137.53	770.00	2.20	
------	-----	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .2449E-02 PERCENT ERROR= 0

*** *** *** *** ***

HYDROGRAPH AT STATION REX4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
138.	12.83	41.	17.	9.	9.	
		(INCHES)	1.322	2.197	2.197	2.197
		(AC-FT)	21	34.	34.	34.

CUMULATIVE AREA = .29 SQ MI

.....

```

*****
*
* 26 KK      * REX4_3 *      ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
*
*****

```

HYDROGRAPH ROUTING DATA

```

27 RD      MUSKINGUM-CUNGE CHANNEL ROUTING
           L      850.  CHANNEL LENGTH
           S      .0090 SLOPE
           N      .030  CHANNEL ROUGHNESS COEFFICIENT
           CA     .00  CONTRIBUTING AREA
           SHAPE  TRAP  CHANNEL SHAPE
           WD     10.00 BOTTOM WIDTH OR DIAMETER
           Z      .33  SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)					
MAIN	1.25	1.50	2.00	425.00	137.43	771.55	2.20	7.09

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.25	1.50	2.00		137.33	772.00	2.20	
------	------	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .8090E-03 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION REX4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
137.	12 87	41.	17.	9.	9.
		(INCHES) 1.322	2.197	2.197	2.197
		(AC-FT) 21.	34.	34.	34.

CUMULATIVE AREA = .29 SQ MI

.....

 28 IK * CP3 * CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL

29 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
599.	13.27	293.	124.	62.	62.
		(INCHES) 1.051	1.786	1.786	1.786
		(AC-FT) 145.	247.	247.	247.

CUMULATIVE AREA = 2.59 SQ MI

.....

 30 KK * REX3_1 * ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL

HYDROGRAPH ROUTING DATA

31 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 914. CHANNEL LENGTH
 S .0030 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
			DT (MIN)	DX (FT)				
MAIN	.72	1.50	1.90	914.00	598.02	797.36	1.79	8.00

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.72	1.50	2.00		597.87	798.00	1.79	
------	-----	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= 2466E+03 EXCESS= .0000E+00 OUTFLOW= .2466E+03 BASIN STORAGE= .1345E-02 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION REX3_1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR

598. 13.30 (CFS) 293. 124. 62. 62.
 (INCHES) 1.050 1.786 1.786 1.786
 (AC-FT) 145. 247. 247. 247.
 CUMULATIVE AREA = 2.59 SQ MI

32 KK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

33 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP1
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 1154. 13.20 (CFS) 617. 262. 131. 131.
 (INCHES) 1.152 1.957 1.958 1.958
 (AC-FT) 306. 520. 520. 520.
 CUMULATIVE AREA = 4.98 SQ MI

34 KK EX5 RUNOFF FROM OFFSITE AREA 5

SUBBASIN RUNOFF DATA

35 BA SUBBASIN CHARACTERISTICS
 TAREA .30 SUBBASIN AREA

PRECIPITATION DATA

14 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .41 .78 1.29 1.39 1.48 1.93 2.87 4.14 .00 .00 .00 .00

STORM AREA = .30

36 LS SCS LOSS RATE
 STRTL .48 INITIAL ABSTRACTION
 CRUNBR 80.50 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

37 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .51 LAG

UNIT HYDROGRAPH
 78 END-OF-PERIOD ORDINATES

5.	13.	26.	41.	58.	79.	105.	134.	167.	197.
225.	245.	261.	272.	276.	277.	275.	268.	257.	245.
232.	218.	201.	182.	161.	143.	126.	113.	102.	92.
83.	75.	69.	62.	56.	51.	46.	40.	37.	33.
30.	27.	25.	22.	20.	18.	16.	14.	13.	12.
11.	10.	9.	8.	7.	6.	6.	5.	5.	4.
4.	3.	3.	3.	3.	2.	2.	2.	2.	2.
1.	1.	1.	1.	1.	1.	0.	0.		

HYDROGRAPH AT STATION EX5
 TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.94, TOTAL EXCESS = 2.20

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 (CFS)

+ 184. 12.57
 (INCHES) 43. 18. 9. 9.
 (AC-FT) 1.335 2.197 2.197 2.197
 22. 35 35. 35.

CUMULATIVE AREA = .30 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	EX1	579	13.27	250.	107.	53.	1.73		
HYDROGRAPH AT	EX2	228.	12.87	76.	31.	15.	.66		
HYDROGRAPH AT	EX3	515.	13.43	252.	107.	54.	2.30		
HYDROGRAPH AT	EX4	138.	12.80	41.	17.	9.	.29		
ROUTED TO	REX4_3	138.	12.83	41.	17.	9.	.29		
ROUTED TO	REX4_3	137.	12.87	41.	17.	9.	.29		
2 COMBINED AT	CP3	599.	13.27	293.	124.	62.	2.59		
ROUTED TO	REX3_1	598.	13.30	293.	124.	62.	2.59		
3 COMBINED AT	CP1	1354.	13.20	617.	262.	131.	4.98		
HYDROGRAPH AT	EX5	184.	12.57	43.	18.	9.	.30		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
REX4_3	MANE	2.00	137.53	770.00	2.20	2.00	137.53	770.00	2.20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .2449E-02 PERCENT ERROR= .0

REX4_3 MANE 2.00 137.43 771.55 2.20 2.00 137.33 772.00 2.20

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .8090E-03 PERCENT ERROR= .0

REX3_1 MANE 1.90 598.02 797.36 1.79 2.00 597.87 798.00 1.79

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2466E+03 EXCESS= .0000E+00 OUTFLOW= .2466E+03 BASIN STORAGE= .1345E-02 PERCENT ERROR= .0

*** NORMAL END OF HEC-1 ***

```

.....
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4 1
*
* RUN DATE 25MAR05 TIME 15.08.17
*
.....

```

```

.....
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
.....

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS-WRITE STAGE FREQUENCY, DSS-READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE-GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 5-YEAR EVENT
2 ID GENERATED 2/2005 BY WOOD RODGERS INC
3 ID -----
*
4 IT 2 17MAR78 0200 19MAR78 0200
5 IN 1
6 IO 3
*
7 KK EX1 RUNOFF FROM EXISTING AREA 1
8 BA 1.7296
9 PH 0.18 0.34 0.56 0.72 0.84 1.20 1.68 2.25
10 LS 0 81.8
11 UD 1.21
*
12 KK EX2 RUNOFF FROM EXISTING AREA 2
13 BA 0.6623
14 LS 0 74.6
15 UD 0.80
*
16 KK EX3 RUNOFF FROM EXISTING AREA 3
17 BA 2.2979
18 LS 0 80.27
19 UD 1.36
*
20 KK EX4 RUNOFF FROM EXISTING AREA 4
21 BA 0.2915
22 LS 0 80.5
23 UD 0.735
*
24 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
* IN OVERLAND SHALLOW FLOW
25 RD 618 0.014 0.04 TRAP 100 0.33
*
26 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
27 RD 850 0.009 0.03 TRAP 10 0.33
*
28 KK CP3 CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
29 HC 2
*
30 KK REX3_1 ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
31 RD 914 0.003 0.03 TRAP 10 0.33
*

```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
12 KK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

```

```

CORNER OF SITE
33      HC      3
      *
      *
34      KK      EX5  RUNOFF FROM OFFSITE AREA 5
35      BA      0 3020
36      LS      0    82 1
37      UD      0.51
      *
38      ZZ

```

1
SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO.        (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

7          EX1

12         .          EX2

16         .          .          EX3

20         .          .          .          EX4
          .          .          .          V
          .          .          .          V
24         .          .          .          REX4_3
          .          .          .          V
          .          .          .          V
26         .          .          .          REX4_3
          .          .          .          .

28         .          .          .          CP3
          .          .          .          V
          .          .          .          V
30         .          .          .          REX3_1
          .          .          .          .

32         CPI . . . . .

34         .          EX5

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998 *
*   VERSION 4 1 *
* RUN DATE 25MAR05 TIME 15.08.17 *
*****

```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 5-YEAR EVENT
GENERATED 2/2005 BY WOOD RODGERS INC

```

6 IO      OUTPUT CONTROL VARIABLES
          IPRNT      3  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      2  MINUTES IN COMPUTATION INTERVAL
          IDATE     17MAR78  STARTING DATE
          ITIME     0200  STARTING TIME
          NO        1441  NUMBER OF HYDROGRAPH ORDINATES
          NDDATE    19MAR78  ENDING DATE
          NDTIME    0200  ENDING TIME
          ICENT     19  CENTURY MARK

          COMPUTATION INTERVAL .03 HOURS
          TOTAL TIME BASE 48.00 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH  INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-Feet
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

*****
*
*   EX1   *   RUNOFF FROM EXISTING AREA 1
*
*****

```

SUBBASIN RUNOFF DATA

```

8 BA   SUBBASIN CHARACTERISTICS
      TAREA      1 73  SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH   DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
      ..... HYDRO-35 ..... TP-40 ..... TP-49 .....
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
      .18   34   56   72   84   1.20  1.68  2.25   .00   .00   .00   .00

      STORM AREA = 1.73

```

```

10 LS  SCS LOSS RATE
      STRTL      44  INITIAL ABSTRACTION
      CRVNR      81.80 CURVE NUMBER
      RTIMP      00  PERCENT IMPERVIOUS AREA

```

```

11 UD  SCS DIMENSIONLESS UNITGRAPH
      TLAG      1 21  LAG

```

UNIT HYDROGRAPH
183 END-OF-PERIOD ORDINATES

6.	11.	17	25	38.	50.	63.	79.	95.	112.
129.	151	173	195.	219.	249	279.	308.	341.	376.
412.	447	477.	506	536.	563.	584.	604.	624.	640.
651.	662	673	676.	678.	680.	681.	679.	677.	675.
669.	657.	646.	635.	623.	610.	597.	583.	569.	554.
539.	522.	504.	485.	467	445.	423.	401.	379.	361.
342.	324.	308	295.	282.	269	257.	246.	235.	224.
215.	206	196.	188	181.	174	168.	161.	154.	147.
141.	135	130	124	119.	113	107.	102.	98.	94.
90.	87	83	79.	75.	72.	69.	66.	64.	61.
58.	55	53.	50	48.	46	44.	42.	40.	38.
37.	35	34	32	31	30	28.	27.	26.	25.
24	23	22.	21	20.	19	18.	18.	17.	16.
15.	15	14	13.	13.	12.	12.	11.	11.	10.
10	9	9	9.	8.	8	8	7.	7.	7.
7.	6	6.	6.	6.	6	5	5.	5.	5.
4.	4	4.	4	4.	3	3.	3.	3.	3.
2.	2.	2.	2.	2.	1.	1	1.	1.	1.
1.	0.	0							

HYDROGRAPH AT STATION EX1

```

TOTAL RAINFALL = 2.24, TOTAL LOSS = 1.44, TOTAL EXCESS = 80

PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 172.         13.37          (CFS)
                        (INCHES)      .514      805      .805      .805
                        (AC-FT)       47.       74.       74       74.

CUMULATIVE AREA = 1.73 SQ MI

```

.....

```

*****
*
*   EX2   *   RUNOFF FROM EXISTING AREA 2
*
*****

```

SUBBASIN RUNOFF DATA

```

13 BA  SUBBASIN CHARACTERISTICS
      TAREA      66  SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH   DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
      ..... HYDRO-35 ..... TP-40 ..... TP-49 .....
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
      .18   .34   .56   .72   84   1.20  1.68  2.25   .00   .00   .00   .00

      STORM AREA = .66

```

14 LS SCS LOSS RATE
 STRTL .68 INITIAL ABSTRACTION
 CRVNR 74.60 CURVE NUMBER
 RTIMP 00 PERCENT IMPERVIOUS AREA

15 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .80 LAG

UNIT HYDROGRAPH
 122 END-OF-PERIOD ORDINATES

5.	10.	18.	29.	41.	55.	69.	87.	106.	127.
152.	178.	207.	237.	266.	292.	317.	336.	354.	368.
378.	387.	389.	391.	391.	389.	387.	378.	368.	358.
346.	335.	322.	309.	294.	278.	262.	242.	223.	207.
191.	176.	165.	154.	144.	135.	126.	118.	110.	104.
98.	92.	86.	81.	76.	71.	66.	61.	57.	54.
51.	47.	44.	41.	39.	36.	34.	32.	29.	28.
26.	24.	22.	21.	20.	19.	17.	16.	15.	14.
13.	13.	12.	11.	10.	10.	9.	8.	8.	7.
7.	6.	6.	6.	5.	5.	5.	4.	4.	4.
4.	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	1.	1.	1.	1.	1.	1.	0.
0.	0.								

HYDROGRAPH AT STATION EX2

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.75, TOTAL EXCESS = .49

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
45.	12.93	23.	9.	4.	4.	
		(INCHES)	.317	.494	.494	.494
		(AC-FT)	12	17.	17.	17.

CUMULATIVE AREA = .66 SQ MI

.....

16 KK EX3 RUNOFF FROM EXISTING AREA 3

SUBBASIN RUNOFF DATA

17 BA SUBBASIN CHARACTERISTICS
 TAREA 2.30 SUBBASIN AREA

PRECIPITATION DATA

DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49					
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = 2.30

18 LS SCS LOSS RATE
 STRTL .49 INITIAL ABSTRACTION
 CRVNR 80.27 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

19 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.36 LAG

UNIT HYDROGRAPH
 206 END-OF-PERIOD ORDINATES

6.	12.	18.	23.	36.	50.	63.	77.	94.	111.
129.	146.	167.	191.	214.	238.	265.	296.	327.	359.
392.	429.	466.	503.	539.	570.	601.	633.	663.	685.
706.	728.	749.	761.	773.	785.	796.	800.	802.	804.
806.	805.	803.	801.	799.	792.	780.	768.	756.	744.
730.	716.	703.	689.	673.	657.	642.	625.	606.	586.
567.	547.	524.	500.	477.	453.	434.	414.	395.	375.
360.	346.	333.	319.	307.	295.	283.	272.	261.	251.
241.	232.	223.	216.	209.	202.	194.	187.	180.	173.
166.	160.	154.	149.	143.	137.	131.	125.	119.	115.
111.	107.	103.	99.	96.	92.	88.	84.	82.	79.
76.	73.	70.	67.	64.	61.	59.	57.	55.	53.
51.	48.	46.	44.	43.	41.	40.	38.	37.	35.
34.	32.	31.	30.	29.	28.	27.	26.	25.	24.
23.	22.	21.	21.	20.	19.	18.	17.	17.	16.

16	15	14.	14.	13.	13.	12.	12.	11.	11.
11	10.	10.	9.	9.	9.	9.	8.	8.	8.
8	7.	7.	7.	7.	6.	6.	6.	6.	5.
5.	5	5	4.	4	4	4.	4.	3	3.
3	3.	3.	2	2	2	2	2.	1.	1.
1	1.	1.	0	0	0	0.	0.	0.	0.

HYDROGRAPH AT STATION EX3

TOTAL RAINFALL = 2.24, TOTAL LOSS = 1.51, TOTAL EXCESS = .73

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
188	13.53	114.	45.	23.	23.
		(INCHES)	.460	.729	.729
		(AC-FT)	56.	89.	89.

CUMULATIVE AREA = 2.30 SQ MI

.....

20 KK EX4 RUNOFF FROM EXISTING AREA 4

SUBBASIN RUNOFF DATA

21 BA SUBBASIN CHARACTERISTICS
TAREA .29 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35		TP-40						TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = .29

22 LS SCS LOSS RATE
SRTL 48 INITIAL ABSTRACTION
CRVNBR 80 50 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

23 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .74 LAG

UNIT HYDROGRAPH
112 END-OF-PERIOD ORDINATES

2	5.	10.	16.	22.	30.	38.	48.	58.	71
84.	99.	115.	130.	143.	156.	165.	174.	179.	184.
186	187.	187.	186.	184.	180.	175.	169.	163.	157.
150.	143.	134.	126.	116.	106.	97.	89.	82.	76.
71	66.	61.	57.	53.	50.	47.	44.	41.	38.
35	33.	30.	28.	26.	24.	23.	21.	20.	18.
17.	16.	15.	14.	13.	12.	11.	10.	9	9
8	8.	7.	7.	6.	6.	5.	5.	5.	4.
4	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1	1.	1.	1.	1.	1.	0.	0.	0.	0.
0.	0								

HYDROGRAPH AT STATION EX4

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.51, TOTAL EXCESS = .74

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
37	12.81	15.	6.	3.	3.
		(INCHES)	.487	.744	.744
		(AC-FT)	8.	12.	12.

CUMULATIVE AREA = .29 SQ MI

.....

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*****
*   REX4_3   *   ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
*****

```

HYDROGRAPH ROUTING DATA

```

25 RD   MUSKINGUM-CUNGE CHANNEL ROUTING
        L   618   CHANNEL LENGTH
        S   .0140 SLOPE
        N   .040   CHANNEL ROUGHNESS COEFFICIENT
        CA  .00   CONTRIBUTING AREA
        SHAPE TRAP CHANNEL SHAPE
        WD  100.00 BOTTOM WIDTH OR DIAMETER
        Z   .33   SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
MAIN	.22	1.64	2.00	36.52	774.00	.74	2.05

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.22	1.64	2.00	36.52	774.00	.74	
------	-----	------	------	-------	--------	-----	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= 1156E+02 BASIN STORAGE= 2335E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION REX4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
37.	12.90	15.	6.	3.	3.
		(INCHES) .487	.744	.744	.744
		(AC-FT) 8	12.	12.	12
CUMULATIVE AREA =		29 SQ MI			

.....

```

*****
*   REX4_3   *   ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
*****

```

HYDROGRAPH ROUTING DATA

```

27 RD   MUSKINGUM-CUNGE CHANNEL ROUTING
        L   850.   CHANNEL LENGTH
        S   .0090 SLOPE
        N   .030   CHANNEL ROUGHNESS COEFFICIENT
        CA  .00   CONTRIBUTING AREA
        SHAPE TRAP CHANNEL SHAPE
        WD  10.00  BOTTOM WIDTH OR DIAMETER
        Z   .33   SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
MAIN	1.25	1.50	2.00	36.52	776.00	.74	4.56

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.25	1.50	2.00	36.52	776.00	.74	
------	------	------	------	-------	--------	-----	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .8096E-03 PERCENT ERROR= .0

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  REX4_3
PEAK FLOW      TIME
+ (CFS)        (HR)
+ 37.          12.93
                (CFS)
                (INCHES)
                (AC-FT)
                6-HR      24-HR      72-HR      48.00-HR
                15.        6          3.          3.
                .487      .744      .744      744
                8         12.       12.       12.
CUMULATIVE AREA = 29 SQ MI

```

.....

```

*****
*          *
* 28 KK    * CP3 * CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
*          *
*****

```

```

29 HC          HYDROGRAPH COMBINATION
                ICOMP          2 NUMBER OF HYDROGRAPHS TO COMBINE

```

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  CP3
PEAK FLOW      TIME
+ (CFS)        (HR)
+ 212.         13.47
                (CFS)
                (INCHES)
                (AC-FT)
                6-HR      24-HR      72-HR      48.00-HR
                129       51         25.        25
                .463     .730     .730     .730
                64       101.     101.     101.
CUMULATIVE AREA = 2.59 SQ MI

```

.....

```

*****
*          *
* 30 KK    * REX3_1 * ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
*          *
*****

```

```

HYDROGRAPH ROUTING DATA
31 RD          MUSKINGUM-CUNGE CHANNEL ROUTING
                L          914. CHANNEL LENGTH
                S          .0030 SLOPE
                N          .030 CHANNEL ROUGHNESS COEFFICIENT
                CA         .00 CONTRIBUTING AREA
                SHAPE      TRAP CHANNEL SHAPE
                WD         10.00 BOTTOM WIDTH OR DIAMETER
                Z          .33 SIDE SLOPE

```

```

***
COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP
ELEMENT  ALPHA  H      DT      DX      PEAK  TIME TO  VOLUME  MAXIMUM
                (MIN) (FT)  (CFS)  (MIN)  (IN)   (FPS)
MAIN     .72   1.50   2.00   457.00  211.94  810.00   .73    5.67

```

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

MAIN     .72   1.50   2.00           211.94  810.00   .73

```

CONTINUITY SUMMARY (AC-FT) ~ INFLOW= 1.009E+03 EXCESS= .0000E+00 OUTFLOW= .1009E+03 BASIN STORAGE= .1381E-02 PERCENT ERROR= .0

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  REX3_1
PEAK FLOW      TIME
+ (CFS)        (HR)
+
                6-HR      24-HR      72-HR      48.00-HR

```


212 13 50 (CFS) 129. 51. 25 25.
 (INCHES) .463 730 .730 730
 (AC-FT) 64. 101 101 101.
 CUMULATIVE AREA = 2.59 SQ MI

32 XK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

33 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP1
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 419 13.33 (CFS) 247 97. 49. 49.
 (INCHES) .461 .725 .725 .725
 (AC-FT) 122. 193. 193. 193.
 CUMULATIVE AREA = 4.98 SQ MI

34 KK EX5 RUNOFF FROM OFFSITE AREA 5

SUBBASIN RUNOFF DATA
 35 BA SUBBASIN CHARACTERISTICS
 TAREA .30 SUBBASIN AREA

PRECIPITATION DATA
 9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 18 .34 .56 .72 .84 1.20 1.68 2.25 00 .00 00 .00
 STORM AREA = .30

36 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNR 82.10 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

37 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .51 LAG

UNIT HYDROGRAPH
 78 END-OF-PERIOD ORDINATES
 5. 13. 26. 41. 58. 79. 105. 134. 167. 197.
 225. 245. 261. 272. 276. 277. 275. 268. 257. 245.
 232. 218. 201. 182. 161. 143. 126. 113. 102. 92.
 83. 75. 69. 62. 56. 51. 46. 40. 37. 33.
 30. 27. 25. 22. 20. 18. 16. 14. 13. 12.
 11. 10 9. 8. 7. 6. 6. 5 5 4.
 4. 3. 3. 3. 3. 2. 2. 2. 2. 2.
 1. 1. 1. 1. 1. 1. 0. 0. 0. 0.

HYDROGRAPH AT STATION EX5
 TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = .82

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 (CFS)

* 54. 12.57
 (INCHES) .541 .18. 7. 3 3
 (AC-FT) 9. 13 .823 .823 823
 CUMULATIVE AREA = .30 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	EX1	172	13.37	96.	37.	19.	2.73		
HYDROGRAPH AT	EX2	45	12.93	23	9.	4	.66		
HYDROGRAPH AT	EX3	188.	13.53	114	45.	23.	2.30		
HYDROGRAPH AT	EX4	37.	12.83	15.	6	3.	.29		
ROUTED TO	REX4_3	37.	12.90	15.	6.	3.	.29		
ROUTED TO	REX4_3	37	12.93	15.	6.	3.	.29		
2 COMBINED AT	CP3	212.	13.47	129.	51.	25.	2.59		
ROUTED TO	REX3_1	212.	13.50	129	51.	25.	2.59		
3 COMBINED AT	CP1	419.	13.33	247	97.	49.	4.98		
HYDROGRAPH AT	EX5	54	12.57	18	7.	3.	.30		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
REX4_3	MANE	2.00	36.52	774.00	.74	2.00	36.52	774.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .2335E-02 PERCENT ERROR= .0									
REX4_3	MANE	2.00	36.52	776.00	.74	2.00	36.52	776.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1156E+02 EXCESS= .0000E+00 OUTFLOW= .1156E+02 BASIN STORAGE= .8996E-03 PERCENT ERROR= .0									
REX3_1	MANE	2.00	211.94	810.00	.73	2.00	211.94	810.00	.73
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1009E+03 EXCESS= .0000E+00 OUTFLOW= .1009E+03 BASIN STORAGE= .1381E-02 PERCENT ERROR= .0									

*** NORMAL END OF HEC-1 ***

```

.....
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
* RUN DATE 25MAR05 TIME 15:07:19
.....

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.....
* U. S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
.....

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X X XXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXX XXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMSBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS.WRITE STAGE FREQUENCY, DSS.READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 100-YEAR EVENT
2 ID GENERATED 2/2005 BY WOOD RODGERS INC
3 ID *****
*
4 IT 2 17MAR78 0200 19MAR78 0200
5 IN 1
6 IO 3
*
7 KK EX1 RUNOFF FROM EXISTING AREA 1
8 BA 1.7296
9 PH 0.41 0.78 1.29 1.39 1.48 1.93 2.87 4.14
10 LS 0 81.8
11 UD 1.21
*
12 KK EX2 RUNOFF FROM EXISTING AREA 2
13 BA 0.6623
14 PH 0.41 0.78 1.29 1.39 1.48 1.93 2.87 4.14
15 LS 0 74.6
16 UD 0.80
*
17 KK EX3 RUNOFF FROM EXISTING AREA 3
18 BA 2.2979
19 UD 1.36
*
20 KK EX4 RUNOFF FROM EXISTING AREA 4
21 BA 0.2915
22 LS 0 80.5
23 UD 0.735
*
24 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
* IN OVERLAND SHALLOW FLOW
25 RD 618 0.014 0.04 TRAP 100 0.33
*
26 KK REX4_3 ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
27 RD 850 0.009 0.03 TRAP 10 0.33
*
28 KK CP3 CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
29 HC 2
*
30 KK REX3_1 ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
31 RD 914 0.003 0.03 TRAP 10 0.33
*

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1

HEC-1 INPUT

PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
32 KK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

```

33	*	HC	3	CORNER OF SITE
	*			
34	KK	EX5	RUNOFF FROM OFFSITE AREA 5	
35	BA	0.3020		
36	LS	0	82 1	
17	UD	0.51		
	*			
38	ZZ			

1
SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	() CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
7	EX1	.
12	EX2	.
17	EX3	.
20	EX4	V
	V	
	V	
24	REX4_3	V
	V	
	V	
26	REX4_3	.
	.	
	.	
28	CP3
	V	
	V	
30	REX3_1	.
	.	
	.	
32	CP1
	.	
34	EX5	.

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*   FLOOD HYDROGRAPH PACKAGE (HEC-1)   *
*         JUN 1998                  *
*       VERSION 4.1                  *
* RUN DATE 25MAR05 TIME 15:07.19    *
*****

```

```

*****
*   U.S. ARMY CORPS OF ENGINEERS     *
*   HYDROLOGIC ENGINEERING CENTER    *
*   609 SECOND STREET                *
*   DAVIS, CALIFORNIA 95616          *
*   (916) 756-1104                   *
*****

```

GOLDEN HILLS SUBDIVISION EXISTING CONDITIONS 24-HOUR, 100-YEAR EVENT
GENERATED 2/2005 BY WOOD RODGERS INC

6 IO OUTPUT CONTROL VARIABLES

I	IPRINT	3	PRINT CONTROL
	IPLOT	0	PLOT CONTROL
	QSCAL	0.	HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

	NMIN	2	MINUTES IN COMPUTATION INTERVAL
	IDATE	17MAR78	STARTING DATE
	ITIME	0200	STARTING TIME
	NQ	1441	NUMBER OF HYDROGRAPH ORDINATES
	NDDATE	19MAR78	ENDING DATE
	NDDTIME	0200	ENDING TIME
	ICENT	19	CENTURY MARK

	COMPUTATION INTERVAL	.03 HOURS
	TOTAL TIME BASE	48.00 HOURS

ENGLISH UNITS

DRAINAGE AREA	SQUARE MILES
PRECIPITATION DEPTH	INCHES
LENGTH, ELEVATION	FEET
FLOW	CUBIC FEET PER SECOND
STORAGE VOLUME	ACRE-FEET
SURFACE AREA	ACRES
TEMPERATURE	DEGREES FAHRENHEIT

```

*****
*          *
7 KK      * EX1 *          RUNOFF FROM EXISTING AREA 1
*          *
*****

```

SUBBASIN RUNOFF DATA

```

8 BA      SUBBASIN CHARACTERISTICS
          TAREA      1.73  SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH      DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          HYDRO-35      TP-40      TP-49
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          .41   .78   1.29   1.39  1.48  1.93  2.87  4.14   .00   .00   .00   .00

          STORM AREA = 1.73

```

```

10 LS     SCS LOSS RATE
          STRTL      .44  INITIAL ABSTRACTION
          CRVMBR     81.80 CURVE NUMBER
          RTIMP      .00  PERCENT IMPERVIOUS AREA

11 UD     SCS DIMENSIONLESS UNITGRAPH
          TLAG      1.21  LAG

```

UNIT HYDROGRAPH
183 END-OF-PERIOD ORDINATES

6.	11.	17.	25.	38.	50.	63.	79.	95.	112.
129.	151.	173.	195.	219.	249.	279.	308.	341.	376.
412.	447.	477.	506.	536.	563.	584.	604.	624.	640.
651.	662.	673.	676.	678.	680.	681.	679.	677.	675.
669.	657.	646.	635.	623.	610.	597.	583.	569.	554.
539.	522.	504.	485.	467.	445.	423.	401.	379.	361.
342.	324.	308.	295.	282.	269.	257.	246.	235.	224.
215.	206.	196.	188.	181.	174.	168.	161.	154.	147.
141.	135.	130.	124.	119.	113.	107.	102.	98.	94.
90.	87.	83.	79.	75.	72.	69.	66.	64.	61.
58.	55.	53.	50.	48.	46.	44.	42.	40.	38.
37.	35.	34.	32.	31.	30.	28.	27.	26.	25.
24.	23.	22.	21.	20.	19.	18.	18.	17.	16.
15.	15.	14.	13.	13.	12.	12.	11.	11.	10.
10.	9.	9.	9.	8.	8.	8.	7.	7.	7.
7.	6.	6.	6.	6.	6.	5.	5.	5.	5.
4.	4.	4.	4.	4.	3.	3.	3.	3.	3.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1.	0.	0.							

HYDROGRAPH AT STATION EX1

```

TOTAL RAINFALL = 4.13, TOTAL LOSS = 1.83, TOTAL EXCESS = 2.30

PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 579.         13.27
-              (CFS)
              (INCHES)  250.      107.      53.      53.
              (AC-FT)  1.344    2.298    2.298    2.298
              (AC-FT)  124.     212     212     212

CUMULATIVE AREA = 1.73 SQ MI

```

```

*****
*          *
12 KK     * EX2 *          RUNOFF FROM EXISTING AREA 2
*          *
*****

```

SUBBASIN RUNOFF DATA

```

13 BA     SUBBASIN CHARACTERISTICS
          TAREA      66  SUBBASIN AREA

```

PRECIPITATION DATA

```

14 PH     DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          HYDRO-35      TP-40      TP-49
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          .41   .78   1.29   1.39  1.48  1.93  2.87  4.14   .00   .00   .00   .00

          STORM AREA = .66

```

15 LS SCS LOSS RATE
 STRTL .68 INITIAL ABSTRACTION
 CRVNBR 74.60 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

16 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .80 LAG

UNIT HYDROGRAPH
 122 END-OF-PERIOD ORDINATES

5.	10.	18.	29.	41.	55	69.	87.	106.	127.
152.	178.	207.	237.	266.	292.	317.	336.	354.	368.
178.	187.	189.	191.	191.	189.	187.	178.	168.	158.
146.	135.	122.	109.	94.	78.	62.	42.	23.	207.
191.	176.	165.	154.	144.	135.	126.	118.	110.	104.
98.	92.	86.	81.	76.	71.	66.	61.	57.	54.
51.	47.	44.	41.	39.	36.	34.	32.	29.	28.
26.	24.	22.	21.	20.	19.	17.	16.	15.	14.
13.	13.	12.	11.	10.	10.	9.	8.	8.	7.
7.	6.	6.	6.	5.	5.	5.	4.	4.	4.
4.	4.	3.	3.	3.	3.	3.	2.	2.	2.
2.	2.	2.	1.	1.	1.	1.	1.	1.	0.
0.	0.								

HYDROGRAPH AT STATION EX2

TOTAL RAINFALL = 4.14, TOTAL LOSS = 2.40, TOTAL EXCESS = 1.74

PEAK FLOW	TIME	6-HR	24-HR	72-HR	48 00-HR
(CFS)	(HR)	(CFS)	(INCHES)	(AC-FT)	
228.	12 87	76.	31.	15.	15.
		1.060	1.740	1.740	1.740
		37.	61.	61.	61

CUMULATIVE AREA = .66 SQ MI

.....

17 KK EX3 RUNOFF FROM EXISTING AREA 3

SUBBASIN RUNOFF DATA

18 BA SUBBASIN CHARACTERISTICS
 TAREA 2.30 SUBBASIN AREA

PRECIPITATION DATA

14 PH	DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM											
	HYDRO-35			TP-40				TP-49				
	5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
	.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = 2.30

15 LS SCS LOSS RATE
 STRTL .68 INITIAL ABSTRACTION
 CRVNBR 74.60 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

19 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.36 LAG

UNIT HYDROGRAPH
 206 END-OF-PERIOD ORDINATES

6	12.	18.	23.	36	50.	63.	77.	94.	111.
129.	146.	167.	191	214.	238.	265.	296.	327.	359.
392.	429.	466.	503.	539.	570.	601.	633.	663.	685.
706.	728.	749.	761.	773.	785.	796.	800.	802.	804.
806.	805.	803.	801.	799.	792.	780.	768.	756.	744.
730.	716.	703.	689.	673.	657.	642.	625.	606.	586.
567.	547.	524.	500.	477.	453.	434.	414.	395.	375.
360.	346.	333.	319.	307.	295.	283.	272.	261.	251.
241.	232.	223.	216.	209.	202.	194.	187.	180.	173.
166.	160.	154.	149.	143.	137.	131.	125.	119.	115.
111.	107.	103.	99.	96.	92.	88.	84.	79.	79.
76.	73.	70.	67.	64.	61.	59.	57.	55.	53.
51.	48.	46.	44.	43.	41.	40.	38.	37.	35.
34.	32.	31.	30.	29.	28.	27.	26.	25.	24.
23	22.	21.	21.	20	19.	18.	17.	17	16.

16.	15	14.	14	13.	13	12.	12.	11	11.
11	10	10.	9.	9	9	8.	8	8	8
8.	7.	7.	7	7	6	6	6	6	5.
5	5.	5	4.	4	4	4.	4	3.	3.
3	3	3.	2.	2	2	2	2	1.	1
1	1	1.	0.	0.	0				

*** *** *** *** ***

HYDROGRAPH AT STATION EX3

TOTAL RAINFALL = 4.13, TOTAL LOSS = 2.39, TOTAL EXCESS = 1.73

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48 00-HR	
515.	13.43	252.	107	54	54.	
		(INCHES)	1.018	1.734	1.734	1.734
		(AC-FT)	125.	212.	212.	212.

CUMULATIVE AREA = 2.30 SQ MI

.....

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*****
*           *
*   EX4   *   RUNOFF FROM EXISTING AREA 4
*           *
*****

```

SUBBASIN RUNOFF DATA

21 BA SUBBASIN CHARACTERISTICS
TAREA .29 SUBBASIN AREA

PRECIPITATION DATA

14 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	78	1.29	1.39	1.48	1.93	2.87	4.14	00	.00	.00	.00

STORM AREA = .29

22 LS SCS LOSS RATE
STRTL 48 INITIAL ABSTRACTION
CRVNR 80.50 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

23 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 74 LAG

UNIT HYDROGRAPH
112 END-OF-PERIOD ORDINATES

2.	5.	10	16.	22.	30.	38	48.	58	71.
84.	99.	115.	130.	143.	156.	165.	174	179	184.
186	187.	187	186	184.	180.	175.	169.	163.	157.
150.	143.	134.	126.	116.	106.	97.	89.	82.	76.
71	66.	61.	57.	53.	50	47.	44.	41.	38.
35.	33.	30.	28.	26.	24.	23.	21.	20.	18.
17.	16.	15	14	13.	12.	11.	10.	9.	9.
8.	8.	7.	7	6.	6	5.	5.	5.	4.
4.	4.	3	3.	3.	3.	3.	2.	2	2.
2.	2.	2	2.	2.	2.	1.	1.	1.	1.
1.	1.	1.	1	1.	1.	0.	0.	0.	0.
0.	0.								

*** *** *** *** ***

HYDROGRAPH AT STATION EX4

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.94, TOTAL EXCESS = 2.20

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
138.	12.80	41.	17.	9.	9.	
		(INCHES)	1.322	2.197	2.197	2.197
		(AC-FT)	21.	34.	34.	34.

CUMULATIVE AREA = .29 SQ MI

.....

24 KK * REX4_3 * ROUTE RUNOFF FROM EXISTING AREA 4 TO DESERT WAY
 * * * * * * * * * * * * * * * *

HYDROGRAPH ROUTING DATA

25 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 618 CHANNEL LENGTH
 S 0140 SLOPE
 N 040 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 100 00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	.22	1 64	2 00	206.00	137.53	770.00	2.20	3.45

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.22	1.64	2 00		137.53	770.00	2.20	
------	-----	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= 2449E-02 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION REX4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
138.	12.83	41.	17.	9.	9.
		(INCHES) 1.322	2.197	2.197	2.197
		(AC-FT) 21	34	34.	34.

CUMULATIVE AREA = 29 SQ MI

.....

26 KK * REX4_3 * ROUTE RUNOFF FROM EXISTING AREA 4 TO CP3 IN DESERT WAY TRAP CHANNEL
 * * * * * * * * * * * * * * *

HYDROGRAPH ROUTING DATA

27 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 850. CHANNEL LENGTH
 S .0090 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10 00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	1.25	1.50	2.00	425.00	137.43	771.55	2.20	7.09

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.25	1.50	2.00		137.33	772.00	2.20	
------	------	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .8090E-03 PERCENT ERROR= .0


```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  REX4_3
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)      6-HR      24-HR      72-HR      48.00-HR
+ 137          12.87      (CFS)
                               41          17          9          9
                               (INCHES)  1.322      2.197      2.197      2.197
                               (AC-FT)   21         34         34         34
CUMULATIVE AREA = 19 SQ MI

```

```

*****
*          *
28 KK      * CP3      * CONCENTRATION OF EX3 AND EX4 WITHIN DESERT WAY CHANNEL
*          *
*****

```

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29 HC      HYDROGRAPH COMBINATION
           ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

```

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  CP3
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)      6-HR      24-HR      72-HR      48.00-HR
+ 599          13.27      (CFS)
                               293         124         62         62
                               (INCHES)  1.051      1.786      1.786      1.786
                               (AC-FT)   145        247        247        247
CUMULATIVE AREA = 2.59 SQ MI

```

```

*****
*          *
30 KK      * REX3_1    * ROUTE CP3 TO CP1 IN DESERT WAY CHANNEL
*          *
*****

```

```

HYDROGRAPH ROUTING DATA
31 RD      MUSKINGUM-CUNGE CHANNEL ROUTING
           L      914. CHANNEL LENGTH
           S      0030 SLOPE
           N      030 CHANNEL ROUGHNESS COEFFICIENT
           CA     00 CONTRIBUTING AREA
           SHAPE  TRAP CHANNEL SHAPE
           WD     10 00 BOTTOM WIDTH OR DIAMETER
           Z      33 SIDE SLOPE

```

```

***
COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP
ELEMENT  ALPHA  M      DT      DK      PEAK  TIME TO  VOLUME  MAXIMUM
          .72  1.50  1.90  914.00  598.02  797.36  1.79    CELERITY
          (MIN) (FT)  (CFS)  (MIN)

```

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

ELEMENT  ALPHA  M      DT      DK      PEAK  TIME TO  VOLUME
          .72  1.50  2.00          597.87  798.00  1.79

```

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2466E+03 EXCESS= 0000E+00 OUTFLOW= .2466E+03 BASIN STORAGE= .1345E-02 PERCENT ERROR= .0

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  REX3_1
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)      6-HR      24-HR      72-HR      48.00-HR

```

598. 13 30 (CFS) 293. 124. 62. 62
 (INCHES) 1.050 1.786 1.786 1.786
 (AC-FT) 145. 247 247. 247

CUMULATIVE AREA = 2.59 SQ MI

32 KK CP1 FINAL CONCENTRATION POINT WITHIN DESERT WAY CHANNEL IN NORTHWEST

33 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
1354.	13.20	617	262	131.	131.
		1,152	1,957	1,958	1,958
		306	520.	520.	520.

CUMULATIVE AREA = 4.98 SQ MI

34 KK EX5 RUNOFF FROM OFFSITE AREA 5

SUBBASIN RUNOFF DATA

35 BA SUBBASIN CHARACTERISTICS
 TAREA .30 SUBBASIN AREA

PRECIPITATION DATA

14 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35		TP-40						TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	00	.00

STORM AREA = .30

36 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNR 82.10 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

17 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .51 LAG

UNIT HYDROGRAPH
 78 END-OF-PERIOD ORDINATES

5.	13.	26.	41	58.	79.	105.	134.	167.	197.
225.	245.	261	272.	276.	277.	275.	268.	257.	245.
232.	218.	201.	182.	161.	143.	126.	113.	102.	92.
83.	75	69.	62.	56.	51.	46	40	37.	33.
30	27	25.	22.	20.	18.	16	14.	13.	12.
11	10	9.	8.	7	6.	6	5.	5.	4.
4.	3.	3.	3.	3.	2.	2.	2.	2.	2.
1.	1.	1.	1.	1.	1.	0	0.		

HYDROGRAPH AT STATION EX5

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.81, TOTAL EXCESS = 2.33

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
		(CFS)			

+ 195. 12 57
 (INCHES) 46 19. 9. 9
 (AC-FT) 1.405 2.330 2.330 2.330
 23. 38 38. 38.
 CUMULATIVE AREA = .30 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	EX1	579	13.27	250.	107.	53	1.73		
HYDROGRAPH AT	EX2	228.	12.87	76.	31.	15.	.66		
HYDROGRAPH AT	EX3	515.	13.43	252.	107.	54.	2.30		
HYDROGRAPH AT	EX4	138.	12.80	41	17.	9.	.29		
ROUTED TO	REX4_3	138.	12.83	41.	17.	9.	.29		
ROUTED TO	REX4_3	137.	12.87	41.	17.	9.	.29		
2 COMBINED AT	CP3	599	13.27	293.	124.	62.	2.59		
ROUTED TO	REX3_1	598.	13.30	293.	124.	62.	2.59		
3 COMBINED AT	CP1	1354	13.20	617.	262.	131.	4.98		
HYDROGRAPH AT	EX5	195.	12.57	46.	19.	9.	.30		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
REX4_3	MANE	2.00	137.53	770.00	2.20	2.00	137.53	770.00	2.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= 0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .2449E-02 PERCENT ERROR= .0									
REX4_3	MANE	2.00	137.43	771.55	2.20	2.00	137.33	772.00	2.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3416E+02 EXCESS= .0000E+00 OUTFLOW= .3416E+02 BASIN STORAGE= .8090E-03 PERCENT ERROR= .0									
REX3_1	MANE	1.90	598.02	797.36	1.79	2.00	597.87	798.00	1.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2466E+03 EXCESS= 0000E+00 OUTFLOW= .2466E+03 BASIN STORAGE= .1345E-02 PERCENT ERROR= .0									

*** NORMAL END OF HEC-1 ***

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 25MAR05 TIME 15:10 03 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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X X XXXXXXX XXXXX X
X X X X X XK
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X X X X X X
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X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION.

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION, KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM.

1

HEC-1 INPUT

PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID GOLDEN HILLS SUBDIVISION PROPOSED CONDITIONS 24-HOUR, 5-YEAR EVENT
2 ID GENERATED 3/2005 BY WOOD RODGERS INC
3 ID *****
4 IT 2 17MAR78 0200 19MAR78 0200
5 IN 1
6 IO 3
*
7 KK OFF4 RUNOFF FROM OFFSITE AREA 4
8 BA 0.2070
9 PH 0 18 0.34 0.56 0.72 0.84 1.20 1.68 2.25
10 LS 0 82
11 UD 0.478
*
12 KK ROFF4 ROUTE OFFSITE WATERSHED 4 TO NORTHERN BOUNDARY OF SITE IN PROPOSED
* TRAPEZOIDAL CHANNEL
13 RD 2137 0.047 0.03 TRAP 5 0.33
*
14 KK OFF3 RUNOFF FROM OFFSITE AREA 3
15 BA 0.0800
16 LS 0 82
17 UD 0.33
*
18 KK DEV4 RUNOFF FROM PROPOSED WATERSHED 4
19 BA 0.0233
20 LS 0 82
21 UD 0.14
*
22 KK CP4 CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE
23 HC 3
*
24 KK RCP4_3 ROUTE CP4 TO CP3
25 RD 636 0.091 0.03 TRAP 10 0.33
*
26 KK OFF2 RUNOFF FROM OFFSITE AREA 2
27 BA 0.1732
28 LS 0 82
29 UD 0.54
*
30 KK DEV3
31 BA 0.0724
32 LS 0 83 5 11.1
33 UD 0.17
*

```

1

HEC-1 INPUT

PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

34 KK CP3 CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE
 35 HC 3
 *

36 KK RCP3_1 ROUTE CP3 TO CP1 (NORTHWEST CORNER OF SITE)
 37 RD 2500 0.024 0.03 TRAP 10 0.33
 *

38 KK OFF1 RUNOFF FROM OFFSITE AREA 1
 39 BA 1.7296
 40 LS 0 81.8
 41 UD 1.21
 *

42 KK DEV2 RUNOFF FROM PROPOSED WATERSHED 2
 43 BA 0.0957
 44 LS 0 77.1 11.5
 45 UD 0.25
 *

46 KK DEV1 RUNOFF FROM PROPOSED WATERSHED 1
 47 BA 0.0115
 48 LS 0 80.2 8.9
 49 UD 0.16
 *

50 KK CP1 CONCENTRATION POINT AT NORTHWEST CORNER OF SITE TO CROSS DESERT WAY
 * IN CULVERT
 51 HC 3
 *

52 KK OFF6 RUNOFF FROM OFFSITE AREA 6
 53 BA 0.1860
 54 LS 0 82
 55 UD 0.459
 *

56 KK ROFF6 ROUTE OFFSITE 6 IN PROPOSED CHANNEL THROUGH DEV10
 57 RD 1230 0.074 0.03 TRAP 10 0.33
 *

58 KK OFF5 RUNOFF FROM OFFSITE AREA 5
 59 BA 2.2212
 60 LS 0 80.7
 61 UD 1.32
 *

62 KK CPOFF CONCENTRATION POINT AT NORTHERN BOUNDARY OF DEV8
 63 HC 2
 *

HEC-1 INPUT

1

LINE ID.....1..... 2 34. 5. . .6.....7.8.....9.....10

64 KK ROFF56 ROUTE CPOFF TO CP8 (DOWNSTREAM BOUNDARY OF DEV8)
 65 RD 1394 0.075 0.03 TRAP 10 0.33
 *

66 KK DEV8 RUNOFF FROM PROPOSED AREA 8
 67 BA 0.0119
 68 LS 0 76.6 10.2
 69 UD 0.070
 *

70 KK DEV10 RUNOFF FROM PROPOSED AREA 10
 71 BA 0.0949
 72 LS 0 84.0 7.3
 73 UD 0.070
 *

74 KK CP8 CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV8
 75 HC 3
 *

76 KK RCP8_7 ROUTE CP8 TO CP7 (DOWNSTREAM BOUNDARY OF DEV7)
 77 RD 1991 0.079 0.03 TRAP 10 0.33
 *

78 KK DEV9 RUNOFF FROM PROPOSED AREA 9
 79 BA 0.0638
 80 LS 0 75.5 12.0
 81 UD 0.11
 *

82 KK DEV7 RUNOFF FROM PROPOSED AREA 7
 83 BA 0.0227
 84 LS 0 70.1 6.8
 85 UD 0.17
 *

86 KK CP7 COCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV7
 87 HC 3
 *

88 KK RCP7_6 ROUTE CP7 TO CP6 (WESTERN BOUNDARY OF SITE)
 89 RD 940 0.016 0.03 TRAP 10 0.33
 *

90 KK DEV6 RUNOFF FROM PROPOSED AREA 6
 91 BA 0.0053
 92 LS 0 72.0
 93 UD 0.11
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7... ..8 . 9 .. 10

94 KK CP6 CONCENTRATION POINT AT THE MID-WESTERN BOUNDARY OF SITE NEAR
 95 HC 2
 *

96 KK RCP6_5 ROUTE RUNOFF CONCENTRATING AT CP6 TO CP5 IN DAMONTE CHANNEL ALONG
 * DESERT WAY
 97 RD 270 0.003 0.03 TRAP 10 0.33
 *

98 KK DEV5 RUNOFF FROM PROPOSED AREA 5
 99 BA 0.0091
 100 LS 0 81.1 13.5
 101 UD 0.11
 *

102 KK CP5 CONCENTRATION POINT WITHIN DAMONTE CHANNEL ALONG DESERT WAY
 103 HC 2
 *

104 KK RCP5_1 ROUTE CP5 TO CP1 (NORTHWEST CORNER OF SITE)
 105 RD 1120 0.003 0.03 TRAP 10 0.33
 *

106 KK TOTCP1 TOTAL ADDITION OF FLOW AT NORTHWEST CORNER OF SITE
 107 HC 2
 *

108 KK OFF7 RUNOFF FROM OFFSITE AREA 7
 109 BA 0.0931
 110 LS 0 82
 111 UD 0.31
 *

112 KK ROFF7 ROUTE OFF7 TO THROUGH DEV7
 113 RD 1035 0.136 0.03 TRAP 5 0.33
 *

114 KK DEV12 RUNOFF FROM PROPOSED AREA 12
 115 BA 0.0346
 116 LS 0 84 2.5
 117 UD 0.04
 *

118 KK CP12 CONCENTRATION POINT AT THE DOWNSTREAM BOUNDARY OF DEV12
 119 HC 2
 *

120 KK RCP12 ROUTE CP12 TO CP11 (DOWNSTREAM BOUNDARY OF DEV11)
 121 RD 800 0.082 0.03 TRAP 5 0.33
 *

HEC-1 INPUT

LINE ID.....1.....2.....3..... .4.....5.....6.....78... ..9... . 10

122 KK DEV11 RUNOFF FROM PROPOSED AREA 11
 123 BA 0.0335
 124 LS 0 83.0 13.0
 125 UD 0.05
 *

126 KK CP11 CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV11
 127 HC 2
 *

128 KK OFF8 RUNOFF FROM OFFSITE AREA 8
 129 BA 0.0228
 130 LS 0 81.4
 131 UD 0.195
 *

132 KK DEV13 RUNOFF FROM PROPOSED AREA 13
 133 BA 0.0911
 134 LS 0 83 2 11.0
 135 UD 0.20
 *

136 KK CP13 COCENTRATION POINT ALONG THE DAMONTE RANCH HIGH SCHOOL
 137 HC 3
 *

```

96 . . . . . RCP6_5
. . . . .
98 . . . . . DEV5
. . . . .
102 . . . . . CP5
. . . . . V
. . . . . V
104 . . . . . RCP5_1
. . . . .
106 . . . . . TOTCP1.....
. . . . .
108 . . . . . OFF7
. . . . . V
. . . . . V
112 . . . . . ROFF7
. . . . .
114 . . . . . DEV12
. . . . .
118 . . . . . CP12.....
. . . . . V
. . . . . V
120 . . . . . RCP12
. . . . .
122 . . . . . DEV11
. . . . .
126 . . . . . CP11. . . . .
. . . . .
128 . . . . . OFF8
. . . . .
132 . . . . . DEV13
. . . . .
136 . . . . . CP13 .. . . .

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 25MAR05 TIME 15.10:03 *
*****

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```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

GOLDEN HILLS SUBDIVISION PROPOSED CONDITIONS 24-HOUR, 5-YEAR EVENT
GENERATED 3/2005 BY WOOD RODGERS INC

```

6 IO OUTPUT CONTROL VARIABLES
   IPRNT      3  PRINT CONTROL
   IPLOT      0  PLOT CONTROL
   QSCAL      0. HYDROGRAPH PLOT SCALE

IT  HYDROGRAPH TIME DATA
     NMIN      2  MINUTES IN COMPUTATION INTERVAL
     TDATE    17MAR78  STARTING DATE
     ITIME     0200  STARTING TIME
     NQ       1441  NUMBER OF HYDROGRAPH ORDINATES
     NDDATE    19MAR78  ENDING DATE
     NDTIME     0200  ENDING TIME
     ICENT     19  CENTURY MARK

     COMPUTATION INTERVAL .03 HOURS
     TOTAL TIME BASE 48.00 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA          SQUARE MILES
PRECIPITATION DEPTH    INCHES
LENGTH, ELEVATION      FEET
FLOW                   CUBIC FEET PER SECOND
STORAGE VOLUME         ACRE-FEET
SURFACE AREA           ACRES
TEMPERATURE            DEGREES FAHRENHEIT

```

7 KK * OFF4 * RUNOFF FROM OFFSITE AREA 4
 * * *

SUBBASIN RUNOFF DATA

8 BA SUBBASIN CHARACTERISTICS
 TAREA .21 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .18 34 .56 .72 .84 1.20 1.68 2.25 00 .00 .00 .00
 STORM AREA = 21

10 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNR 82.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

11 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .48 LAG

UNIT HYDROGRAPH

74 END-OF-PERIOD ORDINATES										
4.	11.	21.	33.	47.	64.	86.	110.	136.	157.	
175.	189.	197.	201.	202.	201.	195.	186.	177.	166.	
155.	141.	125.	110.	96.	86.	76.	68.	61.	55.	
50.	45.	40.	36.	32.	29.	26.	23.	21.	19.	
17.	15.	13.	12.	11.	10.	9.	8.	7.	6.	
6.	5.	4.	4.	4.	3.	3.	3.	2.	2.	
2.	2.	2.	1.	1.	1.	1.	1.	1.	1.	
0.	0.	0.	0.							

*** **

HYDROGRAPH AT STATION OFF4

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = .82

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
38	12.53	12.	5.	2.	2.
		(INCHES) .538	.818	.818	.818
		(AC-FT) 6.	9.	9.	9.

CUMULATIVE AREA = .21 SQ MI

.....

12 KK * ROFF4 * ROUTE OFFSITE WATERSHED 4 TO NORTHERN BOUNDARY OF SITE IN PROPOSED
 * * *

HYDROGRAPH ROUTING DATA

13 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 2137. CHANNEL LENGTH
 S .0470 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 5.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
			DT (MIN)	DX (FT)				
MAIN	4.09	1.42	2.00	534.25	38.28	756.00	.82	9.19

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	4.09	1.42	2.00		38.28	756.00	.82	
------	------	------	------	--	-------	--------	-----	--

*** **

HYDROGRAPH AT STATION ROFF4

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
38.	12 60	12.	5	2.	2
		(INCHES) .538	.818	.818	818
		(AC-FT) 6.	9.	9	9.

CUMULATIVE AREA = 21 SQ MI

14 KK OFF3 RUNOFF FROM OFFSITE AREA 3

SUBBASIN RUNOFF DATA

15 BA SUBBASIN CHARACTERISTICS
TAREA .08 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35	TP-40	TP-49									
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = .08

16 LS SCS LOSS RATE
STRTL .44 INITIAL ABSTRACTION
CRVNR 82.00 CURVE NUMBER
RTIMP 00 PERCENT IMPERVIOUS AREA

17 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .33 LAG

UNIT HYDROGRAPH
52 END-OF-PERIOD ORDINATES

3.	11.	20.	33.	49.	69.	87.	100.	108.	111.
111.	107.	100.	92.	82.	71.	59.	49.	42.	36.
30.	27.	23.	19.	16.	14.	12.	10.	9.	8.
6.	5.	5.	4.	3.	3.	3.	2.	2.	2.
1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.								

*** **

HYDROGRAPH AT STATION OFF3

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = 82

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
19.	12.37	5.	2.	1.	1.
		(INCHES) .539	.818	.818	.818
		(AC-FT) 2.	3.	3	3.

CUMULATIVE AREA = .08 SQ MI

18 KK DEV4 RUNOFF FROM PROPOSED WATERSHED 4

SUBBASIN RUNOFF DATA

19 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00

STORM AREA = 02

20 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNB 82.00 CURVE NUMBER
 RIIMP 00 PERCENT IMPERVIOUS AREA

21 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .14 LAG

UNIT HYDROGRAPH

23 END-OF-PERIOD ORDINATES
 8. 25 52. 69. 71. 63. 50. 33. 23. 17.
 12. 8. 6 4. 3. 2. 1. 1. 1. 1.
 0. 0 0

HYDROGRAPH AT STATION DEV4

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = .82

PEAK FLOW	TIME	6-HR	24-HR	72-HR	48.00-HR
(CFS)	(HR)	(CFS)			
8	12.17	1.	1.	0.	0.
		(INCHES) 54	.819	.819	.819
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 02 SQ MI

.....

22 KK *****
 * *
 * CP4 * CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE
 * *

23 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP4

PEAK FLOW	TIME	6-HR	24-HR	72-HR	48.00-HR
(CFS)	(HR)	(CFS)			
56.	12.50	18.	7.	3.	3.
		(INCHES) 538	.818	.818	.818
		(AC-FT) 9.	14.	14.	14.

CUMULATIVE AREA = 31 SQ MI

.....

24 KK *****
 * *
 * RCP4_3 * ROUTE CP4 TO CP3
 * *

HYDROGRAPH ROUTING DATA

25 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 636. CHANNEL LENGTH
 S .0910 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	3.98	1.50	.93	318.00	55.50	750.44	82	11.36

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.98	1.50	2.00		55.49	750.00	.82	
------	------	------	------	--	-------	--------	-----	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1354E+02 EXCESS= .0000E+00 OUTFLOW= .1354E+02 BASIN STORAGE= 2692E-03 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION RCP4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
55	12.50	18.	7.	3.	3.	
		(INCHES)	.538	.818	.818	.818
		(AC-FT)	9.	14.	14.	14.
CUMULATIVE AREA =		.31 SQ MI				

.....

26 KK *****
 OFF2 RUNOFF FROM OFFSITE AREA 2

SUBBASIN RUNOFF DATA

27 BA SUBBASIN CHARACTERISTICS
 TAREA .17 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35		TP-40						TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00
		STORM AREA = .17									

28 LS SCS LOSS RATE
 SRTTL .44 INITIAL ABSTRACTION
 CRUNBR 82.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

29 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .54 LAG

UNIT HYDROGRAPH
83 END-OF-PERIOD ORDINATES

3.	7	13.	20	28.	39.	51.	66.	82.	99.
113.	126.	136.	143.	149.	150.	150.	149.	145.	140.
134.	127.	120.	112.	103.	92.	82.	73.	65.	59.
54.	48.	44.	40.	37.	34.	30.	28.	25.	22.
20.	19.	17.	15.	14.	13.	11.	10.	9.	8.
8.	7.	6.	6.	5.	5.	4.	4.	4.	3.
3.	3.	2.	2.	2.	2.	2.	2.	1.	1.
1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.	0.							

*** *** *** *** ***

HYDROGRAPH AT STATION OFF2

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = .82

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
30.	12.60	10.	4.	2.	2.	
		(INCHES)	.537	.818	.818	.818

(AC-FT) 5. 8. 8 8
 CUMULATIVE AREA = .17 SQ MI

30 KK

 * DEV3 *
 * *

SUBBASIN RUNOFF DATA

31 BA SUBBASIN CHARACTERISTICS
 TAREA .07 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00
 STORM AREA = .07

32 LS SCS LOSS RATE
 STRTTL .40 INITIAL ABSTRACTION
 CRVNBR 83.50 CURVE NUMBER
 RTIMP 11.10 PERCENT IMPERVIOUS AREA

33 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .17 LAG

UNIT HYDROGRAPH
 27 END-OF-PERIOD ORDINATES
 16. 48. 101. 157 185. 185. 168. 141. 104. 75.
 56 43. 32. 24. 18. 13 10. 7. 6. 4.
 3. 2. 2. 1 1. 1. 0

*** **

HYDROGRAPH AT STATION DEV3

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.20, TOTAL EXCESS = 1.05

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 + 30. 12.20 (CFS) 5. 2. 1. 1.
 (INCHES) .648 1.047 1.048 1.048
 (AC-FT) 3. 4. 4 4.
 CUMULATIVE AREA = .07 SQ MI

34 KK

 * CP3 *
 * *

CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE

35 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP3

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 + 95. 12.47 (CFS) 33 13. 6. 6.
 (INCHES) .551 .847 .848 .848
 (AC-FT) 16. 25. 25. 25.
 CUMULATIVE AREA = .56 SQ MI

```

*****
*
36 KK * RCP3_1 * ROUTE CP3 TO CP1 (NORTHWEST CORNER OF SITE)
*
*****

```

HYDROGRAPH ROUTING DATA

```

37 RD MUSKINGUM-CUNGE CHANNEL ROUTING
      L 2500. CHANNEL LENGTH
      S .0240 SLOPE
      N .030 CHANNEL ROUGHNESS COEFFICIENT
      CA .00 CONTRIBUTING AREA
      SHAPE TRAP CHANNEL SHAPE
      WD 10 00 BOTTOM WIDTH OR DIAMETER
      Z .33 SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT					
		(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)	
MAIN	2.04	1.50	2.00	500.00	94.64	752.00	.85	8.69

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	2.04	1.50	2.00	500.00	94.64	752.00	.85	8.69
------	------	------	------	--------	-------	--------	-----	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2515E+02 EXCESS= .0000E+00 OUTFLOW= .2515E+02 BASIN STORAGE= .1725E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION RCP3_1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
95	12.53	33	13.	6.	6.	
		(INCHES)	.551	.847	.848	.848
		(AC-FT)	16.	25.	25.	25.

CUMULATIVE AREA = 56 SQ MI

```

*****
*
38 KK * OFF1 * RUNOFF FROM OFFSITE AREA 1
*
*****

```

SUBBASIN RUNOFF DATA

```

39 BA SUBBASIN CHARACTERISTICS
      TAREA 1.73 SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
      HYDRO-35 TP-40 TP-49
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
      .18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00

```

STORM AREA = 1.73

```

40 LS SCS LOSS RATE
      STRTL .44 INITIAL ABSTRACTION
      CRVNR 81.80 CURVE NUMBER
      RTIMP .00 PERCENT IMPERVIOUS AREA

```

```

41 UD SCS DIMENSIONLESS UNITGRAPH
      TLAG 1.21 LAG

```

UNIT HYDROGRAPH
183 END-OF-PERIOD ORDINATES

6.	11.	17.	25.	38.	50.	63.	79.	95.	112.
129.	151.	173.	195.	219.	249.	279.	308.	341.	376.

412.	447.	477.	506.	536.	563.	584.	604.	624.	640.
651.	662.	673.	676.	678.	680.	681.	679.	677.	675.
669.	657.	646.	635.	623.	610.	597.	583.	569.	554.
539.	522.	504.	485.	467.	445.	423.	401.	379.	361.
342.	324.	308.	295.	282.	269.	257.	246.	235.	224.
215.	206.	196.	188.	181.	174.	168.	161.	154.	147.
141.	135.	130.	124.	119.	113.	107.	102.	98.	94.
90.	87.	83.	79.	75.	72.	69.	66.	64.	61.
58.	55.	53.	50.	48.	45.	44.	42.	40.	38.
37.	35.	34.	32.	31.	30.	28.	27.	26.	25.
24.	23.	22.	21.	20.	19.	18.	18.	17.	16.
15.	15.	14.	13.	13.	12.	12.	11.	11.	10.
10.	9.	9.	9.	8.	8.	8.	7.	7.	7.
7.	6.	6.	6.	6.	6.	5.	5.	5.	5.
4.	4.	4.	4.	4.	3.	3.	3.	3.	3.
2.	2.	2.	2.	2.	1.	1.	1.	1.	1.
1.	0.	0.							

*** *** *** *** ***

HYDROGRAPH AT STATION OFF1

TOTAL RAINFALL = 2.24, TOTAL LOSS = 1.44, TOTAL EXCESS = .80

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
172.	13.37	96.	37.	19.	19
		(INCHES) .514	.805	.805	.805
		(AC-FT) 47.	74.	74	74.
CUMULATIVE AREA =		1.73 SQ MI			

.....

42 KK *****
 +
 + DEV2 + RUNOFF FROM PROPOSED WATERSHED 2
 +
 +

SUBBASIN RUNOFF DATA

43 BA SUBBASIN CHARACTERISTICS
 TAREA .10 SUBBASIN AREA

PRECIPITATION DATA

9 FH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00
STORM AREA =			.10								

44 LS SCS LOSS RATE-
 STRTL .59 INITIAL ABSTRACTION
 CRVNR 77.10 CURVE NUMBER
 RTIMP 11.50 PERCENT IMPERVIOUS AREA

45 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 25 LAG

UNIT HYDROGRAPH
40 END-OF-PERIOD ORDINATES

8.	25.	49.	82.	121.	152.	169.	173.	169.	155.
139.	118.	93.	74.	60.	49.	41.	33.	27.	22.
18.	15.	12.	10.	8.	6.	5.	4.	4.	3.
2.	2.	2.	1.	1.	1.	1.	0.	0.	0.

*** *** *** *** ***

HYDROGRAPH AT STATION DEV2

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.47, TOTAL EXCESS = .78

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
22.	12.30	5.	2.	1.	1.
		(INCHES) 474	.782	.783	.783
		(AC-FT) 2.	4.	4.	4.
CUMULATIVE AREA =		.10 SQ MI			

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*
*   46 KK   DEV1   RUNOFF FROM PROPOSED WATERSHED 1
*
*****

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SUBBASIN RUNOFF DATA

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47 BA   SUBBASIN CHARACTERISTICS
      TAREA   .01   SUBBASIN AREA

```

PRECIPITATION DATA

```

9 BH   DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
      HYDRO-35   TP-40   TP-49
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
      .18   .34   .56   .72   84   1.20  1.68  2.25   .00   .00   .00   .00

```

STORM AREA = .01

```

48 LS   SCS LOSS RATE
      STRTL   .49   INITIAL ABSTRACTION
      CRVNR   80.20  CURVE NUMBER
      RTIME   8.90  PERCENT IMPERVIOUS AREA

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49 UD   SCS DIMENSIONLESS UNITGRAPH
      TLAG   .16   LAG

```

UNIT HYDROGRAPH
26 END-OF-PERIOD ORDINATES

3.	9.	19.	28.	31.	31.	27	21.	15	11.
8.	6.	4.	3.	2.	2.	1	1.	1	0.
0.	0.	0.	0.	0.	0.				

HYDROGRAPH AT STATION DEV1

```

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.38, TOTAL EXCESS = .87

```

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
4.	12.20	1.	0	0.	0.
		(INCHES) 539	864	865	.865
		(AC-FT) 0.	1.	1.	1

CUMULATIVE AREA = 01 SQ MI

```

*****
*
*   50 KK   CP1   CONCENTRATION POINT AT NORTHWEST CORNER OF SITE TO CROSS DESERT WAY
*
*****

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51 HC   HYDROGRAPH COMBINATION
      ICOMP   3   NUMBER OF HYDROGRAPHS TO COMBINE

```

HYDROGRAPH AT STATION CP1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
177.	13.33	101	40.	20.	20.
		(INCHES) .509	.803	.804	804
		(AC-FT) 50.	79.	79.	79.

CUMULATIVE AREA = 1.84 SQ MI

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*

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52 KK * OFF6 * RUNOFF FROM OFFSITE AREA 6
 * * *

SUBBASIN RUNOFF DATA

53 BA SUBBASIN CHARACTERISTICS
 TAREA 19 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 18 .34 .56 .72 84 1 20 1.68 2.25 .00 .00 .00 .00

STORM AREA = .19

54 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNR 82.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

55 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .46 LAG

UNIT HYDROGRAPH
 71 END-OF-PERIOD ORDINATES

4.	11.	21.	33	47.	65.	86.	111.	134.	155.
170.	180.	187	189	188.	185.	177.	168	158	147.
134	119.	104	90.	80.	71.	63.	56.	51.	46.
41	37.	33.	29.	26.	23.	20.	18.	16.	14.
13.	12.	10	9.	8.	7.	7.	6.	5.	5.
4.	4.	3.	3.	3	2.	2.	2.	2.	2.
1.	1	1.	1.	1.	1.	1.	0.	0.	0.
0									

*** **

HYDROGRAPH AT STATION OFF6

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = .82

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
35	12.50	11	4.	2.	2.	
		(INCHES)	.538	.818	.818	.818
		(AC-FT)	5.	8.	8.	8.

CUMULATIVE AREA = .19 SQ MI

56 KK * ROFF6 * ROUTE OFFSITE 6 IN PROPOSED CHANNEL THROUGH DEV10
 * * *

HYDROGRAPH ROUTING DATA

57 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 1230. CHANNEL LENGTH
 S .0740 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA 00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT	DX				
MAIN	3.59	1.50	2.00	615.00	35.29	752.00	9.11	

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.59	1.50	2.00		35.29	752.00	.82
------	------	------	------	--	-------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .8117E+01 EXCESS= 0000E+00 OUTFLOW= .8117E+01 BASIN STORAGE= .6231E-03 PERCENT ERROR= .0

*** *** *** *** ***

HYDROGRAPH AT STATION ROFF6

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
35.	12.53	11.	4.	2.	2.
		(INCHES) 536	818	.818	.818
		(AC-FT) 5.	8	8.	8.

CUMULATIVE AREA = .19 SQ MI

58 KK OFF5 RUNOFF FROM OFFSITE AREA 'S

SUBBASIN RUNOFF DATA

59 BA SUBBASIN CHARACTERISTICS
TAREA 2.22 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	34	56	72	84	120	1.68	2.25	.00	.00	.00	.00

STORM AREA = 2.22

60 LS SCS LOSS RATE
STRTL .48 INITIAL ABSTRACTION
CRVNR 80 70 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

61 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 1.32 LAG

UNIT HYDROGRAPH
200 END-OF-PERIOD ORDINATES

6	12.	18	24.	38.	52.	66.	80.	98.	116.
134.	152.	176	200.	224.	248.	280.	312.	344	376.
413	451	489.	528.	560	592.	624.	656.	679.	701.
723.	745.	758.	770	782.	794.	797.	799.	801.	803.
801.	799.	797	795	784	772.	760.	748.	734.	720.
706.	692.	676	660.	644	628.	609.	589.	569.	549.
525.	501.	477.	453.	433.	413.	393.	373.	358.	344.
330	316.	303.	291	279.	267.	257.	247.	237.	227.
219	212.	204	197.	190.	182.	175.	168.	161.	155.
149.	143.	137	131.	125.	119.	115.	111.	107.	103.
99.	95	91.	87.	84.	81.	78.	75.	72.	69.
66	63.	60.	58.	56.	54.	51.	49.	47.	45.
43.	42.	40.	39.	37.	36.	34.	33.	31.	30.
29.	28.	27.	26	25	24.	23.	22.	21.	20.
20.	19.	18.	17.	16.	16.	15.	15.	14.	13.
13.	12.	12.	11.	11.	11.	10.	10.	9.	9.
9.	8.	8	8.	8.	7.	7.	7.	7.	7.
6.	6.	6.	6.	5	5.	5.	5.	4.	4.
4.	4.	4.	3.	3.	3.	3.	3.	2.	2.
2.	2	2.	1	1.	1.	1.	1.	0.	0.

*** *** *** *** ***

HYDROGRAPH AT STATION OFF5

TOTAL RAINFALL = 2.24. TOTAL LOSS = 1.49. TOTAL EXCESS = .75

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
192.	13.50	113.	45.	22.	22.
		(INCHES) .475	750	.750	.750
		(AC-FT) 56	89.	89.	89.

CUMULATIVE AREA = 2.22 SQ MI

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*****
*
* CPOFF          CONCENTRATION POINT AT NORTHERN BOUNDARY OF DEV8
*
*****

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63 HC          HYDROGRAPH COMBINATION
              ICOMP          2  NUMBER OF HYDROGRAPHS TO COMBINE

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              HYDROGRAPH AT STATION  CPOFF

PEAK FLOW    TIME                MAXIMUM AVERAGE FLOW
+ (CFS)      (HR)                6-HR      24-HR      72-HR      48.00-HR
+ 203.       13.47              (CFS)
              (INCHES)          124.     49.       24.       24.
              (AC-FT)          .477     .755     .755     .755
              (AC-FT)          61.     97.     97.     97.

              CUMULATIVE AREA = 2.41 SQ MI

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*****
*
* ROFF56        ROUTE CPOFF TO CP8 (DOWNSTREAM BOUNDARY OF DEV8)
*
*****

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HYDROGRAPH ROUTING DATA

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65 RD          MUSKINGUM-CUNGE CHANNEL ROUTING
              L 1394 CHANNEL LENGTH
              S .0750 SLOPE
              N .030 CHANNEL ROUGHNESS COEFFICIENT
              CA .00 CONTRIBUTING AREA
              SHAPE TRAP CHANNEL SHAPE
              WD 10.00 BOTTOM WIDTH OR DIAMETER
              Z .33 SIDE SLOPE

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```

              COMPUTED MUSKINGUM-CUNGE PARAMETERS
              COMPUTATION TIME STEP
              ELEMENT  ALPHA      M      DT      DX      PEAK    TIME TO  VOLUME  MAXIMUM
              (MIN)    (FT)    (CFS)  (MIN)  (IN)    (CFS)  (MIN)   (IN)    CELERITY
              (PPS)
              MAIN     3.61    1.50    1.42    697.00  202.96  808.86  .75     16.37

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INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

              MAIN     3.61    1.50    2.00    202.93  808.00  .75

```

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9691E+02 EXCESS= .0000E+00 OUTFLOW= .9691E+02 BASIN STORAGE= .6481E-03 PERCENT ERROR= .0

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              HYDROGRAPH AT STATION  ROFF56

PEAK FLOW    TIME                MAXIMUM AVERAGE FLOW
+ (CFS)      (HR)                6-HR      24-HR      72-HR      48.00-HR
+ 203.       13.47              (CFS)
              (INCHES)          124.     49.       24.       24.
              (AC-FT)          .477     .755     .755     .755
              (AC-FT)          61.     97.     97.     97.

              CUMULATIVE AREA = 2.41 SQ MI

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*****
*
* DEV8          RUNOFF FROM PROPOSED AREA 8
*
*****

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SUBBASIN RUNOFF DATA

67 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00
STORM AREA = .01

68 LS SCS LOSS RATE
STRTL .61 INITIAL ABSTRACTION
CRVNR 76.60 CURVE NUMBER
RTIMP 10.20 PERCENT IMPERVIOUS AREA

69 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .07 LAG

UNIT HYDROGRAPH
12 END-OF-PERIOD ORDINATES

19 60. 64. 42. 21. 12 6. 3. 2. 1.
1. 0.

*** **

HYDROGRAPH AT STATION DEV8

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.51, TOTAL EXCESS = .74

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
+ 4 12.10 (CFS) 1. 0. 0. 0.
(INCHES) .453 .743 .743 .743
(AC-FT) 0. 0. 0. 0.
CUMULATIVE AREA = .01 SQ MI

.....

70 KK DEV10 RUNOFF FROM PROPOSED AREA 10

SUBBASIN RUNOFF DATA

71 BA SUBBASIN CHARACTERISTICS
TAREA 09 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00
STORM AREA = .09

72 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP 7.30 PERCENT IMPERVIOUS AREA

73 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .07 LAG

UNIT HYDROGRAPH
12 END-OF-PERIOD ORDINATES

154. 475. 507 136. 169. 93 49. 26. 14. 7.
4. 2.

*** **

HYDROGRAPH AT STATION DEV10

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.23, TOTAL EXCESS = 1.02

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

	(HR)	(CFS)	6-HR	24-HR	72-HR	48.00-HR
+	54	12.10	7.	3.	1.	1.
		(INCHES)	.644	1.022	1.022	1.022
		(AC-FT)	3	5.	5.	5.

CUMULATIVE AREA = .09 SQ MI

74 KK *****
 * CP8 * CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV8
 * *****

75 HC HYDROGRAPH COMBINATION
 ICOMP 1 NUMBER OF HYDROGRAPHS TO COMBINE

		HYDROGRAPH AT STATION CP8				
PEAK FLOW	TIME	6-HR	24-HR	72-HR	48.00-HR	
+	208	13.47	129.	52.	26.	26.
		(CFS)	129.	52.	26.	26.
		(INCHES)	.477	.764	.765	.765
		(AC-FT)	64.	102.	103.	103.

CUMULATIVE AREA = 2.51 SQ MI

76 KK *****
 * RCP8_7 * ROUTE CP8 TO CP7 (DOWNSTREAM BOUNDARY OF DEV7)
 * *****

HYDROGRAPH ROUTING DATA

77 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	1991.	CHANNEL LENGTH
S	.0790	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	.33	SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
MAIN	3.70	1.50	1.98	995.50	207.74	810.39	.76	16.79

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.70	1.50	2.00		207.72	810.00	.76	
------	------	------	------	--	--------	--------	-----	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= 1026E+03 EXCESS= .0000E+00 OUTFLOW= .1026E+03 BASIN STORAGE= .1028E-02 PERCENT ERROR= .0

		HYDROGRAPH AT STATION RCP8_7				
PEAK FLOW	TIME	6-HR	24-HR	72-HR	48.00-HR	
+	208.	13.50	129.	52.	26.	26.
		(CFS)	129.	52.	26.	26.
		(INCHES)	.477	.764	.765	.765
		(AC-FT)	64	102.	103.	103.

CUMULATIVE AREA = 2 51 SQ MI

78 KK DEV9 RUNOFF FROM PROPOSED AREA 9

SUBBASIN RUNOFF DATA

79 BA SUBBASIN CHARACTERISTICS TAREA .06 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM HYDRO-35 TP-40 TP-49 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY .18 .34 56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00

STORM AREA = .06

80 LS SCS LOSS RATE STRTL .65 INITIAL ABSTRACTION CRVNBR 75.50 CURVE NUMBER RTIMP 12.00 PERCENT IMPERVIOUS AREA

81 UD SCS DIMENSIONLESS UNITGRAPH TLAG .11 LAG

UNIT HYDROGRAPH 18 END-OF-PERIOD ORDINATES

38. 127. 224 242 205. 143 89 59. 38. 25. 16. 11 7. 4. 3 2. 1. 1. 1.

*** *** *** *** ***

HYDROGRAPH AT STATION DEV9

TOTAL RAINFALL = 2 25, TOTAL LOSS = 1.51, TOTAL EXCESS = .74

PEAK FLOW TIME MAXIMUM AVERAGE FLOW 6-HR 24-HR 72-HR 48.00-HR (CFS) (HR) (CFS) 20. 12.13 3. 1 1. 1. (INCHES) .440 .735 .735 735 (AC-FT) 1. 2. 3. 3.

CUMULATIVE AREA = .06 SQ MI

82 KK DEV7 RUNOFF FROM PROPOSED AREA 7

SUBBASIN RUNOFF DATA

83 BA SUBBASIN CHARACTERISTICS TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM HYDRO-35 TP-40 TP-49 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY .18 .34 56 .72 .84 1.20 1.68 2.25 .00 .00 00 .00

STORM AREA = .02

84 LS SCS LOSS RATE STRTL .85 INITIAL ABSTRACTION CRVNBR 70 10 CURVE NUMBER RTIMP 6.80 PERCENT IMPERVIOUS AREA

85 UD SCS DIMENSIONLESS UNITGRAPH TLAG 17 LAG

UNIT HYDROGRAPH									
27 END-OF-PERIOD ORDINATES									
5.	15.	32.	49.	58.	58.	53.	44.	32	23.
17.	13.	10.	7.	6.	4	3.	2.	2	1
1.	1.	1.	0.	0.	0.	0.			

HYDROGRAPH AT STATION DEV7

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.78, TOTAL EXCESS = .47

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
3	12.20	1.	0.	0.	0.
		(INCHES) .278	.474	474	474
		(AC-FT) 0.	1.	1.	1.
CUMULATIVE AREA =		.02 SQ MI			

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86 KK CP7 COCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV7

87 HC HYDROGRAPH COMBINATION ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP7

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
210	13.50	132.	53.	27.	27
		(INCHES) .474	.760	762	.762
		(AC-FT) 66.	105.	106.	106.
CUMULATIVE AREA =		2.60 SQ MI			

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88 KK RCP7_6 ROUTE CP7 TO CP6 (WESTERN BOUNDARY OF SITE)

HYDROGRAPH ROUTING DATA

89 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	940.	CHANNEL LENGTH
S	.0160	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	.33	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
			DT (MIN)	DX (FT)				
MAIN	1.67	1.50	1.58	470.00	210.35	810.96	.76	9.89

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.67	1.50	2.00		210.31	812.00	.76	
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .1056E+03 EXCESS= .0000E+00 OUTFLOW= 1056E+03 BASIN STORAGE= .7199E-03 PERCENT ERROR= .0

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***          ***          ***          ***          ***
HYDROGRAPH AT STATION  RCP7_6
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)      6-HR      24-HR      72-HR      48 00-HR
+ 210.         13 53      (CFS)
                              132.         53.         27          27
                              (INCHES)      .474         .760         .762         .762
                              (AC-FT)        66.         105.         106          106.
CUMULATIVE AREA = 2.60 SQ MI

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*          *
90 KK      *   DEV6   *   RUNOFF FROM PROPOSED AREA 6
*          *
*****

```

```

SUBBASIN RUNOFF DATA
91 BA      SUBBASIN CHARACTERISTICS
          TAREA      .01  SUBBASIN AREA

```

```

PRECIPITATION DATA
9 PH      DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          HYDRO-35      TP-40      TP-49
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          .18   .34   .56   .72   84   1.20  1.68  2.25  .00   .00   .00   .00
          STORM AREA = .01

```

```

92 LS      SCS LOSS RATE
          STRTL      .78  INITIAL ABSTRACTION
          CRVNR      72 00 CURVE NUMBER
          RTIMP      .00  PERCENT IMPERVIOUS AREA

```

```

93 UD      SCS DIMENSIONLESS UNITGRAPH
          TLAG      .11  LAG

```

```

***
UNIT HYDROGRAPH
18 END-OF-PERIOD ORDINATES
          3.      11.      19.      20.      17.      12      7.      5.      3.      2.
          1.      1.      1.      0.      0      0      0      0.      0.

```

*** *** *** *** ***

```

HYDROGRAPH AT STATION  DEV6
TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.85, TOTAL EXCESS = .40
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)      6-HR      24-HR      72-HR      48.00-HR
+ 1.           12.17      (CFS)
                              0.         0.         0.         0
                              (INCHES)      267         .404         404         .404
                              (AC-FT)        0.         0.         0.         0.
CUMULATIVE AREA = .01 SQ MI

```

.....

```

*****
*          *
94 KK      *   CP6   *   CONCENTRATION POINT AT THE MID-WESTERN BOUNDARY OF SITE NEAR
*          *
*****

```

```

95 HC      HYDROGRAPH COMBINATION
          ICOMP      2  NUMBER OF HYDROGRAPHS TO COMBINE

```

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION  CP6
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
          6-HR      24-HR      72-HR      48.00-HR

```

```

+ (CFS) (HR)
+ 210. 13.53 (CFS) 133. 53. 27. 27.
(INCHES) .473 759 .761 .761
(AC-FT) 66. 106. 106. 106.
CUMULATIVE AREA = 2.61 SQ MI

```

```

*****
* *
96 KK * RCP6_5 * ROUTE RUNOFF CONCENTRATING AT CP6 TO CP5 IN DAMONTE CHANNEL ALONG
* *
*****

```

HYDROGRAPH ROUTING DATA

```

97 RD MUSKINGUM-CUNGE CHANNEL ROUTING
L 270 CHANNEL LENGTH
S .0030 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD 10.00 BOTTOM WIDTH OR DIAMETER
Z .33 SIDE SLOPE

```

```

***
COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP
ELEMENT ALPHA M DT DX PEAK TIME TO VOLUME MAXIMUM
(MIN) (FT) (CFS) (MIN) (IN) CELERITY
(PFS)
MAIN 72 1.50 .80 270.00 210.40 812.29 76 5.66

```

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

MAIN 72 1.50 2.00 210.39 812.00 .76

```

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1057E+03 EXCESS= 0000E+00 OUTFLOW= .1057E+03 BASIN STORAGE= 3743E-03 PERCENT ERROR= 0

*** **

HYDROGRAPH AT STATION RCP6_5

```

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) (CFS) 6-HR 24-HR 72-HR 48 00-HR
+ 210. 13.53 (CFS) 133. 53 27. 27
(INCHES) .473 759 .761 .761
(AC-FT) 66. 106 106. 106.
CUMULATIVE AREA = 2.61 SQ MI

```

```

*****
* *
98 KK * DEV5 * RUNOFF FROM PROPOSED AREA 5
* *
*****

```

SUBBASIN RUNOFF DATA

```

99 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

```

PRECIPITATION DATA

```

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 ..... TP-40 ..... TP-49 .....
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00

```

STORM AREA = .01

```

100 LS SCS LOSS RATE
STRTL 47 INITIAL ABSTRACTION
CRVNR 81.10 CURVE NUMBER
RTIMP 13.50 PERCENT IMPERVIOUS AREA

```


101 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .11 LAG

UNIT HYDROGRAPH
18 END-OF-PERIOD ORDINATES

5. 18. 32. 35. 29. 20. 13. 8. 5. 4.
2. 1. 1. 1. 0. 0 0. 0.

*** **

HYDROGRAPH AT STATION DEVS

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.28, TOTAL EXCESS = 97

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR
4.	12.13	1.	0.	0	0
		(INCHES)	.593	.972	.973
		(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 01 SQ MI

.....

102 KK *****
* *
* CPS = CONCENTRATION POINT WITHIN DAMONTE CHANNEL ALONG DESERT WAY
* *
* *****

103 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CPS

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR
211.	13 53	133.	53.	27.	27.
		(INCHES)	.473	.760	.762
		(AC-FT)	65.	106	106.

CUMULATIVE AREA = 2 61 SQ MI

.....

104 KK *****
* *
* RCP5_1 * ROUTE CPS TO CPI (NORTHWEST CORNER OF SITE)
* *
* *****

HYDROGRAPH ROUTING DATA

105 RD MUSKINGUM-CUNGE CHANNEL ROUTING
L 1120. CHANNEL LENGTH
S .0030 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD 10.00 BOTTOM WIDTH OR DIAMETER
Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
MAIN	.72	1 50	2.00	560.00	210.66	816.00	5.66	

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.72	1 50	2.00		210.66	816.00	.76
------	-----	------	------	--	--------	--------	-----

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1062E+03 EXCESS= 0000E+00 OUTFLOW= .1062E+03 BASIN STORAGE= .1483E-02 PERCENT ERROR= .0

```

***          ***          ***          ***          ***
          HYDROGRAPH AT STATION  RCP5_1
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 211.        13.60          (CFS)
          (INCHES)  133      53.      27.      27.
          (AC-FT)  .473    .760    .762    .762
          (AC-FT)  66.     106.    106     106.
          CUMULATIVE AREA = 2 61 SQ MI
  
```

.....

```

*****
*          *
* 106 KK  * TOTCP1 * TOTAL ADDITION OF FLOW AT NORTHWEST CORNER OF SITE
*          *
*****
  
```

```

107 HC          HYDROGRAPH COMBINATION
          ICOMP          2 NUMBER OF HYDROGRAPHS TO COMBINE
  
```

```

***          ***          ***          ***          ***
          HYDROGRAPH AT STATION  TOTCP1
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 385          13.47          (CFS)
          (INCHES)  234      93.     47.     47.
          (AC-FT)  .488    .778    .779    .779
          (AC-FT)  116.    185.    185.    185.
          CUMULATIVE AREA = 4 45 SQ MI
  
```

.....

```

*****
*          *
* 108 KK  * OFF7 * RUNOFF FROM OFFSITE AREA 7
*          *
*****
  
```

SUBBASIN RUNOFF DATA

```

109 BA          SUBBASIN CHARACTERISTICS
          TAREA          .09 SUBBASIN AREA
  
```

PRECIPITATION DATA

```

9 BH          DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          HYDRO-35          TP-40          TP-49
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          .18 .34 .56 .72 .84 1.20 1.68 2.25 .00 .00 .00 .00
          STORM AREA = .09
  
```

```

110 LS          SCS LOSS RATE
          STRTL          44 INITIAL ABSTRACTION
          CRVNR          82.00 CURVE NUMBER
          RTIMP          .00 PERCENT IMPERVIOUS AREA
  
```

```

111 UD          SCS DIMENSIONLESS UNITGRAPH
          TLAG          .31 LAG
  
```

```

***
          UNIT HYDROGRAPH
          48 END-OF-PERIOD ORDINATES
          4.      14      27.     44.     67.     94.     115.    129.    137.    137.
          134.    126.    116.    101.    89.     73.     60.     51.     43.     37.
          31.     27.     22.     19.     16.     14.     12.     10.     8.      7.
          6.      5.      4.      4.      3.      3.      2.      2.      2.      1.
          1.      1.      1.      1.      1.      0.      0.      0.      0.
  
```

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION   OFF7
TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.43, TOTAL EXCESS = .82
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 22.         12.37      (CFS)
                    (INCHES)  .540      .818      .818      .818
                    (AC-FT)   3.        4.        4.        4.
CUMULATIVE AREA = .09 SQ MI

```

.....

```

*****
112 KK  *  ROFF7  *  ROUTE OFF7 TO THROUGH DEV7
*****

```

```

HYDROGRAPH ROUTING DATA
113 RD  MUSKINGUM-CUNGE CHANNEL ROUTING
        L 1035. CHANNEL LENGTH
        S .1360 SLOPE
        N .030 CHANNEL ROUGHNESS COEFFICIENT
        CA .00 CONTRIBUTING AREA
        SHAPE TRAP CHANNEL SHAPE
        WD 5.00 BOTTOM WIDTH OR DIAMETER
        Z .33 SIDE SLOPE

```

```

***
COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP
ELEMENT  ALPHA  M  DT  DX  PEAK  TIME TO  VOLUME  MAXIMUM
          (MIN) (FT) (CFS)  PEAK  (IN)  CELERITY
          (MIN) (FPS)
MAIN     6.96  1.42  1.52  517.50  22.32  742.61  .82  11.38

```

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

MAIN     6.96  1.42  2.00  22.29  742.00  .82

```

CONTINUITY SUMMARY (AC-FT) - INFLOW= .4064E+01 EXCESS= .0000E+00 OUTFLOW= .4064E+01 BASIN STORAGE= .2376E-01 PERCENT ERROR= .0

```

***          ***          ***          ***          ***
HYDROGRAPH AT STATION   ROFF7
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 22.         12.37      (CFS)
                    (INCHES)  .540      .818      .818      .818
                    (AC-FT)   3.        4.        4.        4.
CUMULATIVE AREA = .09 SQ MI

```

.....

```

*****
114 KK  *  DEV12  *  RUNOFF FROM PROPOSED AREA 12
*****

```

```

SUBBASIN RUNOFF DATA
115 BA  SUBBASIN CHARACTERISTICS
        TAREA .03 SUBBASIN AREA

```

```

PRECIPITATION DATA
9 PH    DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
        HYDRO-35 ..... TP-40 ..... TP-49 .....
        5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY

```

18 .34 56 72 .84 1.20 1.68 2.25 00 00 00 .00

STORM AREA = 03

116 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP 2.50 PERCENT IMPERVIOUS AREA

117 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .04 LAG

UNIT HYDROGRAPH
8 END-OF-PERIOD ORDINATES

189. 280 123. 48. 18. 7. 3. 1.

*** *** *** *** ***

HYDROGRAPH AT STATION DEV12

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.29, TOTAL EXCESS = .96

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
21.	12 07	2.	1.	0.	0.
		(INCHES) .620	.959	.959	959
		(AC-FT) 1.	2.	2	2.

CUMULATIVE AREA = .03 SQ MI

.....

118 KK * CP12 * CONCENTRATION POINT AT THE DOWNSTREAM BOUNDARY OF DEV12
* * *
* * *

119 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CP12

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
27.	12.07	8.	3.	1.	1.
		(INCHES) .560	.856	.856	.856
		(AC-FT) 4.	6.	6	6

CUMULATIVE AREA = .13 SQ MI

.....

120 KK * RCP12 * ROUTE CP12 TO CP11 (DOWNSTREAM BOUNDARY OF DEV11)
* * *
* * *

HYDROGRAPH ROUTING DATA

121 RD MUSKINGUM-CUNGE CHANNEL ROUTING
L 800. CHANNEL LENGTH
S .0820 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD 5.00 BOTTOM WIDTH OR DIAMETER
Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)

MAIN 5.41 1.42 1 32 400.00 27.17 725 52 .86 10.13

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 5.41 1.42 2.00 27.00 726 00 86

CONTINUITY SUMMARY (AC-FT) - INFLOW= 5833E+01 EXCESS= 0000E+00 OUTFLOW= .5833E+01 BASIN STORAGE= .2417E-03 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION RCP12

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
27.	12.10	8.	3.	1.	1.
		(INCHES) 560	.856	.856	.856
		(AC-FT) 4.	6.	6.	6
CUMULATIVE AREA =		.13 SQ MI			

.....

```

*****
122 KK  DEV11  RUNOFF FROM PROPOSED AREA 11
*****

```

SUBBASIN RUNOFF DATA

123 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35				TP-40				TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
18	34	.56	.72	.84	1.20	1.68	2.25	00	00	.00	.00

STORM AREA = 03

124 LS SCS LOSS RATE
STRTL .41 INITIAL ABSTRACTION
CRVNR 83.00 CURVE NUMBER
RTIMP 13.00 PERCENT IMPERVIOUS AREA

125 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .05 LAG

UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

115. 244. 166. 68. 31. 13. 6 3. 1. 0.

*** **

HYDROGRAPH AT STATION DEV11

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.20, TOTAL EXCESS = 1.05

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
21.	12.07	2.	1.	0.	0.
		(INCHES) .644	1.050	1.050	1.050
		(AC-FT) 1.	2.	2.	2.
CUMULATIVE AREA =		.03 SQ MI			

.....

```

*****
126 KK  CP11  CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV11
*****

```

127 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CP11

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	48.00-HR
47	12 07	10.	4.	2.	2.	
		(INCHES)	.576	.895	.897	897
		(AC-FT)	5.	8.	8.	8.

CUMULATIVE AREA = .16 SQ MI

.....

 128 KK OFF8 RUNOFF FROM OFFSITE AREA 8

SUBBASIN RUNOFF DATA

129 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

9 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-15			TP-40						TP-49		
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = .02

130 LS SCS LOSS RATE
 STRTC .46 INITIAL ABSTRACTION
 CRVNR 81.40 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

131 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .19 LAG

UNIT HYDROGRAPH
 31 END-OF-PERIOD ORDINATES

4	11	22.	37.	48	52	51.	46.	40.	31.
23	17.	14.	11.	8.	6.	5.	4.	3.	2.
2.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0									

*** *** *** *** ***

HYDROGRAPH AT STATION OFF8

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.46, TOTAL EXCESS = .79

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	48.00-HR
7	12.23	1.	0.	0.	0.	
		(INCHES)	.521	.788	.788	.788
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = .02 SQ MI

.....

 132 KK DEVL3 RUNOFF FROM PROPOSED AREA 13

SUBBASIN RUNOFF DATA

133 BA SUBBASIN CHARACTERISTICS
 TAREA .09 SUBBASIN AREA

PRECIPITATION DATA

9 PH

DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM											
HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.18	.34	.56	.72	.84	1.20	1.68	2.25	.00	.00	.00	.00

STORM AREA = .09

134 LS

SCS LOSS RATE
 STRTL .40 INITIAL ABSTRACTION
 CRVNB 83 20 CURVE NUMBER
 RTIMP 11 00 PERCENT IMPERVIOUS AREA

135 UD

SCS DIMENSIONLESS UNITGRAPH
 TLAG 20 LAG

UNIT HYDROGRAPH

32 END-OF-PERIOD ORDINATES									
14.	40.	83.	139.	182.	202.	202.	185.	161.	129.
95.	74.	57.	45.	35.	27.	21.	17.	13.	10.
8.	6.	5.	4.	3.	2.	2.	1.	1.	1.
0.	0.								

HYDROGRAPH AT STATION DEV13

TOTAL RAINFALL = 2.25, TOTAL LOSS = 1.22, TOTAL EXCESS = 1.03

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
34.	12.23	6.	3.	1	1.
		(INCHES) 638	1.031	1.032	1.032
		(AC-FT) 3.	5.	5	5

CUMULATIVE AREA = .09 SQ MI

.....

136 KK

 * CP13 *
 * *

COCENTRATION POINT ALONG THE DAMONTE RANCH HIGH SCHOOL

137 HC

HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP13

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
73.	12 13	18.	7.	3.	3.
		(INCHES) .592	.931	.933	.933
		(AC-FT) 9	14.	14.	14.

CUMULATIVE AREA = 28 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+	ROUTED TO								
+	OFF4	38.	12.53	12.	5	2.	.21		
+	ROFF4	38	12.60	12.	5.	2.	.21		
+	HYDROGRAPH AT								
+	OFF3	19.	12 37	5.	2.	1.	.08		
+	HYDROGRAPH AT								
+	DEV4	8	12 17	1.	1	0.	.02		
	3 COMBINED AT								

+		CP4	56	12 50	18.	7.	3.	.31
	ROUTED TO							
+		RCP4_3	55.	12.50	18.	7	3	.31
	HYDROGRAPH AT							
+		OFF2	30.	12.60	10.	4.	2	.17
	HYDROGRAPH AT							
+		DEV3	30	12.20	5	2.	1.	.07
	3 COMBINED AT							
+		CP3	95.	12 47	33.	13.	6.	.56
	ROUTED TO							
+		RCP3_1	95	12.53	33.	13.	6.	.56
	HYDROGRAPH AT							
+		OFF1	172	13.37	96.	37.	19.	1.73
	HYDROGRAPH AT							
+		DEV2	22	12.30	5	2.	1.	.10
	HYDROGRAPH AT							
+		DEV1	4.	12 20	1.	0.	0.	.01
	3 COMBINED AT							
+		CP1	177.	13.33	101.	40.	20.	1.84
	HYDROGRAPH AT							
+		OFF6	35.	12.50	11	4.	2.	.19
	ROUTED TO							
+		ROFF6	35	12 53	11	4.	2.	.19
	HYDROGRAPH AT							
+		OFF5	192.	13.50	133.	45	22.	2.22
	2 COMBINED AT							
+		CPOFF	203.	13.47	124.	49.	24.	2.41
	ROUTED TO							
+		ROFF56	203	13 47	124.	49.	24.	2.41
	HYDROGRAPH AT							
+		DEV8	4.	12.10	1.	0.	0.	.01
	HYDROGRAPH AT							
+		DEV10	54.	12.10	7	3.	1.	.09
	3 COMBINED AT							
+		CP8	208	13 47	129.	52.	26.	2.51
	ROUTED TO							
+		RCP8_7	208.	13 50	129.	52.	26.	2.51
	HYDROGRAPH AT							
+		DEV9	20	12.13	3.	1.	1.	.06
	HYDROGRAPH AT							
+		DEV7	3	12.20	1	0.	0.	.02
	3 COMBINED AT							
+		CP7	210	13.50	132.	53.	27.	2.60
	ROUTED TO							
+		RCP7_6	210.	13.53	132	53.	27.	2.60
	HYDROGRAPH AT							
+		DEV6	1.	12.17	0.	0.	0.	.01
	2 COMBINED AT							
+		CP6	210.	13.53	133	53.	27.	2.61
	ROUTED TO							
+		RCP6_5	210	13.53	133.	53.	27.	2.61
	HYDROGRAPH AT							
+		DEV5	4	12.13	1.	0.	0.	.01
	2 COMBINED AT							
+		CP5	211	13.53	133.	53.	27.	2.61
	ROUTED TO							
+		RCPS_1	211.	13 60	133	53.	27.	2.61
	2 COMBINED AT							
+		TOTCP1	385.	13.47	234	93.	47.	4.45
	HYDROGRAPH AT							
+		OFF7	22.	12.37	5.	2.	1.	.09
	ROUTED TO							
+		ROFF7	22	12.37	5	2	1.	.09

+	HYDROGRAPH AT	DEV12	21.	12.07	2.	1.	0.	03
+	2 COMBINED AT	CP12	27.	12.07	8.	3.	1.	.13
+	ROUTED TO	RCP12	27.	12.10	8.	3.	1.	.13
+	HYDROGRAPH AT	DEV11	21	12.07	2	1	0.	.03
+	2 COMBINED AT	CP11	47	12.07	10.	4.	2.	.16
+	HYDROGRAPH AT	OFF8	7.	12.23	1.	0.	0.	02
+	HYDROGRAPH AT	DEV13	34.	12.23	6.	3.	1.	.09
+	3 COMBINED AT	CP13	73.	12.13	18	7	3.	.28

1

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)	
						PEAK (CFS)	TIME TO PEAK (MIN)		
ROFF4	MANE	2.00	38.28	756.00	82	2.00	38.28	756.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9033E+01 EXCESS= .0000E+00 OUTFLOW= .9033E+01 BASIN STORAGE= .7624E-03 PERCENT ERROR= .0									
RCP4_3	MANE	.93	55.50	750.44	82	2.00	55.49	750.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1354E+02 EXCESS= .0000E+00 OUTFLOW= .1354E+02 BASIN STORAGE= .2692E-03 PERCENT ERROR= 0									
RCP3_1	MANE	2.00	94.64	752.00	.85	2.00	94.64	752.00	.85
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2515E+02 EXCESS= .0000E+00 OUTFLOW= .2515E+02 BASIN STORAGE= .1725E-02 PERCENT ERROR= .0									
ROFF6	MANE	2.00	35.29	752.00	.82	2.00	35.29	752.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .8117E+01 EXCESS= .0000E+00 OUTFLOW= .8117E+01 BASIN STORAGE= .6231E-03 PERCENT ERROR= .0									
ROFF56	MANE	1.42	202.96	808.86	.75	2.00	202.93	808.00	.75
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9691E+02 EXCESS= .0000E+00 OUTFLOW= .9691E+02 BASIN STORAGE= .6481E-03 PERCENT ERROR= .0									
RCP8_7	MANE	1.98	207.74	810.39	.76	2.00	207.72	810.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1026E+03 EXCESS= .0000E+00 OUTFLOW= .1026E+03 BASIN STORAGE= .1028E-02 PERCENT ERROR= .0									
RCP7_6	MANE	1.58	210.35	810.96	.76	2.00	210.32	812.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1056E+03 EXCESS= .0000E+00 OUTFLOW= .1056E+03 BASIN STORAGE= .7199E-03 PERCENT ERROR= .0									
RCP6_5	MANE	.80	210.40	812.29	.76	2.00	210.39	812.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1057E+03 EXCESS= .0000E+00 OUTFLOW= .1057E+03 BASIN STORAGE= .3743E-03 PERCENT ERROR= 0									
RCP5_1	MANE	2.00	210.66	816.00	.76	2.00	210.66	816.00	.76
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1062E+03 EXCESS= .0000E+00 OUTFLOW= .1062E+03 BASIN STORAGE= 1483E-02 PERCENT ERROR= .0									
ROFF7	MANE	1.52	22.32	742.61	.82	2.00	22.29	742.00	.82
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4064E+01 EXCESS= .0000E+00 OUTFLOW= .4064E+01 BASIN STORAGE= .2376E-03 PERCENT ERROR= .0									
RCP12	MANE	1.32	27.17	725.52	.86	2.00	27.00	726.00	.86

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*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4 1 *
* RUN DATE 25MAR05 TIME 15:09:56 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

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X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID GOLDEN HILLS SUBDIVISION PROPOSED CONDITIONS 24-HOUR, 100-YEAR EVENT
2 ID GENERATED 3/2005 BY WOOD RODGERS INC
3 ID WITHOUT DETENTION IN SOUTHERN PORION OF SITE
4 ID =====
*
5 IT 2 17MAR78 0200 19MAR78 0200
6 IN 1
7 IO 3
*
8 KK OFF4 RUNOFF FROM OFFSITE AREA 4
9 BA 0 2070
10 PH 0.41 0.78 1.29 1.39 1.48 1.93 2.87 4.14
11 LS 0 82
12 UD 0.478
*
13 KK ROFF4 ROUTE OFFSITE WATERSHED 4 TO NORTHERN BOUNDARY OF SITE IN PROPOSED
* TRAPEZOIDAL CHANNEL
14 RD 2137 0 047 0.03 TRAP 5 0.33
*
15 KK OFF3 RUNOFF FROM OFFSITE AREA 3
16 BA 0.0800
17 LS 0 82
18 UD 0 13
*
19 KK DEV4 RUNOFF FROM PROPOSED WATERSHED 4
20 BA 0.0233
21 LS 0 82
22 UD 0.14
*
23 KK CP4 CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE
24 HC 3
*
25 KK RCP4_3 ROUTE CP4 TO CP3
26 RD 636 0.091 0.03 TRAP 10 0.33
*
27 KK OFF2 RUNOFF FROM OFFSITE AREA 2
28 BA 0.1732
29 LS 0 82
30 UD 0.54
*
31 KK DEV3
32 BA 0.0724
33 LS 0 83.5 11.1
34 UD 0 17
*

```

1

HEC-1 INPUT

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

35	KK	CP3	CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE								
36	HC	3									
	*										
37	KK	RCP1_1	ROUTE CP3 TO CP1 (NORTHWEST CORNER OF SITE)								
38	RD	2500	0.024	0.03	TRAP	10 0.33					
	*										
39	KK	OFF1	RUNOFF FROM OFFSITE AREA 1								
40	BA	1.7296									
41	LS	0	81.8								
42	UD	1.21									
	*										
43	KK	DEV2	RUNOFF FROM PROPOSED WATERSHED 2								
44	BA	0.0957									
45	LS	0	77.1	11.5							
46	UD	0.25									
	*										
47	KK	DEV1	RUNOFF FROM PROPOSED WATERSHED 1								
48	BA	0.0115									
49	LS	0	80.2	8.9							
50	UD	0.16									
	*										
51	KK	CP1	CONCENTRATION POINT AT NORTHWEST CORNER OF SITE TO CROSS DESERT WAY								
	*										
52	HC	3	IN CULVERT								
	*										
53	KK	OFF6	RUNOFF FROM OFFSITE AREA 6								
54	BA	0.1860									
55	LS	0	82								
56	UD	0.459									
	*										
57	KK	ROFF6	ROUTE OFFSITE 6 IN PROPOSED CHANNEL THROUGH DEV10								
58	RD	1230	0.074	0.03	TRAP	10 0.33					
	*										
59	KK	OFF5	RUNOFF FROM OFFSITE AREA 5								
60	BA	2.2212									
61	LS	0	80.7								
62	UD	1.32									
	*										
63	KK	CPOFF	CONCENTRATION POINT AT NORTHERN BOUNDARY OF DEV8								
64	HC	2									
	*										
			HEC-1 INPUT								
LINE	ID	1	2	3	4	5	6	7	8	9	10
65	KK	ROFF56	ROUTE CPOFF TO CP8 (DOWNSTREAM BOUNDARY OF DEV8)								
66	RD	1394	0.075	0.03	TRAP	10	0.33				
	*										
67	KK	DEV8	RUNOFF FROM PROPOSED AREA 8								
68	BA	0.0119									
69	LS	0	76.6	10.2							
70	UD	0.070									
	*										
71	KK	DEV10	RUNOFF FROM PROPOSED AREA 10								
72	BA	0.0949									
73	LS	0	84.0	7.3							
74	UD	0.070									
	*										
75	KK	CP8	CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV8								
76	HC	3									
	*										
77	KK	RCP8_7	ROUTE CP8 TO CP7 (DOWNSTREAM BOUNDARY OF DEV7)								
78	RD	1991	0.079	0.03	TRAP	10	0.33				
	*										
79	KK	DEV9	RUNOFF FROM PROPOSED AREA 9								
80	BA	0.0638									
81	LS	0	75.5	12.0							
82	UD	0.11									
	*										
83	KK	DEV7	RUNOFF FROM PROPOSED AREA 7								
84	BA	0.0227									
85	LS	0	70.1	6.8							
86	UD	0.17									
	*										
87	KK	CP7	CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV7								
88	HC	3									

89 KK RCP7_6 ROUTE CP7 TO CP6 (WESTERN BOUNDARY OF SITE)
 90 RD 940 0 016 0 03 TRAP 10 0.33

91 KK DEV6 RUNOFF FROM PROPOSED AREA 6
 92 BA 0.0053
 93 LS 0 72.0
 94 UD 0.11

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

95 KK CP6 CONCENTRATION POINT AT THE MID-WESTERN BOUNDARY OF SITE NEAR
 96 HC 2

97 KK RCP6_5 ROUTE RUNOFF CONCENTRATING AT CP6 TO CP5 IN DAMONTE CHANNEL ALONG
 * DESERT WAY
 98 RD 270 0 003 0.03 TRAP 10 0.33

99 KK DEV5 RUNOFF FROM PROPOSED AREA 5
 100 BA 0.0091
 101 LS 0 81.1 13.5
 102 UD 0.11

103 KK CP5 CONCENTRATION POINT WITHIN DAMONTE CHANNEL ALONG DESERT WAY
 104 HC 2

105 KK RCP5_1 ROUTE CP5 TO CP1 (NORTHWEST CORNER OF SITE)
 106 RD 1120 0.003 0 03 TRAP 10 0.33

107 KK TOTCP1 TOTAL ADDITION OF FLOW AT NORTHWEST CORNER OF SITE
 108 HC 2

109 KK OFF7 RUNOFF FROM OFFSITE AREA 7
 110 BA 0.0931
 111 LS 0 82
 112 UD 0.31

113 KK ROFF7 ROUTE OFF7 TO THROUGH DEV7
 114 RD 1035 0.136 0.03 TRAP 5 0.33

115 KK DEV12 RUNOFF FROM PROPOSED AREA 12
 116 BA 0.0346
 117 LS 0 84 2.5
 118 UD 0.04

119 KK CP12 CONCENTRATION POINT AT THE DOWNSTREAM BOUNDARY OF DEV12
 120 HC 2

121 KK RCP12 ROUTE CP12 TO CP11 (DOWNSTREAM BOUNDARY OF DEV11)
 122 RD 800 0.082 0 03 TRAP 5 0.33

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

123 KK DEV11 RUNOFF FROM PROPOSED AREA 11
 124 BA 0.0335
 125 LS 0 83.0 13.0
 126 UD 0.05

127 KK CP11 CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV11
 128 HC 2

* KK DETEN DETENTION TO MITIGATE INCREASE IN FLOW IN SOUTH PORTION OF PROPERTY
 * RS 1 STOR -1
 * SA 1.26 1.35 1.43 1.52 1.60 1.69 1.77 1.86 1.90 1.
 * SA 2 00 2.07 2.15 2.22 2.29 2.36 2.43
 * SE4588.5 4589 4589.5 4590 4590.5 4591 4591.5 4592 4592.5 45
 * SE 4594 4595 4596 4597 4598 4599 4600
 * SQ 0 1.3 1.4 1.5 1.6 1.7 1.8 1.9 1.4 7
 * SQ 24.2 48.2 77.2 107.7 131.6 151.2 168.4

129 KK OFF8 RUNOFF FROM OFFSITE AREA 8
 130 BA 0.0228
 131 LS 0 81.4
 132 UD 0.195

89 V
 RCP7_6
 91 DEV6
 95 CP6.....
 V
 97 RCP6_5
 V
 99 DEV5
 103 CP5.....
 V
 105 RCP5_1
 V
 107 TOTCP1.....
 109 OFF7
 V
 113 ROFF7
 V
 115 DEV12
 119 CP12.....
 V
 121 RCP12
 V
 123 DEV11
 127 CP11.....
 129 OFF8
 133 DEV13
 137 CP13.....

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998                     *
*   VERSION 4.1                   *
* RUN DATE 25MAR05 TIME 15:09:56 *
*****
  
```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET            *
* DAVIS, CALIFORNIA 95616     *
* (916) 756-1104              *
*****
  
```

GOLDEN HILLS SUBDIVISION PROPOSED CONDITIONS 24-HOUR, 100-YEAR EVENT
 GENERATED 3/2005 BY WOOD RODGERS INC
 WITHOUT DETENTION IN SOUTHERN PORION OF SITE

7 10

OUTPUT CONTROL VARIABLES

```

IPRNT      3  PRINT CONTROL
IPLOT      0  PLOT CONTROL
QSCAL      0.  HYDROGRAPH PLOT SCALE
  
```

IT

HYDROGRAPH TIME DATA

```

NMIN       2  MINUTES IN COMPUTATION INTERVAL
IDATE      17MAR78  STARTING DATE
ITIME      0200  STARTING TIME
NQ         1441  NUMBER OF HYDROGRAPH ORDINATES
NDDATE     19MAR78  ENDING DATE
NDTIME     0200  ENDING TIME
ICENT      19  CENTURY MARK
  
```

```

COMPUTATION INTERVAL  .03 HOURS
TOTAL TIME BASE       48.00 HOURS
  
```

ENGLISH UNITS

```

DRAINAGE AREA           SQUARE MILES
PRECIPITATION DEPTH    INCHES
LENGTH, ELEVATION      FEET
  
```

FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE- FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

8 KK *****
 * OFF4 * RUNOFF FROM OFFSITE AREA 4
 * *

SUBBASIN RUNOFF DATA

9 BA SUBBASIN CHARACTERISTICS
 TAREA .21 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .41 78 1.29 1.39 1.48 1.93 2.87 4.14 .00 .00 .00 .00
 STORM AREA = .21

11 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNR 82.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

12 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .48 LAG

UNIT HYDROGRAPH
 74 END-OF-PERIOD ORDINATES

4.	11.	21	33	47.	64.	86.	110.	136.	157.
175.	189.	197.	201	202.	201.	195	186	177	166.
155.	141.	125.	110.	96	86.	76.	68.	61	55.
50	45.	40.	36	32.	29.	26	23.	21.	19.
17.	15.	13	12	11	10.	9.	8	7.	6.
6.	5.	4.	4.	4.	3.	3.	3.	2.	2.
2.	2	2.	1.	1.	1.	1	1.	1.	1.
0.	0.	0	0.						

HYDROGRAPH AT STATION OFF4

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.82, TOTAL EXCESS = 2.32
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 48.00-HR
 + 139. 12.53 (CFS) 31. 13. 6. 6
 (INCHES) 1.403 2.322 2.322 2.322
 (AC-FT) 15 26 26. 26.
 CUMULATIVE AREA = .21 SQ MI

13 KK *****
 * ROFF4 * ROUTE OFFSITE WATERSHED 4 TO NORTHERN BOUNDARY OF SITE IN PROPOSED
 * *

HYDROGRAPH ROUTING DATA

14 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 1137. CHANNEL LENGTH
 S .0470 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 5.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM Celerity
---------	-------	---	----	----	------	--------------	--------	------------------

			(MIN)	(PT)	(CFS)	(MIN)	(IN)	(FPS)
MAIN	4.09	1.42	2.00	712.33	139.34	754.00	2.32	13.47

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	4.09	1.42	2.00	139.34	754.00	2.32
------	------	------	------	--------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= 2564E+02 EXCESS= .0000E+00 OUTFLOW= .2564E+02 BASIN STORAGE= 7478E-03 PERCENT ERROR= 0

*** **

HYDROGRAPH AT STATION ROFF4

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	48.00-HR
+	139.	12.57				
		(CFS)	31.	13.	6.	6.
		(INCHES)	1.403	2.322	2.322	2.322
		(AC-FT)	15.	26.	26.	26.
		CUMULATIVE AREA =	.21 SQ MI			

.....

15 KK OFF3 RUNOFF FROM OFFSITE AREA 3

SUBBASIN RUNOFF DATA

16 BA SUBBASIN CHARACTERISTICS
TAREA .08 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

	HYDRO-35				TP-40					TP-49		
	5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
	41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .08

17 LS SCS LOSS RATE
STRTL .44 INITIAL ABSTRACTION
CRVNR 82.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

18 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .33 LAG

UNIT HYDROGRAPH
52 END-OF-PERIOD ORDINATES

3.	11.	20.	33.	49.	69.	87.	100.	108.	111.
111.	107.	100.	92.	82.	71.	59.	49.	42.	36.
30.	27.	23.	19.	16.	14.	12.	10.	9.	8.
6.	5.	5.	4.	3.	3.	3.	2.	2.	2.
1.	1.	1.	1.	1.	1.	1.	0.	0.	0.
0.	0.								

*** **

HYDROGRAPH AT STATION OFF3

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.82, TOTAL EXCESS = 2.32

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	48.00-HR
+	68.	12.37				
		(CFS)	12.	5.	2.	2.
		(INCHES)	1.411	2.323	2.323	2.323
		(AC-FT)	6.	10.	10.	10.
		CUMULATIVE AREA =	.08 SQ MI			

.....

```

*****
*                               *
19 KK  *   DEV4   *   RUNOFF FROM PROPOSED WATERSHED 4
*                               *
*****

```

SUBBASIN RUNOFF DATA

```

20 BA   SUBBASIN CHARACTERISTICS
      TAREA    .02  SUBBASIN AREA

```

PRECIPITATION DATA

```

10 PH   DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
      HYDRO-35  TP-40  TP-49
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
      .41   .78   1.29   1.39  1.48  1.93  2.87  4.14   .00   .00   .00   .00
      STORM AREA = .02

```

```

21 LS   SCS LOSS RATE
      STRTL    .44  INITIAL ABSTRACTION
      CRVNR    82.00 CURVE NUMBER
      RTIMP    .00  PERCENT IMPERVIOUS AREA

```

```

22 UD   SCS DIMENSIONLESS UNITGRAPH
      TLAG    .14  LAG

```

UNIT HYDROGRAPH

```

23 END-OF-PERIOD ORDINATES
      8.    25.    52.    69    71    63    50.    33.    23.    17.
      12.    8.    6.    4     3.    2     1.    1.    1.    1.
      0.    0.    0.

```

HYDROGRAPH AT STATION DEV4

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.82, TOTAL EXCESS = 2.32

```

PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+   31.        12.17      (CFS)
      (INCHES)   1.419   2.323   2.323   2.323
      (AC-FT)    2.     3.     3.     3.
      CUMULATIVE AREA = .02 SQ MI

```

```

*****
*                               *
23 KK  *   CP4   *   CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE
*                               *
*****

```

```

24 HC   HYDROGRAPH COMBINATION
      ICOMP    3  NUMBER OF HYDROGRAPHS TO COMBINE

```

HYDROGRAPH AT STATION CP4

```

PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+  205.        12.47      (CFS)
      (INCHES)   1.402   2.322   2.322   2.322
      (AC-FT)    23.    38.    38.    38.
      CUMULATIVE AREA = .31 SQ MI

```

```

*****
*                               *
25 KK  *   RCP4_3 *   ROUTE CP4 TO CP3
*                               *
*****

```


HYDROGRAPH ROUTING DATA

26 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 536. CHANNEL LENGTH
 S .0910 SLOPE
 N 030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 33 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	3.98	1 50	61	118.00	204.39	748.94	2.32	17.51

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.98	1.50	2 00		204.06	748.00	2.32	
------	------	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3843E+02 EXCESS= .0000E+00 OUTFLOW= .3843E+02 BASIN STORAGE= .2863E-03 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION RCP4_3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
204.	12.47	47.	19	10	10.	
		(INCHES)	1.402	2.322	2.322	2.322
		(AC-FT)	23.	38.	38.	38.
CUMULATIVE AREA		31 50 MI				

.....

27 KK *****
 * OFF2 * RUNOFF FROM OFFSITE AREA 2
 * *

SUBBASIN RUNOFF DATA

28 BA SUBBASIN CHARACTERISTICS
 TAREA .17 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35				TP-40				TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .17

29 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNB 82.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

30 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .54 LAG

 UNIT HYDROGRAPH
 81 END-OF-PERIOD ORDINATES

3.	7.	13.	20	28.	39.	51.	66.	82.	99.
113.	126.	136.	143.	149	150.	150.	149.	145.	140.
134.	127.	120.	112	103.	92.	82.	73.	65.	59.
54.	48.	44	40	37.	34.	30	28.	25.	22.
20.	19.	17.	15.	14	13.	11.	10.	9.	8.
8.	7.	6.	6	5.	5.	4.	4.	4.	3.
3.	3.	2.	2	2.	2.	2.	2.	1.	1.
1.	1.	1.	1.	1	1.	1.	0.	0.	0.
0.	0.	0.							

*** **

HYDROGRAPH AT STATION OFF2

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.82, TOTAL EXCESS = 2.32

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
108.	12.60	26.	11.	5.	5
		(INCHES) 1.400	2.322	2.322	2.322
		(AC-FT) 13.	21.	21.	21.

CUMULATIVE AREA = .17 SQ MI

31 KK

 * DEV3 *
 * *

SUBBASIN RUNOFF DATA

32 BA SUBBASIN CHARACTERISTICS
 TAREA .07 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .07

33 LS SCS LOSS RATE
 STRTL .40 INITIAL ABSTRACTION
 CRVNR 83.50 CURVE NUMBER
 RTIMP 11.10 PERCENT IMPERVIOUS AREA

34 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .17 LAG

UNIT HYDROGRAPH
 27 END-OF-PERIOD ORDINATES

16.	48.	101.	157.	185.	186.	168.	141.	104.	75.
56.	43.	32.	24.	18.	13.	10.	7.	6.	4.
3.	2.	2.	1.	1.	1.	0.			

HYDROGRAPH AT STATION DEV3

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.50, TOTAL EXCESS = 2.64

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
97.	12.20	12.	5.	3.	3.
		(INCHES) 1.541	2.636	2.638	2.638
		(AC-FT) 6.	10.	10.	10.

CUMULATIVE AREA = .07 SQ MI

35 KK

 * CP3 * CONCENTRATION POINT ALONG THE NORTHERN BOUNDARY OF THE SITE
 * *

36 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP3

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

			6-HR	24-HR	72-HR	48.00-HR
+	(CFS)	(HR)				
+	342.	12.47	85	35.	18.	18.
		(CFS)				
		(INCHES)	1.416	2.361	2.363	2.363
		(AC-FT)	42.	70.	70.	70.
		CUMULATIVE AREA =	.56 SQ MI			

```

*****
37 KK * RCP3_1 * ROUTE CP3 TO CP1 (NORTHWEST CORNER OF SITE)
*****

```

HYDROGRAPH ROUTING DATA

```

38 RD MUSKINGUM-CUNGE CHANNEL ROUTING
      L 2500. CHANNEL LENGTH
      S .0240 SLOPE
      N .030 CHANNEL ROUGHNESS COEFFICIENT
      CA .00 CONTRIBUTING AREA
      SHAPE TRAP CHANNEL SHAPE
      WD 10 00 BOTTOM WIDTH OR DIAMETER
      Z 33 SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT				
		(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
MAIN	2.04	1.50	2.00	833 33	342.17	750.00	2.36

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	2.04	1.50	2.00	342.17	750.00	2.36
------	------	------	------	--------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7007E+02 EXCESS= .0000E+00 OUTFLOW= .7007E+02 BASIN STORAGE= .1794E-02 PERCENT ERROR= .0

HYDROGRAPH AT STATION RCP3_1

			6-HR	24-HR	72-HR	48 00-HR
+	PEAK FLOW	TIME				
+	(CFS)	(HR)				
		(CFS)	85	35.	18.	18.
		(INCHES)	1.416	2.361	2.363	2.363
		(AC-FT)	42.	70.	70.	70.
		CUMULATIVE AREA =	56 SQ MI			

```

*****
39 KK * OFF1 * RUNOFF FROM OFFSITE AREA 1
*****

```

SUBBASIN RUNOFF DATA

```

40 BA SUBBASIN CHARACTERISTICS
      TAREA 1 73 SUBBASIN AREA

```

PRECIPITATION DATA

10 PH	DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM											
	HYDRO-15	TP-40				TP-49						
	5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
	.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = 1 73

```

41 LS SCS LOSS RATE
      STRTL .44 INITIAL ABSTRACTION
      CRVNR 81.80 CURVE NUMBER

```

RTIMP .00 PERCENT IMPERVIOUS AREA
 42 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.21 LAG

UNIT HYDROGRAPH
 183 END-OF-PERIOD ORDINATES

6.	11	17	25	38.	50.	63.	79	95.	112.
129.	151.	173.	195	219.	249	279.	308.	341.	376.
412.	447.	477	506.	536.	563.	584.	604.	624	640.
651.	662.	673.	676.	678.	680.	681	679.	677.	675.
669.	657.	646	635	623	610.	597.	583	569.	554.
539.	522.	504	485	467.	445.	423.	401.	379.	361.
342.	324.	308.	295	282	269.	257.	246.	235.	224.
215.	206.	196	188	181.	174.	168.	161.	154.	147.
141.	135.	130.	124	119.	113.	107.	102.	98.	94.
90.	87.	83.	79.	75.	72.	69.	66.	64.	61.
58.	55.	53.	50	48.	46.	44.	42	40.	38.
37.	35.	34.	32.	31.	30.	28.	27.	26.	25.
24.	23.	22.	21.	20.	19.	18	18	17.	16.
15.	15.	14.	13	13.	12.	12.	11.	11.	10.
10.	9.	9	9.	8.	8.	8.	7.	7.	7.
7.	6.	6.	6.	6.	6.	5	5.	5.	5.
4.	4	4	4	4.	3.	3.	3.	3.	3.
2.	2.	2.	2	2	1.	1.	1.	1.	1.
1.	0.	0							

HYDROGRAPH AT STATION OFF1

TOTAL RAINFALL = 4.13, TOTAL LOSS = 1.83, TOTAL EXCESS = 2.30

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
579.	13.27	250	107	53.	53.	
		(INCHES)	1.344	2.298	2.298	2.298
		(AC-FT)	124	212	212.	212.

CUMULATIVE AREA = 1.73 SQ MI

.....

43 XK DEV2 RUNOFF FROM PROPOSED WATERSHED 2

SUBBASIN RUNOFF DATA

44 BA SUBBASIN CHARACTERISTICS
 TAREA .10 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35		TP-40				TP-49					
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = 10

45 LS SCS LOSS RATE
 STRTL .59 INITIAL ABSTRACTION
 CRVNR 77.10 CURVE NUMBER
 RTIMP 11.50 PERCENT IMPERVIOUS AREA

46 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .25 LAG

UNIT HYDROGRAPH
 40 END-OF-PERIOD ORDINATES

8.	25.	49	82.	121.	152.	169.	173.	169.	155.
139.	118.	93.	74.	60.	49.	41.	33.	27.	22.
18.	15.	12.	10.	8.	6.	5.	4.	4.	3.
2.	2.	2	1.	1.	1.	1.	0.	0	0.

HYDROGRAPH AT STATION DEV2

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.96, TOTAL EXCESS = 2.18

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

			6-HR	24-HR	72-HR	48 00-HR	
+	(CFS)	(HR)					
+	86.	12.30	(CFS)	13.	6	3.	3
			(INCHES)	1.291	2.180	2.183	2.183
			(AC-FT)	7.	11	11.	11.

CUMULATIVE AREA = .10 SQ MI

.....

```

*****
*          *
* 47 KK   *   DEVI   *   RUNOFF FROM PROPOSED WATERSHED 1
*          *
*****

```

SUBBASIN RUNOFF DATA

48 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

	HYDRO-35				TP-40					TP-49		
	5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
	41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .01

49 LS SCS LOSS RATE

STRFL	.49	INITIAL ABSTRACTION
CRVNR	80.20	CURVE NUMBER
RTIMP	8.90	PERCENT IMPERVIOUS AREA

50 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	.16	LAG
------	-----	-----

UNIT HYDROGRAPH

26 END-OF-PERIOD ORDINATES

3.	9.	19.	28.	31.	31.	27.	21.	15	11.
8.	6.	4.	3.	2	2.	1.	1.	1	0.
0	0.	0.	0.	0.	0.				

HYDROGRAPH AT STATION DEVI

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.79, TOTAL EXCESS = 2.35

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	48.00-HR	
+	(CFS)	(HR)					
+	14	12.20	(CFS)	2.	1	0	0.
			(INCHES)	1.398	2.347	2.349	2.349
			(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = .01 SQ MI

.....

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*****
*          *
* 51 KK   *   CP1   *   CONCENTRATION POINT AT NORTHWEST CORNER OF SITE TO CROSS DESERT WAY
*          *
*****

```

52 HC HYDROGRAPH COMBINATION

YCMP	3	NUMBER OF HYDROGRAPHS TO COMBINE
------	---	----------------------------------

HYDROGRAPH AT STATION CP1

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	48.00-HR	
+	(CFS)	(HR)					
+	584.	13.27	(CFS)	264.	113.	57.	57.
			(INCHES)	1.334	2.289	2.292	2.292
			(AC-FT)	131.	224.	225.	225.

MAIN 3 59 1.50 1.46 615.00 128.39 750.93 2 32 14 00

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 3 59 1.50 2.00 128.25 752.00 2 32

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2304E+02 EXCESS= .0000E+00 OUTFLOW= .2304E+02 BASIN STORAGE= .6351E-03 PERCENT ERROR= 0

*** HYDROGRAPH AT STATION ROFF6 ***

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
128	12.53	28	12	6	6
		(INCHES) 1.404	2.322	2.322	2.322
		(AC-FT) 14.	23.	23.	23.

CUMULATIVE AREA = .19 SQ MI

 59 KK OFF5 RUNOFF FROM OFFSITE AREA 5

SUBBASIN RUNOFF DATA

60 BA SUBBASIN CHARACTERISTICS
 TAREA 2.22 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35		TP-40						TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = 2.22

61 LS SCS LOSS RATE
 STRTL .48 INITIAL ABSTRACTION
 CRVNBR 80 70 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

62 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 1.32 LAG

UNIT HYDROGRAPH
 200 END-OF-PERIOD ORDINATES

6	12.	18.	24.	38.	52.	66.	80.	98	116.
134.	152.	176.	200.	224.	248.	280.	312	344.	376
413.	451.	489.	528.	560.	592.	624.	656.	679.	701.
723.	745.	758.	770.	782.	794.	797.	799.	801.	803.
801.	799.	797.	795.	784.	772.	760.	748.	734.	720.
706.	692.	676.	660.	644.	628.	609.	589.	569	549.
525.	501.	477.	453.	433.	413.	393.	373.	358.	344.
330.	316.	303.	291.	279.	267.	257.	247.	237.	227.
219.	212.	204.	197.	190.	182.	175.	168.	161.	155.
149.	143.	137.	131.	125.	119.	115.	111.	107.	103.
99.	95.	91.	87.	84.	81.	78.	75.	72.	69.
66.	63.	60.	58.	56.	54.	51.	49.	47.	45.
43.	42.	40.	39.	37.	36.	34.	33.	31.	30.
29.	28.	27.	26.	25.	24.	23.	22.	21.	20.
20.	19.	18.	17.	16.	16.	15.	15.	14.	13.
13.	12.	12.	11.	11.	11.	10.	10.	9.	9.
9.	8.	8.	8.	8.	7.	7.	7.	7.	7.
6.	6.	6.	6.	5.	5.	5.	5.	4.	4.
4.	4.	4.	3.	3.	3.	3.	3.	2.	2.
2.	2.	2.	1.	1.	1.	1.	1.	0.	0.

HYDROGRAPH AT STATION OFF5

TOTAL RAINFALL = 4.13, TOTAL LOSS = 1.92, TOTAL EXCESS = 2.20

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR

```

+ (CFS) (HR)
+ 663. 13.37 (CFS) 307. 132. 66. 66.
              (INCHES) 1.286 2.205 2.205 2.205
              (AC-FT) 152 261. 261. 261
              CUMULATIVE AREA = 2.22 SQ MI

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.....

```

*****
*          *
63 KK * CPOFF * CONCENTRATION POINT AT NORTHERN BOUNDARY OF DEV8
*          *
*****

```

```

64 HC HYDROGRAPH COMBINATION
      ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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***          ***          ***          ***          ***

```

HYDROGRAPH AT STATION CPOFF

```

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 48 00-HR
+ 687. 13.33 (CFS) 334. 143. 72. 72.
              (INCHES) 1.291 2.214 2.214 2.214
              (AC-FT) 166. 284. 284. 284
              CUMULATIVE AREA = 2.41 SQ MI

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.....

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*****
*          *
65 KK * ROFF56 * ROUTE CPOFF TO CP8 (DOWNSTREAM BOUNDARY OF DEV8)
*          *
*****

```

HYDROGRAPH ROUTING DATA

```

66 RD MUSKINGUM-CUNGE CHANNEL ROUTING
      L 1394. CHANNEL LENGTH
      S .0750 SLOPE
      N .030 CHANNEL ROUGHNESS COEFFICIENT
      CA .00 CONTRIBUTING AREA
      SHAPE TRAP CHANNEL SHAPE
      WD 10.00 BOTTOM WIDTH OR DIAMETER
      Z .33 SIDE SLOPE

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELEBRITY
		M	DT				
MAIN	3.61	1.50	.95	697.00	686.89	799.78	2.21

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.61	1.50	2.00	686.88	800.00	2.21
------	------	------	------	--------	--------	------

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2842E+03 EXCESS= .0000E+00 OUTFLOW= .2842E+03 BASIN STORAGE= .6838E-03 PERCENT ERROR= .0

```

***          ***          ***          ***          ***

```

HYDROGRAPH AT STATION ROFF56

```

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 48 00-HR
+ 687. 13.33 (CFS) 334. 143 72. 72
              (INCHES) 1.291 2.214 2.214 2.214
              (AC-FT) 166. 284 284. 284.
              CUMULATIVE AREA = 2.41 SQ MI

```



```

*****
*
* 67 KK      DEV8      RUNOFF FROM PROPOSED AREA 8
*
*****

```

SUBBASIN RUNOFF DATA

```

68 BA      SUBBASIN CHARACTERISTICS
          TAREA      .01 SUBBASIN AREA

```

PRECIPITATION DATA

```

10 PH      DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          ..... HYDRO-35 ..... TP-40 ..... TP-49 .....
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          .41   78   1.29  1.39  1.48  1.93  2.87  4.14  .00   .00   .00   .00

          STORM AREA =      01

```

```

69 LS      SCS LOSS RATE
          STRTL      .61 INITIAL ABSTRACTION
          CRVNR      76.60 CURVE NUMBER
          RTIMP      10.20 PERCENT IMPERVIOUS AREA

```

```

70 UD      SCS DIMENSIONLESS UNITGRAPH
          TLAG      .07 LAG

```

UNIT HYDROGRAPH
12 END-OF-PERIOD ORDINATES

```

          19.      60.      64.      42      21.      12.      6.      3.      2.      1.
          1.      0

```

HYDROGRAPH AT STATION DEV8

TOTAL RAINFALL = 4.14, TOTAL LOSS = 2.02, TOTAL EXCESS = 2.12

PEAK FLOW	TIME	6-HR	24-HR	72-HR	48 00-HR	
(CFS)	(HR)	(CFS)				
18.	12.10	2.	1	0.	0	
		(INCHES)	1.268	2.120	2.121	2.121
		(AC-FT)	1.	1.	1.	1.
CUMULATIVE AREA =		01 SQ MI				

```

*****
*
* 71 KK      DEV10     RUNOFF FROM PROPOSED AREA 10
*
*****

```

SUBBASIN RUNOFF DATA

```

72 BA      SUBBASIN CHARACTERISTICS
          TAREA      .09 SUBBASIN AREA

```

PRECIPITATION DATA

```

10 PH      DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
          ..... HYDRO-35 ..... TP-40 ..... TP-49 .....
          5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
          .41   78   1.29  1.39  1.48  1.93  2.87  4.14  .00   .00   .00   .00

          STORM AREA =      .09

```

```

73 LS      SCS LOSS RATE
          STRTL      .38 INITIAL ABSTRACTION
          CRVNR      84.00 CURVE NUMBER
          RTIMP      7.30 PERCENT IMPERVIOUS AREA

```

```

74 UD      SCS DIMENSIONLESS UNITGRAPH
          TLAG      .07 LAG

```

UNIT HYDROGRAPH

12 END-OF-PERIOD ORDINATES
 154. 475. 507. 336. 169. 93 49. 26. 14 7.
 4. 2.

*** **

HYDROGRAPH AT STATION DEV10

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.52, TOTAL EXCESS = 2.61

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR
176	12.10	16.	7.	3.	3.
		(INCHES) 1.545	2.614	2.614	2.614
		(AC-FT) 8	13.	13.	13.

CUMULATIVE AREA = .09 SQ MI

75 KK *****
 + CP8 + CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV8
 + *****

76 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP8

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR
692.	13.33	348.	150.	75.	75.
		(INCHES) 1.287	2.226	2.228	2.228
		(AC-FT) 173.	299.	299.	299.

CUMULATIVE AREA = 2.51 SQ MI

77 KK *****
 + RCP8_7 + ROUTE CP8 TO CP7 (DOWNSTREAM BOUNDARY OF DEV7)
 + *****

HYDROGRAPH ROUTING DATA

78 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 1991. CHANNEL LENGTH
 S .0790 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	H	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM Celerity
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
MAIN	3.70	1.50	1.33	995.50	691.76	801.89	2.23	25.04

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.70	1.50	2.00		691.73	802.00	2.23	
------	------	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2988E+03 EXCESS= .0000E-00 OUTFLOW= .2988E+03 BASIN STORAGE= .1033E-02 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION RCP8_7

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
692.	13.37	348	150	75	75
		(INCHES) 1.287	2.226	2.228	2.228
		(AC-FT) 173.	299	299	299.

CUMULATIVE AREA = 2.51 SQ MI

79 KK *****
 * DEV9 * RUNOFF FROM PROPOSED AREA 9
 * *****

SUBBASIN RUNOFF DATA

80 BA SUBBASIN CHARACTERISTICS
 TAREA .06 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
S-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .06

81 LS SCS LOSS RATE
 STRTL 65 INITIAL ABSTRACTION
 CRVNR 75.50 CURVE NUMBER
 RTIMP 12.00 PERCENT IMPERVIOUS AREA

82 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 11 LAG

UNIT HYDROGRAPH
 18 END-OF-PERIOD ORDINATES

38.	127.	224.	242.	206.	143	89.	59.	38.	25.
16	11.	7.	4.	3	2	1.	1.		

*** *** *** *** ***

HYDROGRAPH AT STATION DEV9

TOTAL RAINFALL = 4.14, TOTAL LOSS = 2.05, TOTAL EXCESS = 2.09

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
80.	12.13	8.	4	2	2.
		(INCHES) 1.238	2.087	2.089	2.089
		(AC-FT) 4.	7	7	7.

CUMULATIVE AREA = .06 SQ MI

83 KK *****
 * DEV7 * RUNOFF FROM PROPOSED AREA 7
 * *****

SUBBASIN RUNOFF DATA

84 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
S-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .02

85 LS SCS LOSS RATE
 STRTL .85 INITIAL ABSTRACTION
 CRVNR 70.10 CURVE NUMBER
 RTIMP 6.80 PERCENT IMPERVIOUS AREA

86 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 17 LAG

UNIT HYDROGRAPH
 27 END-OF-PERIOD ORDINATES

5.	15.	32.	49.	58.	58.	53.	44.	32.	23.
17.	13.	10.	7.	6.	4.	3.	2.	2.	1.
1.	1.	1.	0.	0.	0.	0.			

HYDROGRAPH AT STATION DEV7

TOTAL RAINFALL = 4.14, TOTAL LOSS = 2.53, TOTAL EXCESS = 1.61

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR	
18.	12.20	2.	1	0.	0.	
		(INCHES)	.977	1.613	1.615	1.615
		(AC-FT)	1	2.	2.	2.

CUMULATIVE AREA = .02 SQ MI

.....

87 KK *****
 * CP7 * COCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV7
 * *****

88 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION CP7

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	48.00-HR	
695.	13.37	358	155.	78.	78.	
		(INCHES)	1.281	2.216	2.220	2.220
		(AC-FT)	178.	307.	308.	308.

CUMULATIVE AREA = 2.60 SQ MI

.....

89 KK *****
 * RCP7_6 * ROUTE CP7 TO CP6 (WESTERN BOUNDARY OF SITE)
 * *****

HYDROGRAPH ROUTING DATA

90 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	940.	CHANNEL LENGTH
S	.0160	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	.33	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY	
		M	DT					
			(MIN)	(FT)	(CFS)	(MIN)	(FPS)	
MAIN	1.67	1.50	1.06	470.00	695.02	801.91	2.22	14.71

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1 67 1.50 2.00 695.02 802.00 2 22

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3078E+03 EXCESS= 0000E+00 OUTFLOW= .3078E+03 BASIN STORAGE= .7405E-03 PERCENT ERROR= 0

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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION  RCP7_6
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 695.         13 37          (CFS)
          (INCHES)      358.        155.        78.         78.
          (AC-FT)       1.281       2.216       2.220       2.220
          CUMULATIVE AREA = 2 60 SQ MI
    
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*****
91 KK  *   DEV6   *   RUNOFF FROM PROPOSED AREA 6
*****
    
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SUBBASIN RUNOFF DATA
92 BA  SUBBASIN CHARACTERISTICS
      TAREA .01 SUBBASIN AREA
    
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PRECIPITATION DATA
10 PH  DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
      HYDRO-35 ..... TP-40 ..... TP-49 .....
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
      41 .78 1.29 1.39 1.48 1.93 2.87 4.14 .00 .00 .00 .00
      STORM AREA = .01
    
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93 LS  SCS LOSS RATE
      STRTL .78 INITIAL ABSTRACTION
      CRVNBR 72.00 CURVE NUMBER
      RTIMP .00 PERCENT IMPERVIOUS AREA
    
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94 UD  SCS DIMENSIONLESS UNITGRAPH
      TLAG .11 LAG
    
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          UNIT HYDROGRAPH
          18 END-OF-PERIOD ORDINATES
          J      11.      19.      20      17.      12.      7.      5.      3.      2.
          1      1.       1.       0.       0.       0.       0.       0.       0.       0.
    
```

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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION  DEV6
TOTAL RAINFALL = 4.14, TOTAL LOSS = 2.58, TOTAL EXCESS = 1.56
    
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PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      48.00-HR
+ 5.           12.13          (CFS)
          (INCHES)      1.         0.         0.         0.
          (AC-FT)       .984       1.559       1.559       1.559
          CUMULATIVE AREA = .01 SQ MI
    
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*****
95 KK  *   CP6   *   CONCENTRATION POINT AT THE MID-WESTERN BOUNDARY OF SITE NEAR
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96 KC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP6

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	48.00-HR
695.	13.37	359.	155.	78.	78.	
		(INCHES)	1.280	2.215	2.218	2.218
		(AC-FT)	178.	308.	308.	308.
CUMULATIVE AREA =			2.61 SQ MI			

.....

97 KK RCP6_5 ROUTE RUNOFF CONCENTRATING AT CP6 TO CP5 IN DAMONTE CHANNEL ALONG

HYDROGRAPH ROUTING DATA

98 RD MUSKINGUM-CUNGE CHANNEL ROUTING
 L 270. CHANNEL LENGTH
 S .0030 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
MAIN	.72	1.50	.53	694.99	802.37	2.22	8.41

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.72	1.50	2.00	694.96	802.00	2.22	
------	-----	------	------	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3083E+03 EXCESS= .0000E+00 OUTFLOW= .3083E+03 BASIN STORAGE= .3814E-03 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION RCP6_5

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	48.00-HR
695.	13.37	359.	155.	78.	78.	
		(INCHES)	1.280	2.215	2.218	2.218
		(AC-FT)	178.	308.	308.	308.
CUMULATIVE AREA =			2.61 SQ MI			

.....

99 KK DEVS RUNOFF FROM PROPOSED AREA 5

SUBBASIN RUNOFF DATA

100 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35				TP-40				TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	00	00	00

STORM AREA = .01

101 LS SCS LOSS RATE

STRTL	.47	INITIAL ABSTRACTION
CRVNBR	81.10	CURVE NUMBER
RTIMP	13.50	PERCENT IMPERVIOUS AREA

102 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	.11	LAG
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UNIT HYDROGRAPH

18 END-OF-PERIOD ORDINATES									
5.	18.	32.	35.	29.	20.	13.	8.	5.	4.
2.	1.	1.	1	0.	0	0.	0.		

HYDROGRAPH AT STATION DEV5

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.64, TOTAL EXCESS = 2.50

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
14	12.13	1.	1.	0.	0.	
		(INCHES)	1.465	2.501	2.503	2.503
		(AC-FT)	1.	1.	1.	1

CUMULATIVE AREA = .01 SQ MI

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103 KK CPS CONCENTRATION POINT WITHIN DAMONTE CHANNEL ALONG DESERT WAY

104 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION CP5

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	48.00-HR	
695.	13.37	360.	156.	78.	78	
		(INCHES)	1.280	2.215	2.219	2.219
		(AC-FT)	179.	309.	309.	309.

CUMULATIVE AREA = 2.61 SQ MI

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105 KK RCP5_1 ROUTE CP5 TO CP1 (NORTHWEST CORNER OF SITE)

HYDROGRAPH ROUTING DATA

106 RD MUSKINGUM-CUNGE CHANNEL ROUTING

L	1120.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	.33	SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.72	1.50	2.00	1120.00	694.91	804.00	2.22	8.41

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.72	1.50	2.00		694.91	804.00	2.22	
------	-----	------	------	--	--------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3095E+03 EXCESS= .0000E+00 OUTFLOW= .3095E+03 BASIN STORAGE= 1793E-02 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION RCP5_1

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR MAXIMUM AVERAGE FLOW	72-HR MAXIMUM AVERAGE FLOW	48.00-HR MAXIMUM AVERAGE FLOW
695.	13.40	360.	156.	78.	78.
		(INCHES) 1.279	2.215	2.219	2.219
		(AC-FT) 178.	309.	309.	309.
CUMULATIVE AREA =		2.61 SQ MI			

.....

107 KK *****
 * TOTCP1 * TOTAL ADDITION OF FLOW AT NORTHWEST CORNER OF SITE

108 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION TOTCP1

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR MAXIMUM AVERAGE FLOW	72-HR MAXIMUM AVERAGE FLOW	48.00-HR MAXIMUM AVERAGE FLOW
1274.	13.33	623.	269.	135.	135.
		(INCHES) 1.302	2.246	2.249	2.249
		(AC-FT) 309.	533.	534.	534.
CUMULATIVE AREA =		4.45 SQ MI			

.....

109 KK *****
 * OFF7 * RUNOFF FROM OFFSITE AREA 7

SUBBASIN RUNOFF DATA

110 BA SUBBASIN CHARACTERISTICS
 TAREA .09 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM											
HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .09

111 LS SCS LOSS RATE
 STRTL .44 INITIAL ABSTRACTION
 CRVNBR 82.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

112 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .31 LAG

UNIT HYDROGRAPH

48 END-OF-PERIOD ORDINATES									
4.	14.	27	44.	67.	94.	115.	129.	137.	137.
134	126.	116.	103.	89.	73	60.	51.	43.	37
31.	27	22.	19.	16.	14.	12.	10.	8.	7.
6	5.	4.	4.	3.	3	2.	2.	2.	1.
1	1.	1.	1.	1.	0	0.	0.		

HYDROGRAPH AT STATION OFF7

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.02, TOTAL EXCESS = 2.32

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48 00-HR
82	12 33	14.	6.	3.	3
		(INCHES) 1.411	2.323	2.323	2.323
		(AC-FT) 7.	12.	12	12.
CUMULATIVE AREA =		.09 SQ MI			

.....

113 KK

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*****
*      ROFF7      *
*                *
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ROUTE OFF7 TO THROUGH DEV7

HYDROGRAPH ROUTING DATA

114 RD

MUSKINGUM-CUNGE CHANNEL ROUTING	
L	1035 CHANNEL LENGTH
S	.1360 SLOPE
N	.030 CHANNEL ROUGHNESS COEFFICIENT
CA	.00 CONTRIBUTING AREA
SHAPE	TRAP CHANNEL SHAPE
WD	5.00 BOTTOM WIDTH OR DIAMETER
Z	.33 SIDE SLOPE

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
			DT (MIN)	DX (FT)				
MAIN	6.96	1.42	1.03	517.50	81.92	741.75	2.32	16.72

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	6.96	1.42	2.00		81.83	742.00	2.32	
------	------	------	------	--	-------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1153E+02 EXCESS= .0000E+00 OUTFLOW= .1153E+02 BASIN STORAGE= .2440E-03 PERCENT ERROR= .0

HYDROGRAPH AT STATION ROFF7

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
82.	12.37	14.	6.	3.	3.
		(INCHES) 1.411	2.323	2.323	2.323
		(AC-FT) 7.	12.	12.	12.
CUMULATIVE AREA =		.09 SQ MI			

.....

115 KK

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*****
*      DEV12      *
*                *
*****

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RUNOFF FROM PROPOSED AREA 12

SUBBASIN RUNOFF DATA

116 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .03

117 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP 2.50 PERCENT IMPERVIOUS AREA

118 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 04 LAG

UNIT HYDROGRAPH
8 END-OF-PERIOD ORDINATES

189. 280. 123. 48. 18. 7. 3. 1.

*** **

HYDROGRAPH AT STATION DEV12

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.60, TOTAL EXCESS = 2.54

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
70.	12.07	6	2.	1	1.
		(INCHES) 1.523	2.536	2.536	2.536
		(AC-FT) 1	5.	5	5.

CUMULATIVE AREA = .03 SQ MI

119 KK *****
* CP12 * CONCENTRATION POINT AT THE DOWNSTREAM BOUNDARY OF DEV12
* *

120 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CP12

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
96.	12.07	20.	8.	4	4.
		(INCHES) 1.434	2.380	2.380	2.380
		(AC-FT) 10.	16.	16	16.

CUMULATIVE AREA = .13 SQ MI

121 KK *****
* RC12 * ROUTE CP12 TO CP11 (DOWNSTREAM BOUNDARY OF DEV11)
* *

HYDROGRAPH ROUTING DATA

122 RD MUSKINGUM-CUNGE CHANNEL ROUTING
L 800 CHANNEL LENGTH
S .0820 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA

SHAPE TRAP CHANNEL SHAPE
 WD 5.00 BOTTOM WIDTH OR DIAMETER
 Z .33 SIDE SLOPE

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	5.41	1.42	.91	400 00	95.15	725.06	2.38	14.66

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	5.41	1.42	2.00		94.49	726 00	2 38	
------	------	------	------	--	-------	--------	------	--

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1621E+02 EXCESS= .0000E+00 OUTFLOW= .1621E+02 BASIN STORAGE=. .2206E-03 PERCENT ERROR= .0

*** **

HYDROGRAPH AT STATION RCP12

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	48.00-HR (CFS)
94.	12.10	20.	1.434	10.	4.
		8.	2.380	16.	2.380
		4.	2.380	16.	16.
		4.	2.380	16.	16.

CUMULATIVE AREA = .13 SQ MI

.....

123 KK *****
 * DEV11 * RUNOFF FROM PROPOSED AREA 11
 * *****

SUBBASIN RUNOFF DATA

124 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35	TP-40	TP-49
5-MIN .41	2-HR 1.39	2-DAY .00
15-MIN .78	3-HR 1.48	4-DAY .00
60-MIN 1.29	6-HR 1.93	7-DAY .00
	12-HR 2.87	10-DAY .00
	24-HR 4.14	

STORM AREA = .03

125 LS SCS LOSS RATE
 STRTL .41 INITIAL ABSTRACTION
 CRVNR 93.00 CURVE NUMBER
 RTIMP 13.00 PERCENT IMPERVIOUS AREA

126 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .05 LAG

UNIT HYDROGRAPH
 10 END-OF-PERIOD ORDINATES

115.	244.	166.	68.	31.	13	6	2.	1.	0.
------	------	------	-----	-----	----	---	----	----	----

*** **

HYDROGRAPH AT STATION DEV11

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.51, TOTAL EXCESS = 2.63

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	48.00-HR (CFS)
67.	12.07	6.	1.537	3.	1.
		2.	2.632	5.	2.633
		1.	2.633	5.	5.
		1.	2.633	5.	5.

CUMULATIVE AREA = .03 SQ MI

.....

127 KK *****
* CP11 * CONCENTRATION POINT AT DOWNSTREAM BOUNDARY OF DEV11
* *

128 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CP11

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
		(CFS)			
+ 159.	12.07	25.	11.	5	5.
		(INCHES)			
		1.454	2.430	2.433	2.433
		(AC-FT)			
		13	21.	21.	21.
CUMULATIVE AREA =		.16 SQ MI			

.....

129 KK *****
* OFF8 * RUNOFF FROM OFFSITE AREA 8
* *

SUBBASIN RUNOFF DATA

130 BA SUBBASIN CHARACTERISTICS
TAREA 02 SUBBASIN AREA

PRECIPITATION DATA

10 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.41	.78	1.29	1.39	1.48	1.93	2.87	4.14	.00	.00	.00	.00

STORM AREA = .02

131 LS SCS LOSS RATE

STRTL	.46	INITIAL ABSTRACTION
CRVNR	81.40	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

132 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .19 LAG

UNIT HYDROGRAPH
31 END-OF-PERIOD ORDINATES

4.	11.	22.	37.	48.	52.	51.	46.	40.	31.
23	17.	14.	11.	8.	6.	5.	4.	3.	2.
2.	1.	1.	1.	1.	1.	0.	0.	0.	0.
0									

*** *** *** *** ***

HYDROGRAPH AT STATION OFF8

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.87, TOTAL EXCESS = 2.27

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
		(CFS)			
+ 25.	12.23	3.	1	1.	1.
		(INCHES)			
		1.390	2.273	2.273	2.273
		(AC-FT)			
		2.	3.	3.	3.
CUMULATIVE AREA =		.02 SQ MI			

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*   *
133 KK *   DEV13   *   RUNOFF FROM PROPOSED AREA 13
*   *
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SUBBASIN RUNOFF DATA

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134 BA   SUBBASIN CHARACTERISTICS
        TAREA      .09  SUBBASIN AREA

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PRECIPITATION DATA

```

10 PH   DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM
        HYDRO-35   TP-40   TP-49
        5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
        .41   .78   1.29   1.39 1.48 1.93 2.87 4.14 .00 .00 .00 .00

```

STORM AREA = .09

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135 LS   SCS LOSS RATE
        STRTL      .40  INITIAL ABSTRACTION
        CRVNR      83.20 CURVE NUMBER
        RTIMP      11.00 PERCENT IMPERVIOUS AREA

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136 UD   SCS DIMENSIONLESS UNITGRAPH
        TLAG      .20  LAG

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UNIT HYDROGRAPH

32 END-OF-PERIOD ORDINATES

14	40.	83.	139	182.	202.	202.	185.	161.	129
95	74.	57.	45.	35.	27.	21.	17.	13.	10.
8	6.	5.	4.	3	2.	2.	1.	1	1
0.	0.								

*** *** *** *** ***

HYDROGRAPH AT STATION DEV13

TOTAL RAINFALL = 4.14, TOTAL LOSS = 1.53, TOTAL EXCESS = 2.61

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
112.	12.23	15.	6.	3.	3.
		(INCHES) 1.528	2.610	2.614	2.614
		(AC-FT) 7	13.	13.	13.

CUMULATIVE AREA = .09 SQ MI

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*****
*   *
137 KK *   CP13   *   COCENTRATION POINT ALONG THE DAMONTE RANCH HIGH SCHOOL
*   *
*****

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138 HC   HYDROGRAPH COMBINATION
        ICOMP      3   NUMBER OF HYDROGRAPHS TO COMBINE

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*** *** *** *** ***

HYDROGRAPH AT STATION CP13

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	48.00-HR
248	12.13	44.	18.	9.	9.
		(INCHES) 1.473	2.476	2.479	2.479
		(AC-FT) 22.	36.	36.	36.

CUMULATIVE AREA = .28 SQ MI

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	OFF4	139.	12.53	31.	13.	6.	.21		

+	ROUTED TO	ROFF4	139.	12.57	31.	13	6.	.21
+	HYDROGRAPH AT	OFF3	68.	12.37	12	5.	2.	.08
+	HYDROGRAPH AT	DEV4	31.	12.17	4.	1	1.	.02
+	3 COMBINED AT	CP4	205.	12.47	47	19.	10.	.31
+	ROUTED TO	RCP4_3	204.	12.47	47.	19	10.	.31
+	HYDROGRAPH AT	OFF2	108.	12.60	26.	11	5.	.17
+	HYDROGRAPH AT	DEV3	97.	12.20	12	5.	3.	.07
+	3 COMBINED AT	CP3	342.	12.47	85	35.	18.	.56
+	ROUTED TO	RCP3_1	342.	12.50	85	35.	18.	.56
+	HYDROGRAPH AT	OFF1	579.	13.27	250.	107.	53.	1.73
+	HYDROGRAPH AT	DEV2	86.	12.30	13.	6.	3.	.10
+	HYDROGRAPH AT	DEV1	14.	12.20	2.	1	0.	.01
+	3 COMBINED AT	CP1	584.	13.27	264	113.	57.	1.84
+	HYDROGRAPH AT	OFF6	129.	12.50	28	12.	6.	.19
+	ROUTED TO	ROFF6	128.	12.53	28	12	6.	.19
+	HYDROGRAPH AT	OFF5	663.	13.37	307	132	66.	2.22
+	2 COMBINED AT	CPOFF	687.	13.33	334	143	72.	2.41
+	ROUTED TO	ROFF56	687.	13.33	334.	143	72.	2.41
+	HYDROGRAPH AT	DEV8	18.	12.10	2.	1.	0.	.01
+	HYDROGRAPH AT	DEV10	176.	12.10	16.	7	3.	.09
+	3 COMBINED AT	CP8	692	13.33	348.	150	75.	2.51
+	ROUTED TO	RCP8_7	692.	13.37	348.	150.	75.	2.51
+	HYDROGRAPH AT	DEV9	80.	12.13	8	4.	2.	.06
+	HYDROGRAPH AT	DEV7	18.	12.20	2.	1	0.	.02
+	3 COMBINED AT	CP7	695.	13.37	358.	155.	78.	2.60
+	ROUTED TO	RCP7_6	695.	13.37	358.	155	78.	2.60
+	HYDROGRAPH AT	DEV6	5.	12.13	1.	0	0	.01
+	2 COMBINED AT	CP6	695.	13.37	359.	155.	78.	2.61
+	ROUTED TO	RCP6_5	695.	13.37	359	155.	78.	2.61
+	HYDROGRAPH AT	DEV5	14.	12.13	1.	1	0.	.01
+	2 COMBINED AT	CP5	695.	13.37	360	156.	78.	2.61
	ROUTED TO							

+		RCP5_1	695.	13.40	360.	156	78.	2.61
+	2 COMBINED AT	TOTCF1	1274	13.33	623.	269.	135.	4.45
+	HYDROGRAPH AT	OPF7	82.	12.33	14.	6.	3.	.09
+	ROUTED TO	ROFF7	82.	12.37	14.	6.	3.	.09
+	HYDROGRAPH AT	DEV12	70.	12.07	6.	2	1.	.03
+	2 COMBINED AT	CP12	96.	12.07	20.	8.	4.	.13
+	ROUTED TO	RCP12	94.	12.10	20.	8.	4	.13
+	HYDROGRAPH AT	DEV11	67.	12.07	6.	2	1.	.03
+	2 COMBINED AT	CP11	159.	12.07	25.	11.	5	.16
+	HYDROGRAPH AT	OFF8	25.	12.23	3.	1.	1.	.02
+	HYDROGRAPH AT	DEV13	112.	12.23	15.	6.	3.	.09
+	3 COMBINED AT	CP13	248.	12.13	44.	18.	9.	.28

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)	
							PEAK (CFS)	TIME TO PEAK (MIN)		
	ROFF4	MANE	2.00	139.34	754.00	2.32	2.00	139.34	754.00	2.32
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2564E+02 EXCESS= .0000E+00 OUTFLOW= .2564E+02 BASIN STORAGE= .7473E-03 PERCENT ERROR= .0										
	RCP4_3	MANE	61	204.39	748.94	2.32	2.00	204.06	748.00	2.32
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3843E+02 EXCESS= .0000E+00 OUTFLOW= .3843E+02 BASIN STORAGE= .2863E-03 PERCENT ERROR= .0										
	RCP3_1	MANE	2.00	342.17	750.00	2.36	2.00	342.17	750.00	2.36
CONTINUITY SUMMARY (AC-FT) - INFLOW= .7007E+02 EXCESS= .0000E+00 OUTFLOW= .7007E+02 BASIN STORAGE= .1794E-02 PERCENT ERROR= .0										
	ROFF6	MANE	1.46	128.39	750.93	2.32	2.00	128.25	752.00	2.32
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2304E+02 EXCESS= .0000E+00 OUTFLOW= .2304E+02 BASIN STORAGE= .6351E-03 PERCENT ERROR= .0										
	ROFF56	MANE	.95	686.89	799.78	2.21	2.00	686.88	800.00	2.21
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2842E+03 EXCESS= .0000E+00 OUTFLOW= .2842E+03 BASIN STORAGE= .6838E-03 PERCENT ERROR= .0										
	RCP8_7	MANE	1.33	691.76	801.89	2.23	2.00	691.73	802.00	2.23
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2988E+03 EXCESS= .0000E+00 OUTFLOW= .2988E+03 BASIN STORAGE= .1033E-02 PERCENT ERROR= .0										
	RCP7_6	MANE	1.06	695.02	801.91	2.22	2.00	695.02	802.00	2.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3078E+03 EXCESS= .0000E+00 OUTFLOW= .3078E+03 BASIN STORAGE= .7405E-03 PERCENT ERROR= .0										
	RCP6_5	MANE	.53	694.99	802.37	2.22	2.00	694.96	802.00	2.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3083E+03 EXCESS= .0000E+00 OUTFLOW= .3083E+03 BASIN STORAGE= .3814E-03 PERCENT ERROR= .0										
	RCP5_1	MANE	2.00	694.91	804.00	2.22	2.00	694.91	804.00	2.22



INITIAL SUBMITTAL

DATE:	JULY 2005
SCALE:	H: 1" = 150' V: N/A
DRAWN BY:	DK
DESIGNED BY:	DK
ENGR. INT.	
BY:	
DATE:	
COUNTY APPROVED:	
DESCRIPTION:	
NO.	

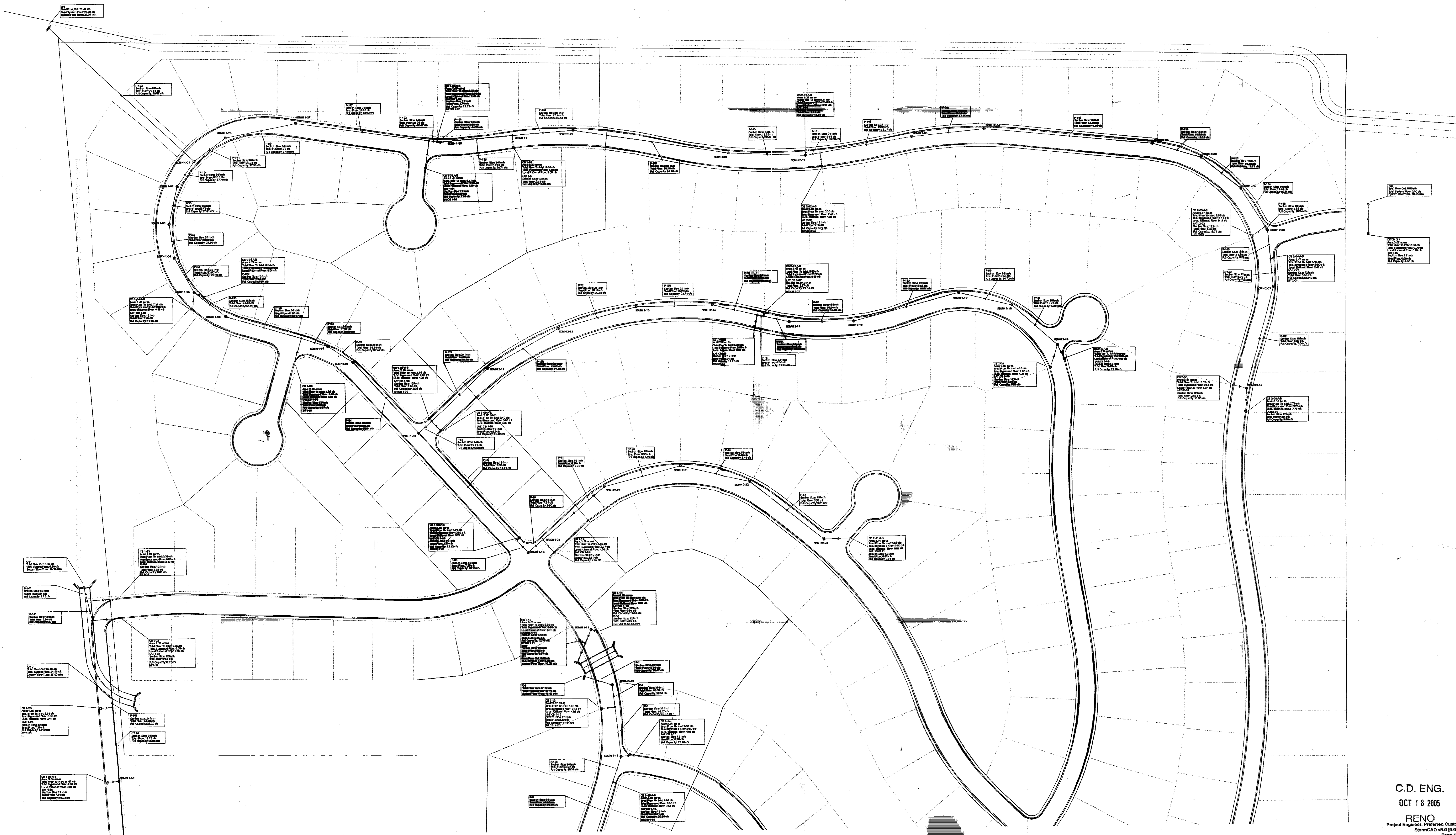
WOOD RODGERS
 ENGINEERING - MAPPING - PLANNING - SURVEYING
 6774 South McCarran Blvd. Reno, NV 89509
 Tel 775.823.4068 Fax 775.823.4066

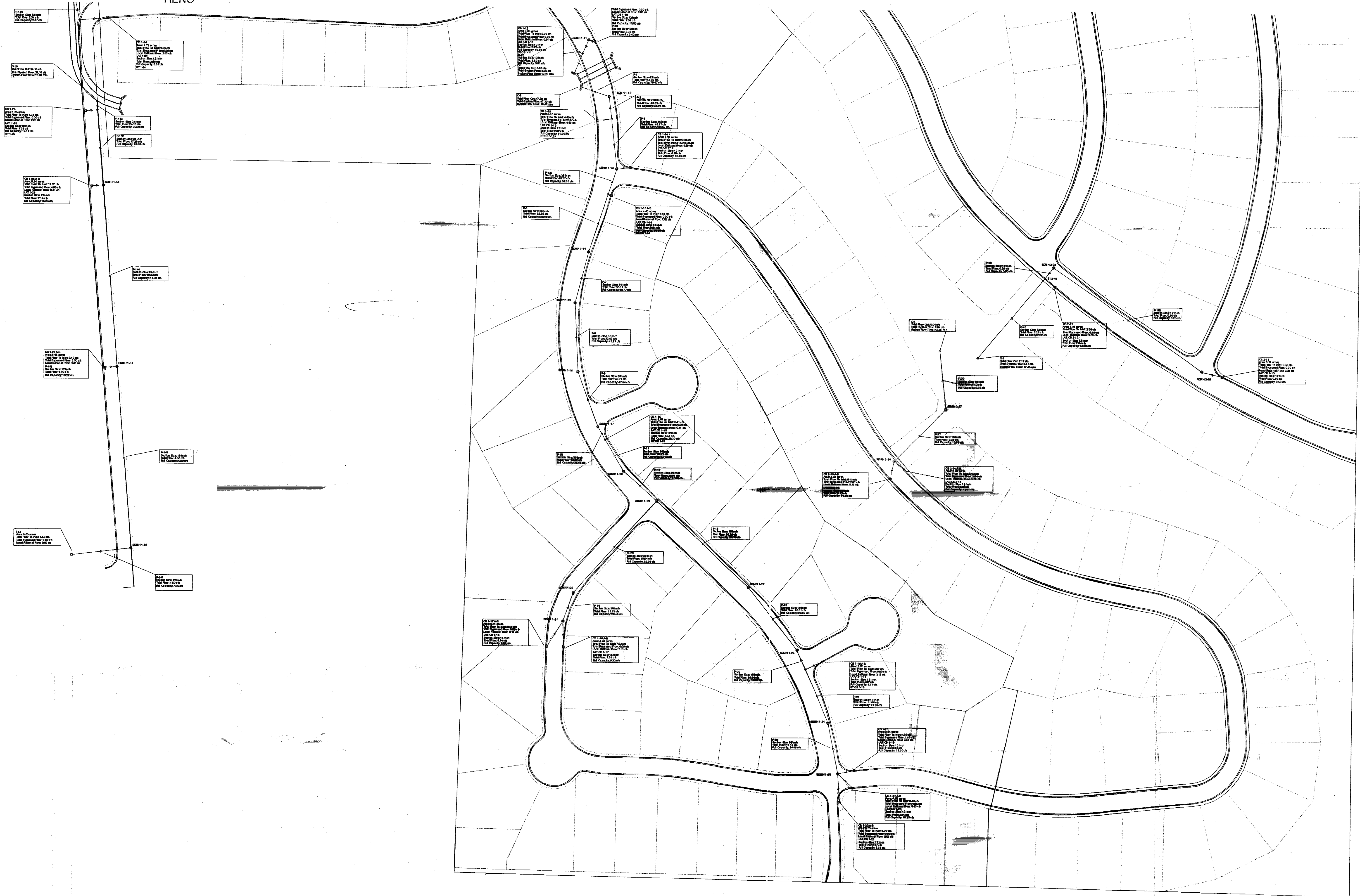
IMPROVEMENT PLANS FOR
GOLDEN HILLS PHASES 1A & 1B
 DRAINAGE PLAN FOR
GOLDEN HILLS PHASES 1 & 2
 CITY OF RENO NEVADA

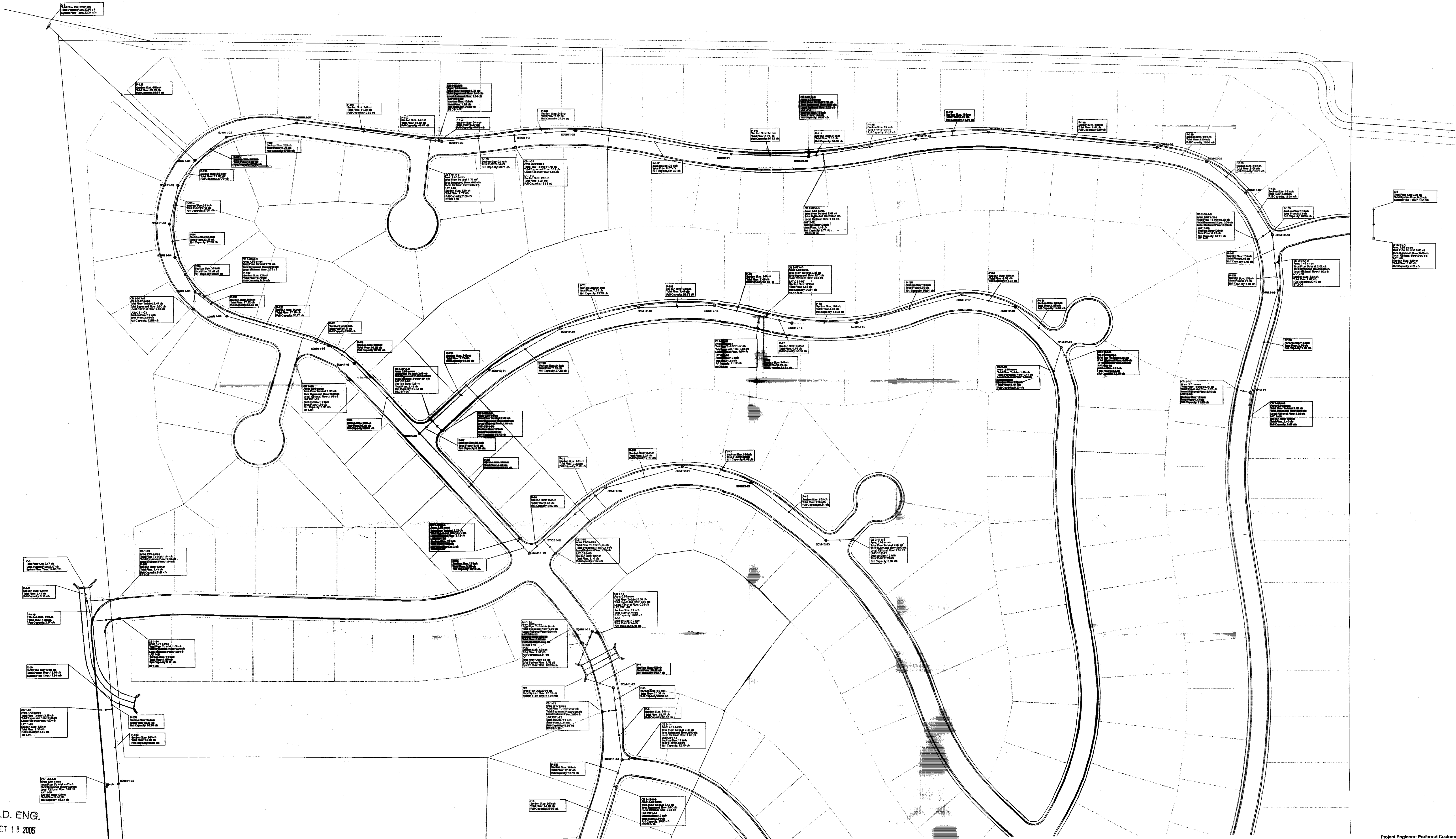
PROJECT NO.	1452.003
DRAWING	DR-1
SHT	51 OF 58

WOOD RODGERS
 ENGINEER - STATE OF NEVADA
 DAVID M. KITCHEN
 EXP-630/07
 CIVIL
 No. 14487

DATE: OCT 18 2005
 RENO







C.D. ENG.
OCT 13 2005

File: C:\G\HILLS CA
H:_civ\stud\drain\storm\ghos_5.sdm
10/06/05 10:10:45 AM

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