

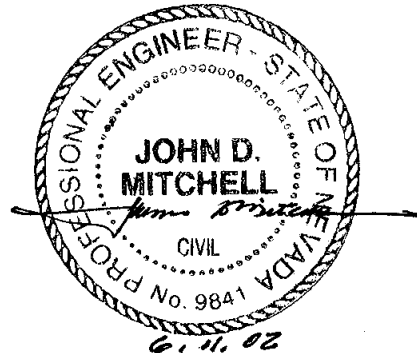
*LDPAJ-03946*  
**COIT PLAZA WAL-MART**

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CITY OF RENO  
Community Development Dept.

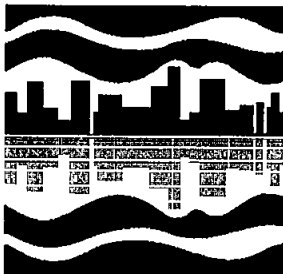
**HYDROLOGY**

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PREPARED BY: John Mitchell, P.E.  
Paula Hicks, E.I.



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June 7, 2002

2002.0003

## INTRODUCTION

Coit Plaza, APN numbers 39-051-07 & 39-490-02, totaling approximately 28.8 acres, is located in the southeast corner of Section 5, Township 19 North, Range 19 East M.D.M. The site, zoned AC, is bounded by McCarran Boulevard on the East, West Seventh Street on the North, Sierra Highlands Drive on the West and Mae Anne Boulevard and existing commercial development to the south. Apartments are located to the North and West and commercial development on the East and South. The site is undeveloped with ground cover of sage brush, grasses and stock piles of earth that are partially over grown. Figure 1, the vicinity map, shows the site in relationship to these surrounding features.

The site is shown on FEMA Flood Insurance Rate Map, (FIRM), Panel 320021 - 2984 E dated September 30, 1994. The map shows the site in an unshaded flood zone X , an areas determined to be outside the 500-year flood plain. A copy of this FIRM is included in the calculation section for reference.

## RELATED STUDIES:

1. Improvement Plans for Coit Heights Unit No.1, SEA Engineers, October 1983.
2. Improvement Plans for Coit Heights Unit No.2, Joe L. Murin, November 1984.
3. Improvement Plans for Sierra Highlands Apartments, Jeff Codega Planning/Design, February 1995.
4. Hydrology Report for Pine Creek Village Apartments, Fricke Engineering, March 1993.
5. Hydrology Report Silverado Estates Unit 2 Phase 1, Summit Engineering, September 1994.
6. Hydrology Report for Silverado Estates Unit 2 Phase 2, Pyramid Engineers, January 1996.
7. Westcreek Apartments Hydrology, Jeff Codega Planning\Design, April 1996.
8. Coit Plaza Hydrology, Jeff Codega Planning\Design, February 1997.
9. Hydrology Report for Silverado Ranch Estates Unit #6, Summit Engineering, May 1999.

## METHODOLOGY

The peak discharges for the project were calculated using the Rational Method:

$$Q=CiA$$

Where;

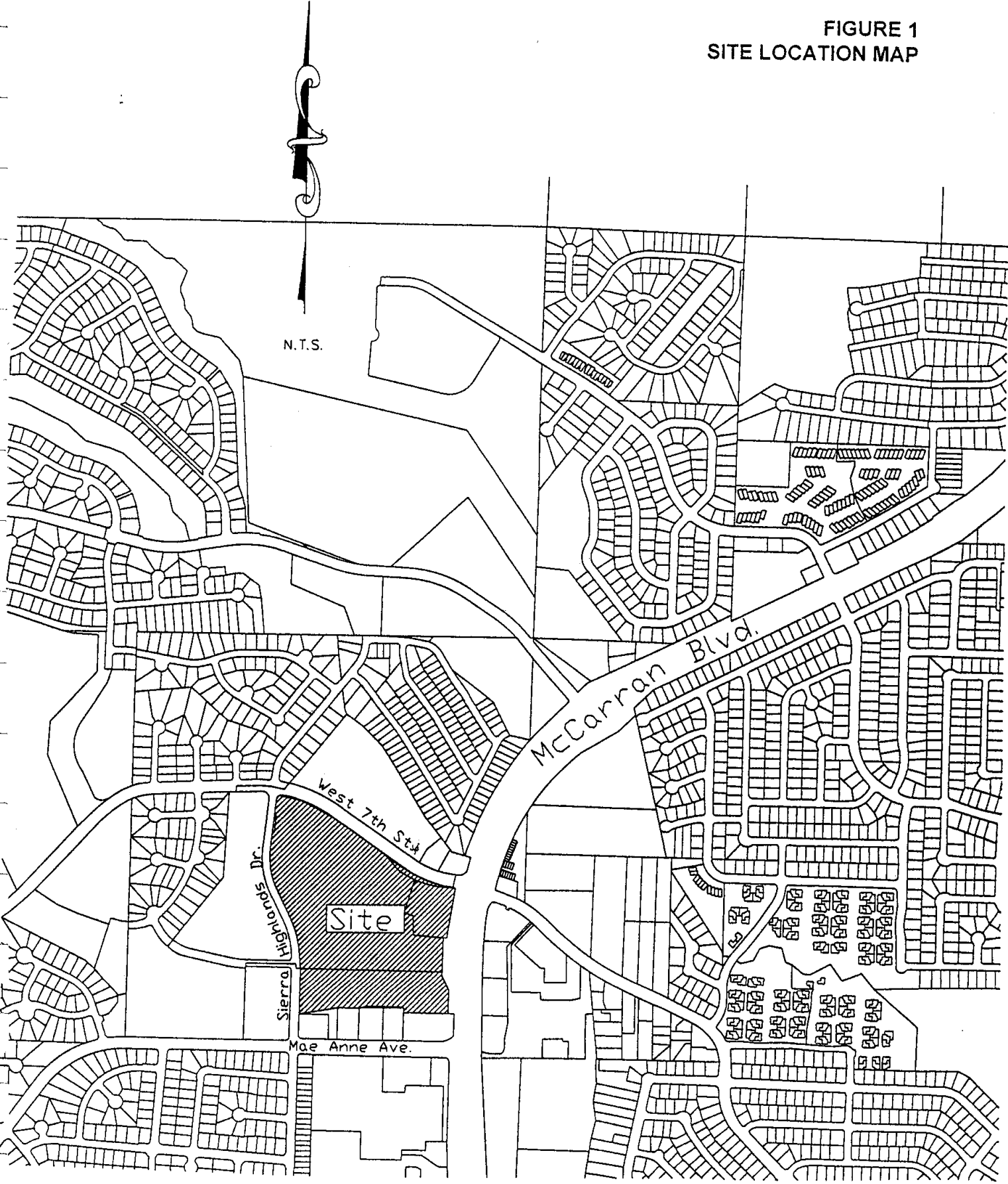
- Q= peak discharge in cubic feet per second,
- C= Rational discharge coefficient based on surface characteristics,
- I= peak rainfall intensity in inches per hour based on basin travel times,
- A= basin area in acres.

Where travel times were calculated to be less than 10 minutes a travel time of 10 minutes, was used.

Detention facilities were analyzed and designed using Pond Pack V7 from Haestad Methods.

The storm drain network for the site was analyzed using Flow Master from Haestad Methods.

FIGURE 1  
SITE LOCATION MAP



## EXISTING CONDITIONS

The site is currently undeveloped with a vegetative cover of sagebrush and grasses. The terrain is typically gully and ridge. Some localized soil stock piling has occurred on the site in the past. The site drains generally to the southeast and exits the site in a 60" CMP under McCarran Boulevard. There is an existing 24" RCP storm drain system that flows west to east along the south of the site, that also exits under McCarran Boulevard near the Wells Fargo Bank. Both the 60" CMP and the 24" RCP drainage are collected in the 54" storm system constructed with Canyon Center Phase I. The 54" storm system exits into the existing drainage east of McCarran Boulevard. Figure 2 is the existing condition drainage map showing these features. The area of the overall watershed that will be affected by the proposed development is 28.8 acres. The rational coefficient used for the existing condition was 0.40 from the City of Reno Design Manual for open space. A travel time of 10 minutes was used to derive the rainfall intensity as per the City of Reno Design Manual. Table 1 is a summary of the hydrologic data and the discharges calculated for the watershed.

**TABLE 1** Existing Condition Site Discharge

	Area (ac)	C	Travel Time (min)	Intensity (in/hr)	Discharge (cfs)
5 YEAR	28.8	0.40	10	1.4	16.1
100 YEAR	28.8	0.40	10	3.8	43.8

Some of the perimeter streets and lots surface drain onto the site. This perimeter flow is tabulated in Table 2.

**TABLE 2** Existing Condition Perimeter Discharge

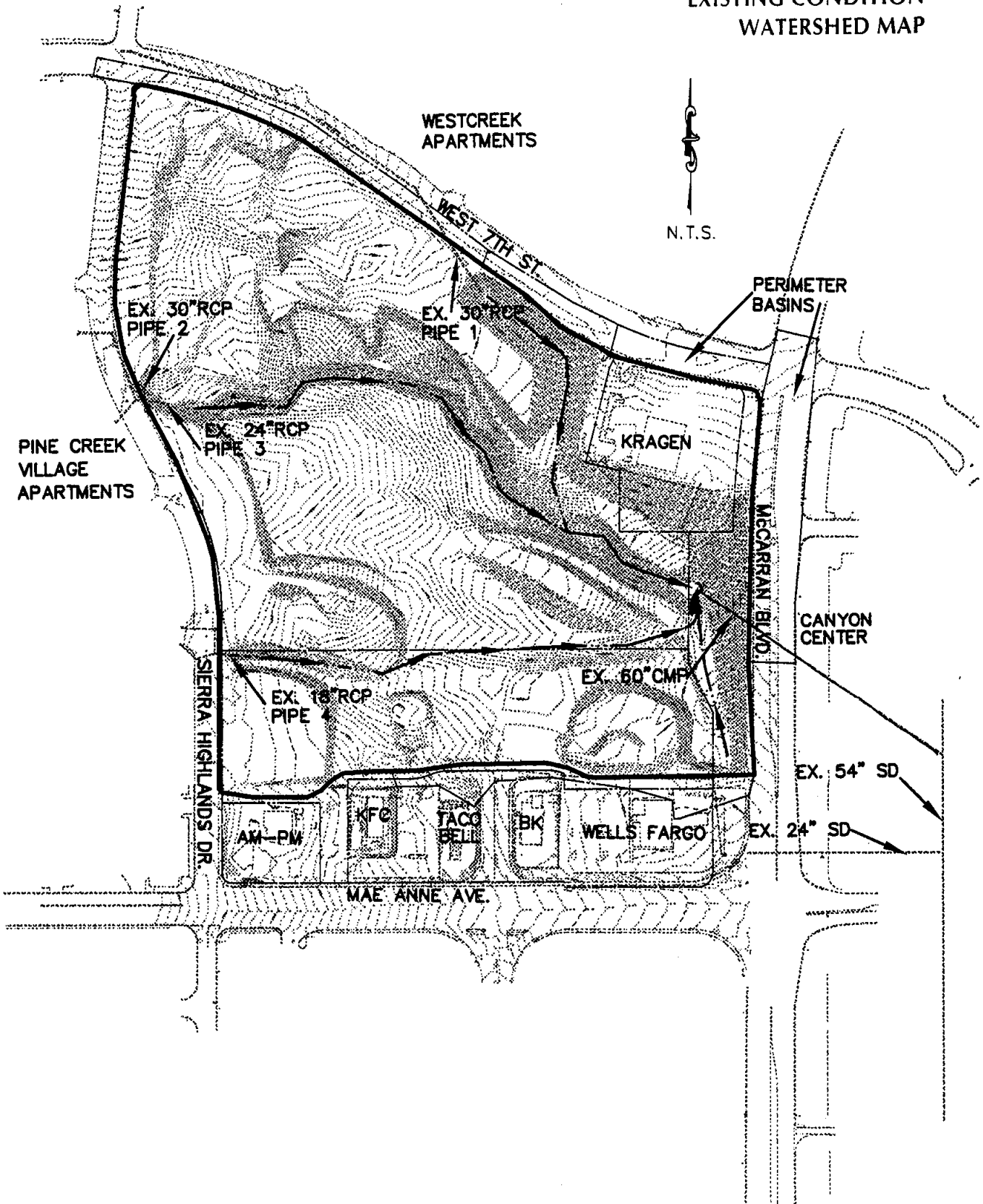
Basin #	Area (ac)	C	Travel Time (min)	Discharge 5-yr (cfs)	Discharge 100-yr(cfs)
13	1.56	0.90	10	1.97	5.33
14	0.42	0.90	10	0.53	1.43
15	0.33	0.90	10	0.42	1.13
16	0.77	0.90	10	0.97	2.63
17	0.70	0.85	10	0.83	2.26

Four existing storm drain pipes enter the site. Pipe number 1 is a 30" RCP located mid way along West Seventh Street, pipe number 2 is a 30" RCP and pipe 3 is a 24" RCP that enters one-third of the way south along Sierra Highlands Drive and pipe 4 is an 18" RCP is located east of the intersection of Villa Verde and Sierra Highlands Drives. Table 3 shows the estimated discharge for each of the 4 pipes as modeled by HEC-1 (see calculations section). These discharges were estimated based on the applicable upstream hydrology reports and plans. The detention basin designed with Silverado Estates Unit 2 Phase 1 was included in the HEC-1 model for Pipe 1 to determine the detained flow in this pipe.

**TABLE 3.** Existing Discharge on Existing Pipes

PIPE	Q5 (cfs)	Q100 (cfs)	Capacity (cfs)
Pipe 1 (30" RCP)	25	140	91.6
Pipe 2 (30" RCP)	*	*	50.2
Pipe 3 (24" RCP)	12	60	17.1
Pipe 4 (18" RCP)	5	25	53.8
* Because Pipes 2 and 3 drain nearly the same area, the discharge for these areas is combined and is shown as the discharge in Pipe 3.			

FIGURE 2  
EXISTING CONDITION  
WATERSHED MAP



DEVELOPED CONDITIONS

The proposed development consists of the Wal-mart site (22.37ac), and two Out-lots (3.66ac and 0.59ac). This proposed development area (26.62ac) in addition to the existing Kragen auto Parts lot (2.18ac) composes the 28.8ac total area for Coit Plaza. The main Wal-mart retail building is near the west edge of the site with Sierra Highlands Drive on one side. The other three sides are parking areas. There is an area for a detention pond located south of the existing Kragen Auto Parts Building. The two Out-lots are located in the northwest and southeast corners of Coit Plaza. It is assumed that these Out-lots will be developed in the future.

Three systems to be dedicated to the City of Reno are continuations of the existing drainage entering the site, and these systems are displayed in Figure 3. System A is the continuation of the existing 30" RCP in West Seventh Street, Pipe 1. System B intercepts the existing 30" and 24" RCP in Sierra Highlands Drive, Pipes 2 and 3. Perimeter Basin 16 drains into a proposed D.I. in West 7<sup>th</sup> Street which joins System A and System B. System C is the continuation of the 30" RCP at the intersection of Villa Verde & Sierra Highland Drives, Pipe 4. Perimeter Basin 13 sheet flows into an existing rip rap swale that will be extended to discharge next to Systems A & B. Systems A, B, and C discharge into an open rip rap lined channel between McCarran and the onsite detention pond. From the rip rap channel the water will drop into the existing 60" RCP through a large drop inlet. (See Details 2 and 3)

The on-site developed flows were separated into two systems that run from the west side of the site to the detention pond on the east side of the site. System D connects basins 1, 2, 3, 5, and 6 on the north side of the Wal-Mart building. System E connects basins 4, 12, 11, 10, and 9 on the south side of the building. Basin 8 sheet flows into the pond. Perimeter Basin 17 drains into Basins 8, 10 and 11. Basin 7 (Kragen Auto Parts) and Perimeter Basins 14 and 15 drain into the detention pond through two existing 8" storm drain lines. The storage volume of water that must be detained is less than 3.0 acre-feet. The total pond volume is over 3.0 acre-feet calculated from a bottom elevation of 54.0 to the top water surface of 65.0. Detention calculations are provided for both the 5 year and 100 year storms. A detail of the outlet structure is included (Detail 4) which consists of a modified type 1A DI with a 15" RCP. The 15" RCP will function in the lower flow events, while the high flow will flow over the 48" grate on the top of the drop inlet (DI).

**TABLE 3a.** Developed Condition Site Discharge (overall)

	Area (ac)	C	Travel Time (min)	Intensity (in/hr)	Discharge (cfs)	Increase (cfs)
5 YEAR	28.8	0.850	10	1.4	34.3	18.2
100 YEAR	28.8	0.850	10	3.8	93.0	49.2



TABLE 3b. Developed Condition Site Discharge (by basin)

Basin #	Area (ac)	C	Travel Time (min)	Discharge 100-yr (cfs)	Discharge 5-yr (cfs)
1	5.46	0.850	10	17.6	6.5
2	1.44	0.850	10	4.6	1.7
3	1.45	0.850	10	4.7	1.7
4	6.10	0.850	10	19.7	7.3
5	0.32	0.850	10	1.0	0.4
6	2.62	0.850	10	8.5	3.1
7	1.68	0.850	10	5.4	2.0
8	3.34	0.850	10	10.8	4.0
9	2.62	0.850	10	8.4	3.1
10	1.70	0.850	10	5.5	2.0
11	0.89	0.850	10	2.9	1.1
12	1.20	0.850	10	3.9	1.4
TOTAL	28.8	0.850	10	93.0	34.3

Some of the perimeter streets and lots surface drain onto the site. This perimeter flow is tabulated in Table 3c. (Note: perimeter flow does not change with site development).

**TABLE 3c** Proposed Condition Perimeter Discharge

Basin #	Area (ac)	C	Travel Time (min)	Discharge 5-yr (cfs)	Discharge 100-yr(cfs)
13	1.56	0.90	10	1.97	5.33
14	0.42	0.90	10	0.53	1.43
15	0.33	0.90	10	0.42	1.13
16	0.77	0.90	10	0.97	2.63
17	0.70	0.85	10	0.83	2.26

### ON SITE DETENTION

The detention basin outlet structure will control the outlet flow rate. The 15 " RCP will be the limiting structure for 5-yr flows. This two stage structure will limit the 5 year and 100 year storms for the onsite water. The offsite water will bypass the detention pond and outlet structure. A detail of the outlet structure is included in the calculations section.

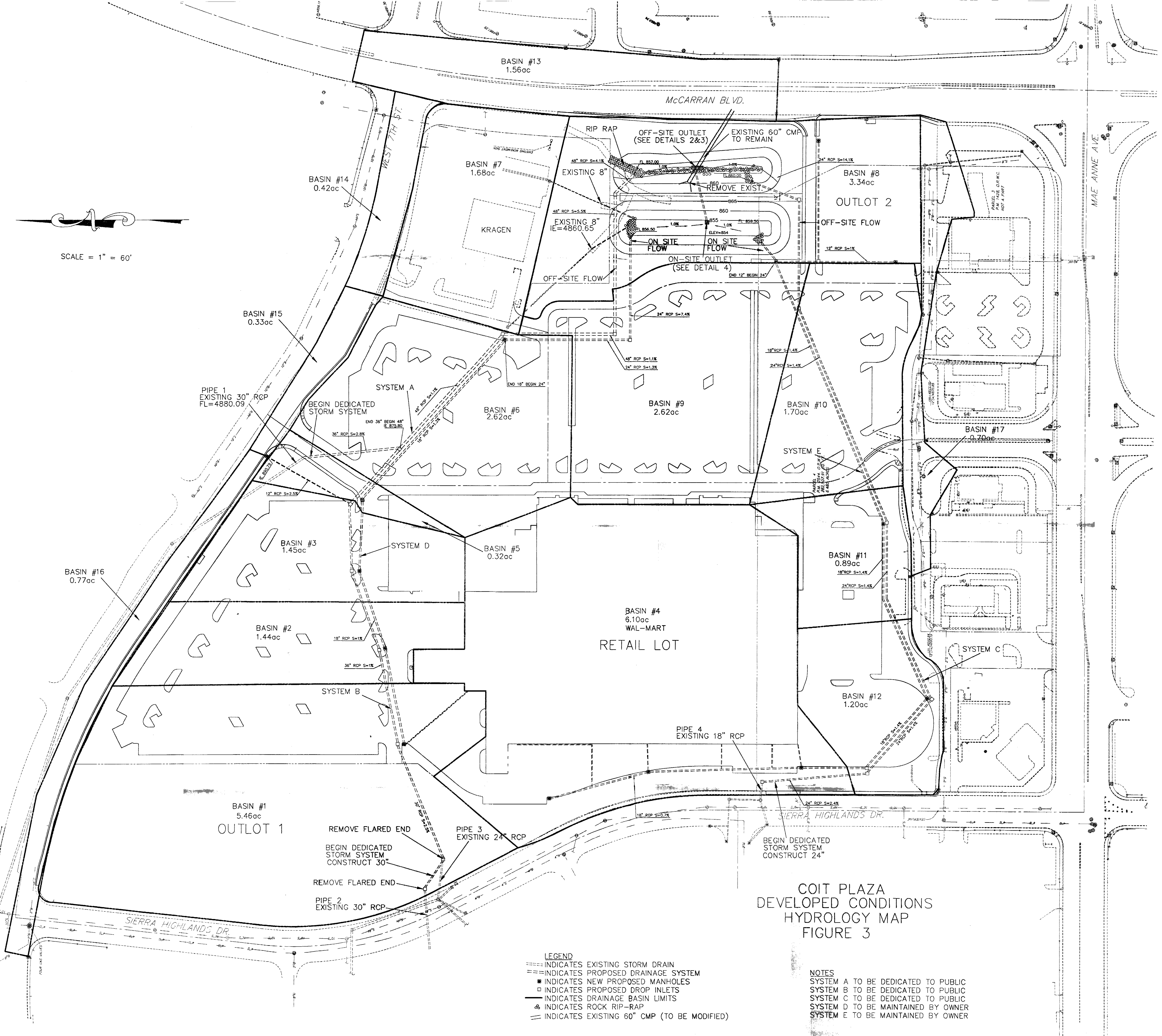
The detention basin will have 3:1 side slopes from the inlet elevation to the top of the basin at elevation 65.0. This provides more than 4' of freeboard from the 100-yr elevation 60.64. Drainage from the surface of McCarran Blvd. Will drain to the east and not enter the detention pond. Drainage from the DOT ROW west of the west shoulder of McCarran will enter the pond as part of Basin #8.

The detention pond and outlet structure were designed using the Pond Pack program. The increase in onsite flow (5-yr and 100-yr) due to development will all be detained in the onsite pond.

**FIGURE 3  
DEVELOPED CONDITION  
WATERSHED MAP**



SCALE = 1" = 60'



- LEGEND**
- INDICATES EXISTING STORM DRAIN
  - - - - INDICATES PROPOSED DRAINAGE SYSTEM
  - INDICATES NEW PROPOSED MANHOLES
  - INDICATES PROPOSED DROP INLETS
  - INDICATES DRAINAGE BASIN LIMITS
  - ⊗ INDICATES ROCK RIP-RAP
  - INDICATES EXISTING 60" CMP (TO BE MODIFIED)

- NOTES**
- SYSTEM A TO BE DEDICATED TO PUBLIC
  - SYSTEM B TO BE DEDICATED TO PUBLIC
  - SYSTEM C TO BE DEDICATED TO PUBLIC
  - SYSTEM D TO BE MAINTAINED BY OWNER
  - SYSTEM E TO BE MAINTAINED BY OWNER

COIT PLAZA  
DEVELOPED CONDITIONS  
HYDROLOGY MAP  
FIGURE 3

## CONCLUSIONS

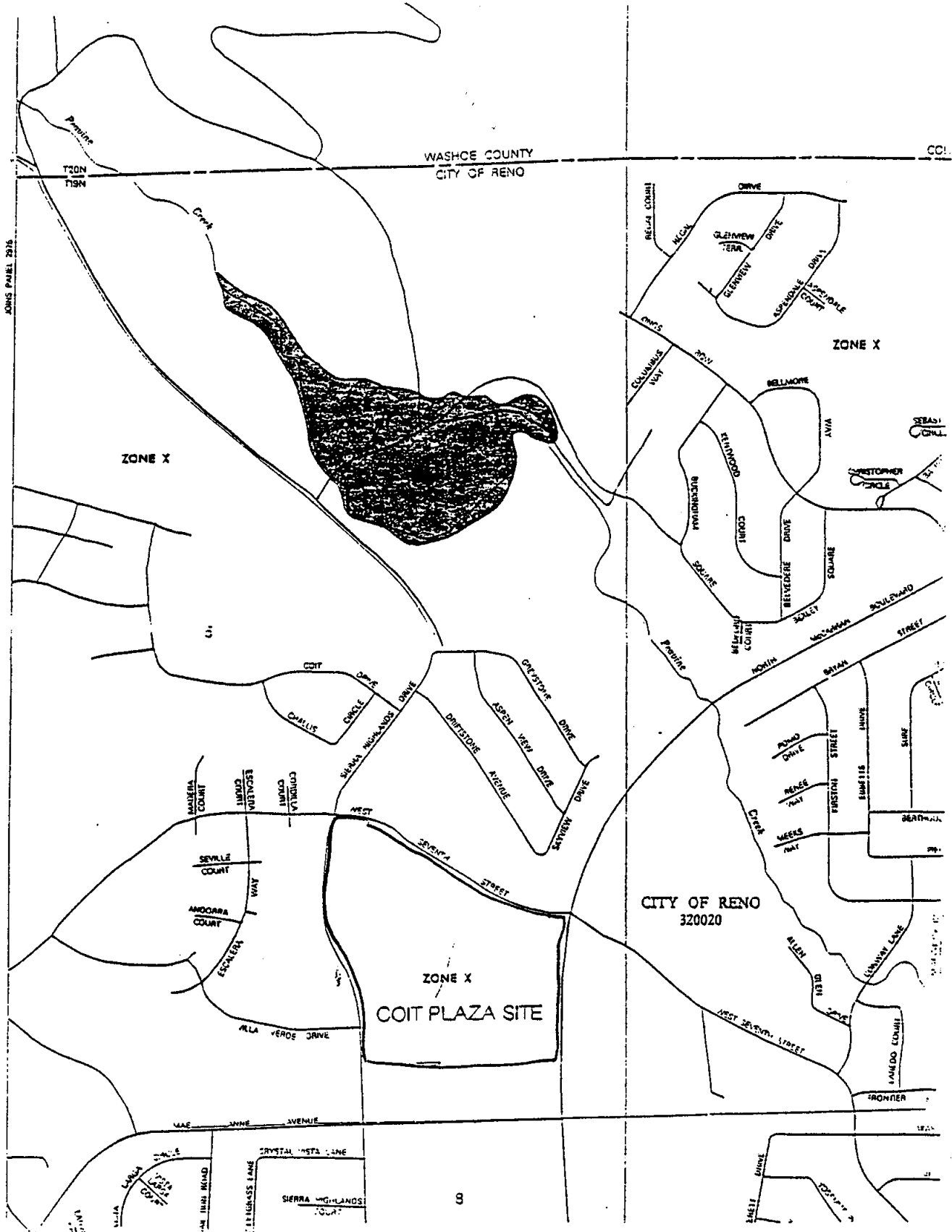
The design of the storm drain system in Coit Plaza is intended to provide adequate capacity to convey the flows for the 5 year storm onsite. The 100 year runoff onsite will be conveyed in the driveways and parking areas between the buildings as well as the storm drain system. The final building pad elevations should be set at least one foot above the 100 year water surface elevation in the area between the buildings. The 5-yr and 100-yr runoff arriving at the site (from off site) will be conveyed through a separate storm system.

The detention facility and both on and off site storm systems will be constructed with the development of Wal-mart.

The detention pond is utilized to detain onsite flows for both the 5-yr and 100-yr storm.

This report is intended to represent the fully developed Coit Center as it is planned at the date of this report. Development of this project should not adversely affect any adjacent or down stream properties.

CALCULATIONS SECTION



**FIRM MAP PANEL NO. 2986**  
 320020 2986E DATED 9-30-94

1"=52'  
 1995-10



**JEFF CODEGA**  
 PLANNING/DESIGN, INC.

planners

landscape architects

engineers

**Rainfall Depth - Duration - Frequency Data**  
 Source: City of Reno Public Works Manual IDF Curve From Cannon Airport

Project:  
 JCPD Job No.  
 Date: 13-Feb-97  
 Watershed name:  
 NOAA Atlas Reigon #: 2

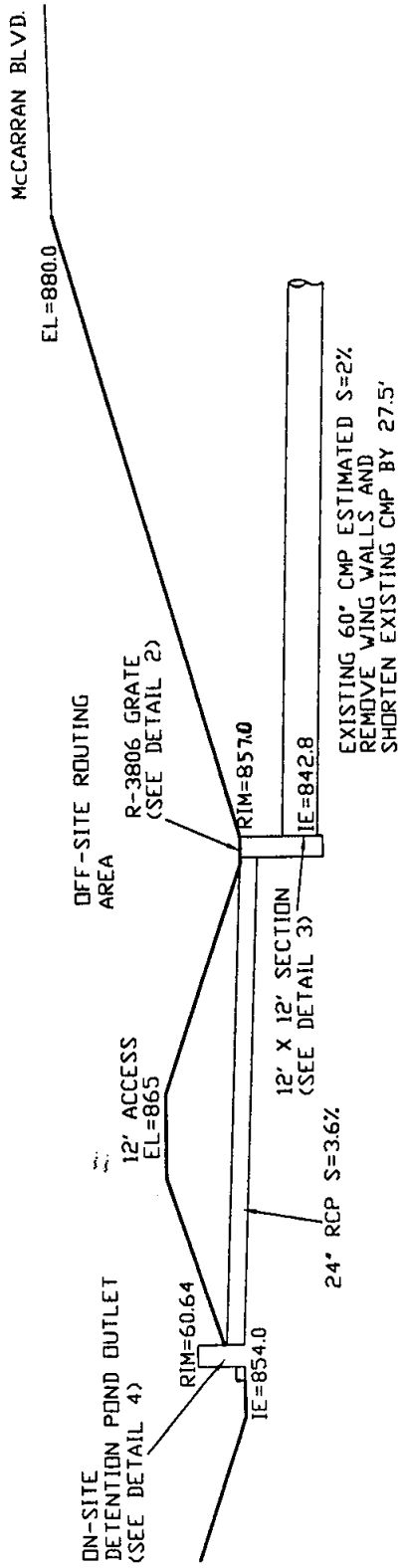
**IDF CURVE VALUES**

DEPTH (in)											
Return Period (Yr.)	5 min	10 min	15 min	30 min	1 hr	2 hr	3 hr	6 hr	12 hr	24 hr	
2	0.11	0.16	0.19	0.24	0.29	0.40	0.48	0.66	0.84	1.03	
5	0.18	0.23	0.28	0.34	0.40	0.52	0.60	0.78	1.02	1.42	
10	0.23	0.31	0.36	0.45	0.52	0.62	0.72	0.90	1.20	1.68	
25	0.33	0.42	0.50	0.59	0.70	0.80	0.87	1.08	1.56	2.14	
50	0.38	0.53	0.60	0.73	0.85	0.96	1.05	1.32	1.80	2.64	
100	0.48	0.63	0.73	0.90	1.08	1.20	1.32	1.62	2.16	2.88	

INTENSITY (in/hr)											
Return Period (Yr.)	5 min	10 min	15 min	30 min	60 min	120 min	180 min	360 min	720 min	1440 min	
2 yr	1.35	0.95	0.75	0.48	0.29	0.20	0.16	0.11	0.07	0.05	
5 yr	2.10	1.40	1.10	0.68	0.40	0.26	0.20	0.13	0.09	0.06	
10 yr	2.70	1.85	1.45	0.89	0.52	0.31	0.24	0.15	0.10	0.07	
25 yr	3.90	2.51	2.00	1.18	0.70	0.40	0.29	0.18	0.13	0.09	
50 yr	4.60	3.20	2.40	1.45	0.85	0.48	0.35	0.22	0.15	0.11	
100 yr	5.80	3.80	2.90	1.80	1.08	0.60	0.44	0.27	0.18	0.12	

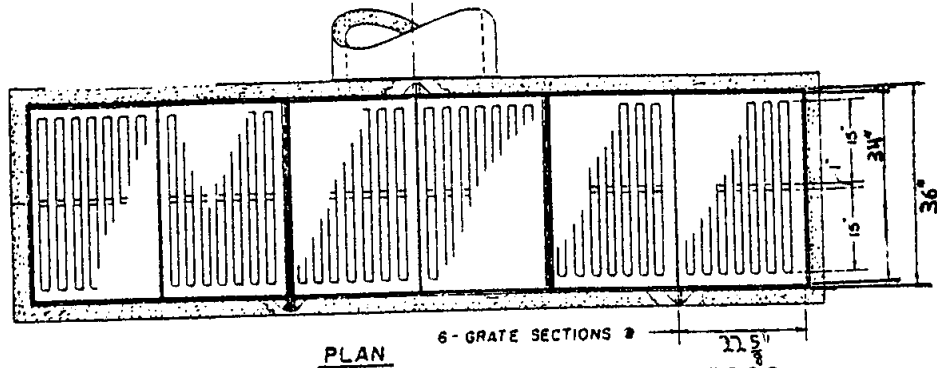


DETENTION AND ROUTING CROSS-SECTION  
DETAIL 1

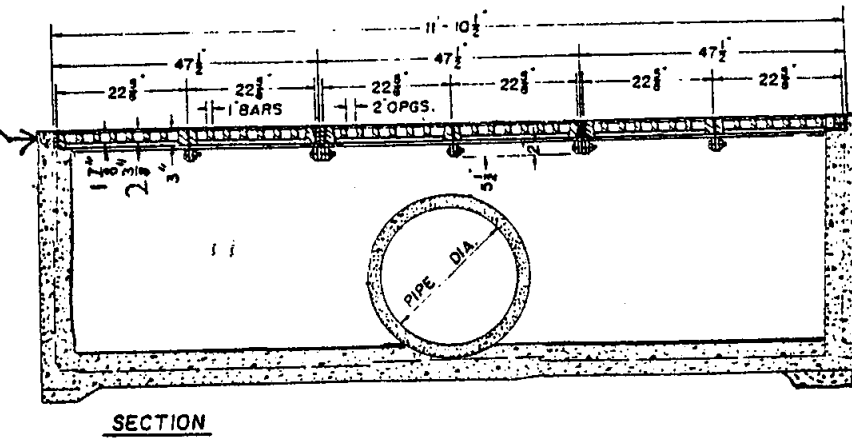
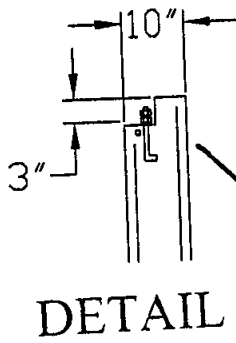


DETENTION AND ROUTING CROSS-SECTION

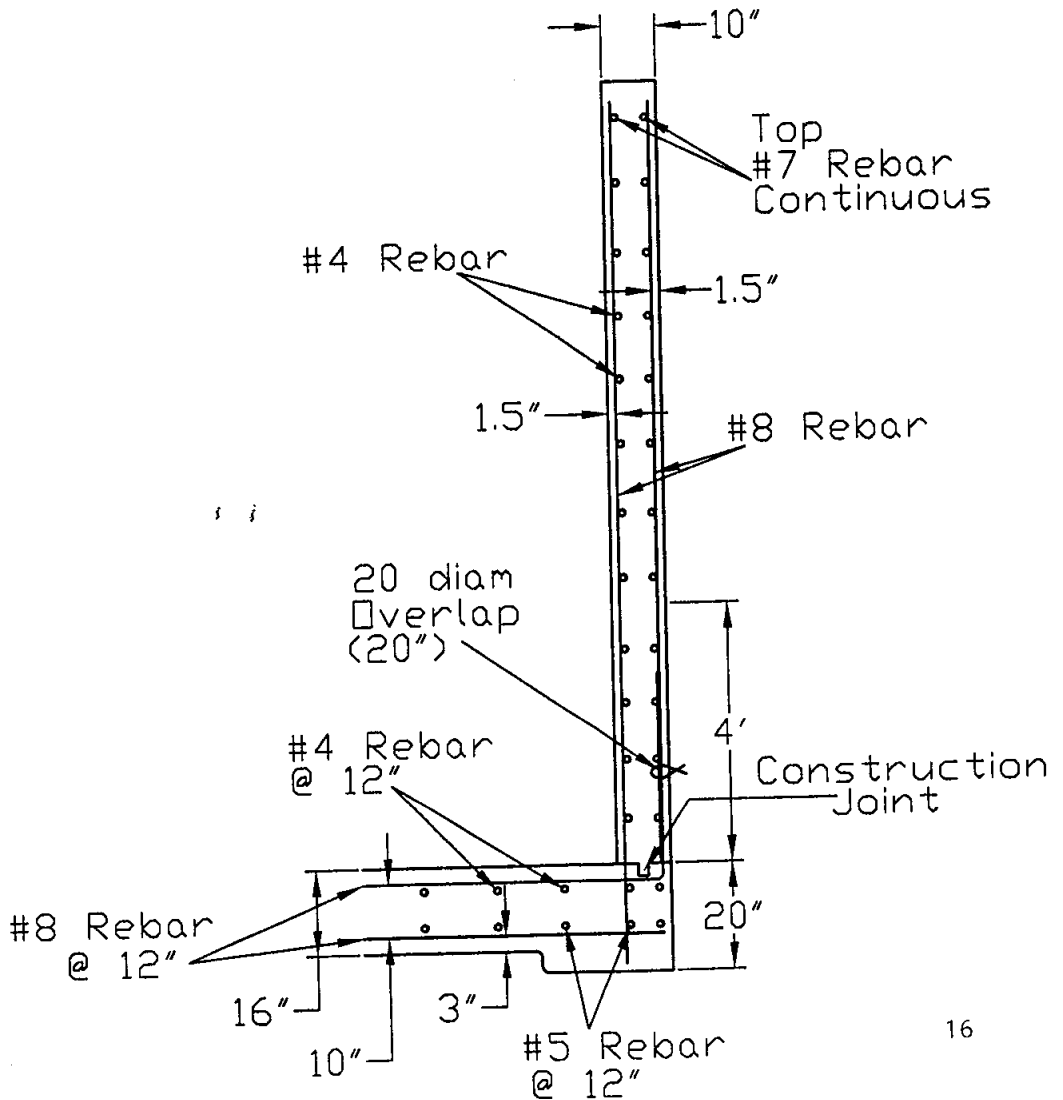
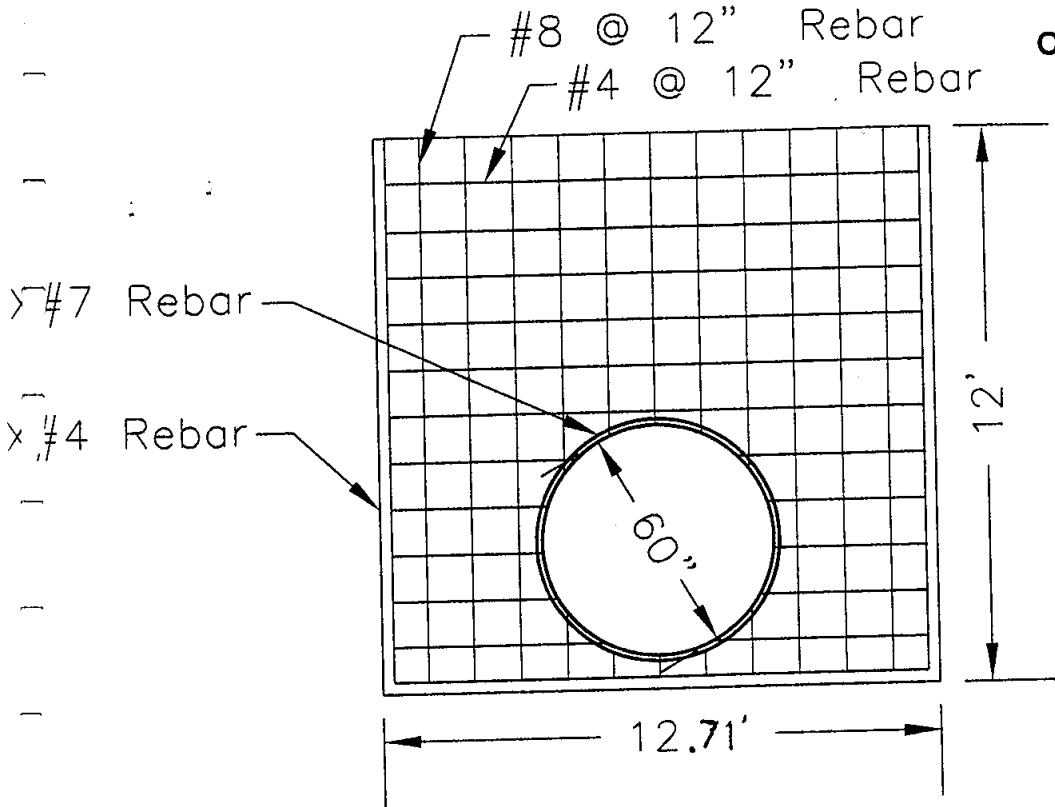
OFF-SITE OUTLET GRATE  
DETAIL 2



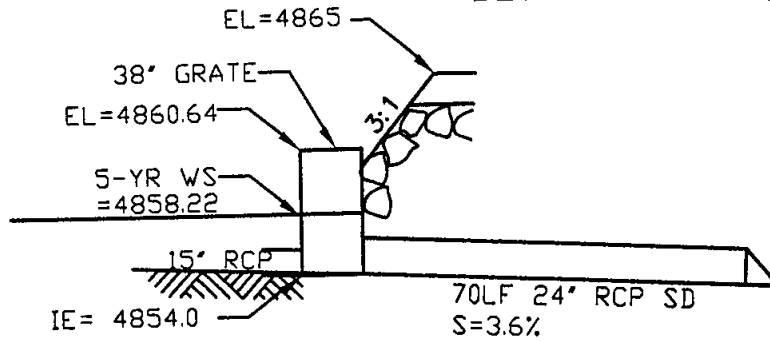
CAT. NO. R-3806  
MEDIAN SLOPE OR SIDE SLOPE  
AND DITCH CHECK DRAIN



OFF-SITE OUTLET  
DETAIL 3

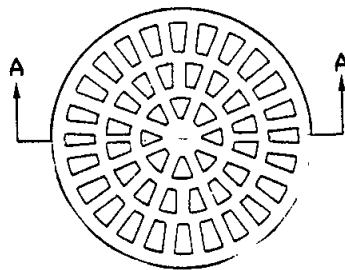


DETENTION POND (ON-SITE) OUTLET  
DETAIL 4



DETENTION POND OUTLET

NTS

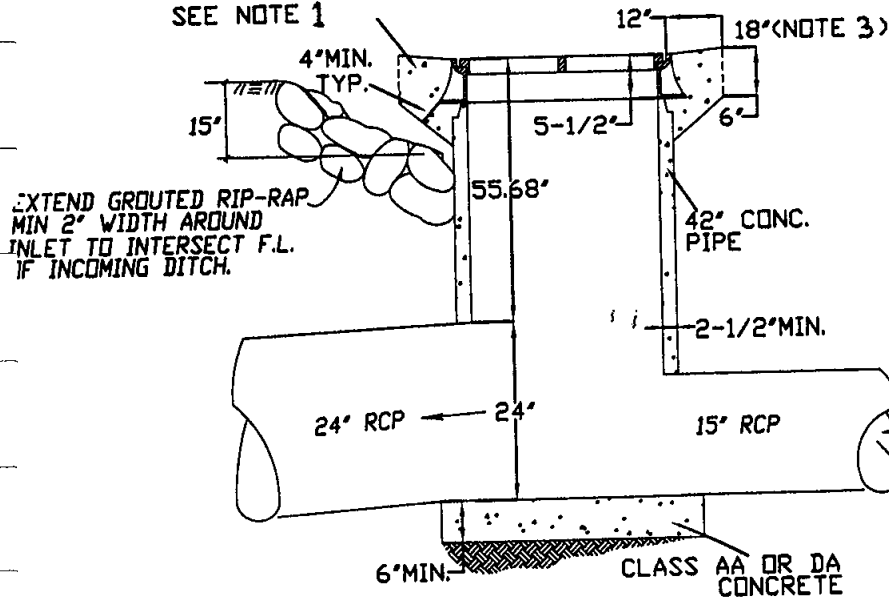


PLAN

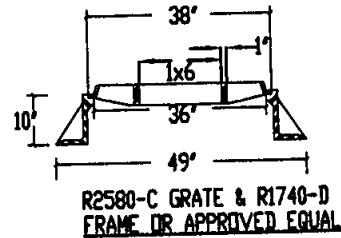
NOTES:

- 1.) RENO-FOR USE ONLY IN UNIMPROVED AREAS. A CONCRETE COLLAR SHALL BE CONSTRUCTED AS SHOWN.
- 2.) OUTLET PIPE TO BE MINIMUM SIZE AS SHOWN ON DWG.
- 3.) IN WASHOE CO. CONC. COLLAR SHALL BE 18" IN WIDTH AT ALL LOCATIONS.

SEE NOTE 1



SECTION A-A



R2580-C GRATE & R1740-D  
FRAME OR APPROVED EQUAL

DETENTION POND OUTLET (MODIFIED TYPE 3 DI)

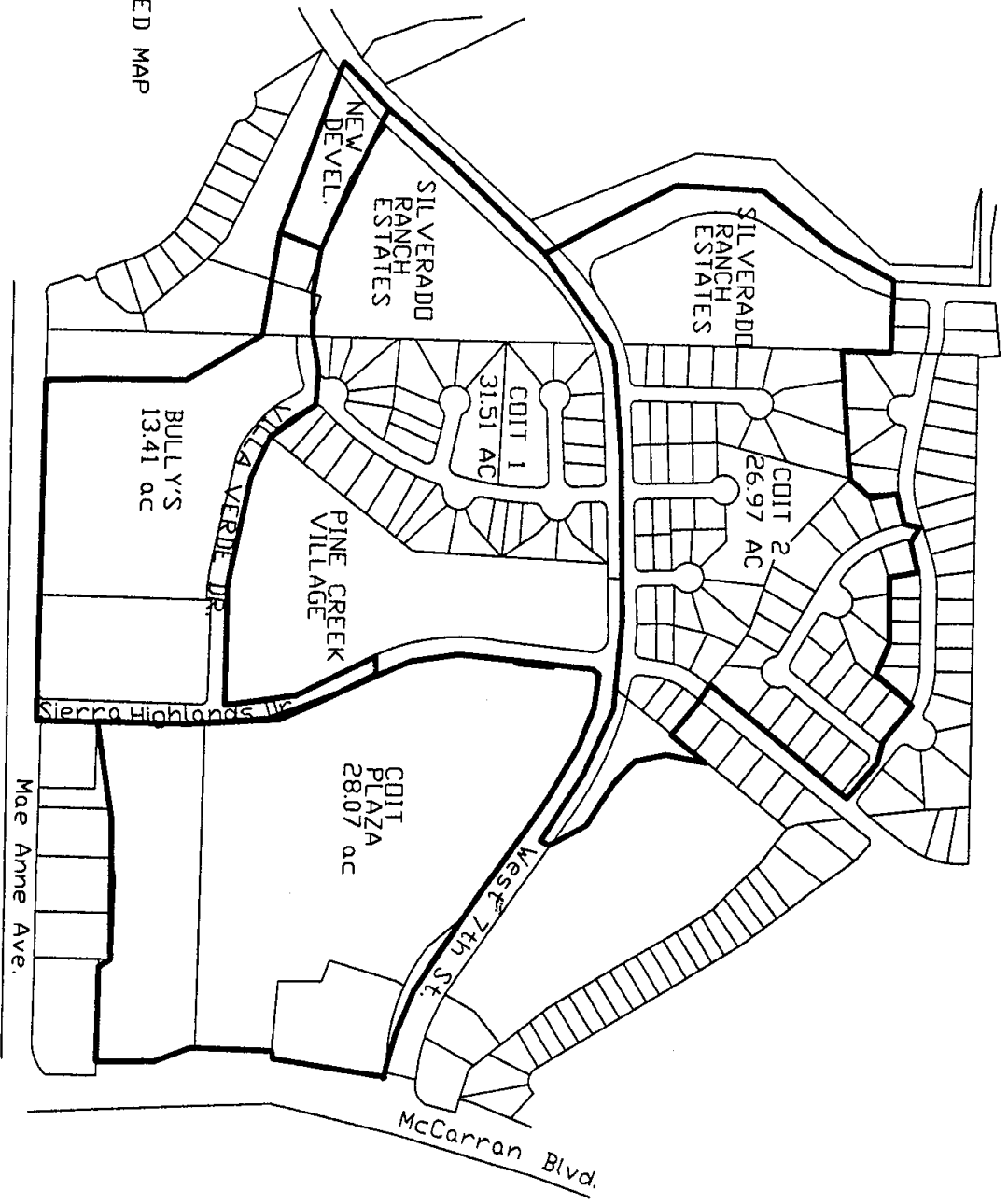
NTS

**OFF-SITE CALCULATIONS  
HEC-1 MODEL**



N.T.S.

FIGURE 4  
OFFSITE WATERSHED MAP  
AREAS USED IN  
HEC - 1 MODEL



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*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   MAY 1991 *
*   VERSION 4.0.1E *
*   Lahey F77L-EM/32 version 5.01 *
*   Dodson & Associates, Inc. *
* RUN DATE 02/14/97 TIME 10:35:51 *
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
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X  X  XXXXXXXX  XXXXX  X
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

*Byer*

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DIAGRAM
1  ID *****
2  ID      Jeff Codega Planning/Design
3  ID      433 West Plumb Lane
4  ID      Reno NV 89509
5  ID      (702) 322-5100 Fax (702) 322-1551
6  ID
7  ID
8  ID      Coit Center
9  ID
10 ID
11 ID      JCPD JOB 1317.07
12 ID
13 ID
14 ID
15 ID
16 ID      RAIN FALL DATA FROM NOAA ATLAS 2, VOLUME VII
17 ID      LAG TIME COMPUTED WITH THE UPLAND METHOD AND THE PROCEDURES DESCRIBED IN TR
18 ID      CURVE NUMBER FROM TR-55 AND NEH-4
19 ID      ROUTING PREFORMED WITH MODIFIDE PULS
20 ID
21 ID      ===== 005 YEAR, 24 HOUR EVENT =====
22 ID
23 ID
24 ID      =====
25 IT      1          1440
26 IO      3          0

27 KK SREU21 Silverado Ranch Estates Unit 2 Phase 1 Detention Basin Calculation
28 BA 0.1065
29 PH 20          .18   .28   .40   .52   .60   .78   1.02   1.42
30 LS          85
31 UD .1823

32 KK Silv08
33 KM Silverado Ranch Estates Detention Basin at Intersection of 7th and Britannia
34 KM Data from Summit Engineering Report for Silverado Ranch Estate Unit 2 Phase 1
35 RS 1  STOR      -1
36 SV 0  .2982  .5784  1.2810  2.0177  2.9420  3.8663  4.8843
37 SQ 0  0  2.3  4.5  6.0  7.0  8.0  9.0
38 SE 4970  4971  4972  4973  4974  4975  4976  4977

39 KK RipRap Watershed Contributing to Riprap Ditch from Silverado Estates U2 P1
40 BA .0848
41 PH 20          .18   .28   .40   .52   .60   .78   1.02   1.42
42 LS          85
43 UD .15

44 KK DB&RR Combine Hydrographs From Riprap Swale and Detention basin
45 HC 2
    
```



LINE	ID	1	2	3	4	5	6	7	8	9	10
46	KK RT C2	Route the outlet from D. Basin and RR Swale to outlet of Coit 2									
47	RK	2500	0.025	.014		CIRC	30	0	YES		
48	RM	1	.11	.35							
49	KK Coit 2	Watershed of Coit Heights Unit 2 and Area 15 from Silverado U2 P1									
50	BA	.04214									
51	PH	20		.18	.28	.40	.52	.60	.78	1.02	1.42
52	LS		87								
53	UD	.25									
54	KK Comb	Combine Routed Detention basin and Riprap swale with Coit Heights 2									
55	HC	2									
56	KK RTCOIT	Route the outlet from D. Basin and RR Swale to the Coit D. Basin									
57	RK	1000	0.04	.014		CIRC	48	0	YES		
58	RM	1	.11	.35							
59	KK Coit 1	Watershed of Coit Heights Unit 1, Sierra Highlands and Future Dev.									
60	BA	.04923									
61	PH	20		.18	.28	.40	.52	.60	.78	1.02	1.42
62	LS		87								
63	UD	.17									
64	KK RTCOIT	Route the outlet from D. Basin and RR Swale to the Coit D. Basin									
65	RK	1000	0.025	.014		CIRC	36	0	YES		
66	RM	1	.11	.35							
67	KK Bullys	Watershed Concentrating at Bullys Sports bar									
68	BA	.02094									
69	PH	20		.18	.28	.40	.52	.60	.78	1.02	1.42
70	LS		87								
71	UD	.17									
72	KK RTCOIT	Route the outlet from D. Basin and RR Swale to the Coit D. Basin									
73	RK	1000	0.025	.014		CIRC	36	0	YES		
74	RM	1	.11	.35							
75	KK CoitPl	Watershed of Coit Plaza									
76	BA	.04386									
77	PH	20		.18	.28	.40	.52	.60	.78	1.02	1.42
78	LS		87								
79	UD	.17									
80	KK Comb	Combine outlet of Routed Silverado Detention Basin with Coit D3									
81	HC	4									
82	KK Mccarrn										
83	KM	Reservoir routing at McCarran Blvd.									
84	KM	With 54 inch storm drain in place through Canyon Center									
85	RS	1	STOR	-1							
86	SV	0	.038	.272	.589	.939	1.324	1.745	2.204	2.702	3.240
87	SV	3.819	4.442	5.110	5.826	6.592	7.410	8.281			
88	SQ	0	5.1	18.3	37.8	61	79.3	94	106.6	118.1	123.4
89	SQ	137.9	146.9	155.3	163.3	170.9	178.2	185.2			



\*\*\*\*\*  
\*  
\* U.S. ARMY CORPS OF ENGINEERS  
\* HYDROLOGIC ENGINEERING CENTER  
\* 609 SECOND STREET  
\* DAVIS, CALIFORNIA 95616  
\* (916) 551-1748  
\*  
\*\*\*\*\*

\*\*\*\*\*  
Planning/Design  
Plumb Lane  
V 89509  
Fax (702) 322-1551

enter

JB 1317.07

FROM NOAA ATLAS 2, VOLUME VII  
) WITH THE UPLAND METHOD AND THE PROCEDURES DESCRIBED IN TR  
4 TR-55 AND NEH-4  
) WITH MODIFIDE PULS

=== 005 YEAR, 24 HOUR EVENT=====

\*\*\*\*\*  
BIT CONTROL  
CONTROL  
HYDROGRAPH PLOT SCALE

STEPS IN COMPUTATION INTERVAL  
STARTING DATE  
STARTING TIME  
NUMBER OF HYDROGRAPH ORDINATES  
STARTING DATE  
STARTING TIME  
MARK

2 HOURS  
8 HOURS

LES

LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FeET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

\*\*\*\*\*

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 \* \*  
 \* \*  
 \* \*  
 \*\*\*\*\*

27 KK \* SREU21 \* Silverado Ranch Estates Unit 2 Phase 1 Detention Basin Calculation

SUBBASIN RUNOFF DATA

28 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.11 SUBBASIN AREA

PRECIPITATION DATA

29 PH DEPTHS FOR 20-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.18	0.28	0.40	0.52	0.60	0.78	1.02	1.42	0.00	0.00	0.00	0.00

STORM AREA = 0.11

30 LS SCS LOSS RATE  
 STRTL 0.35 INITIAL ABSTRACTION  
 CRVNR 85.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

31 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.18 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH  
 57 END-OF-PERIOD ORDINATES

7.	22.	42.	67.	100.	139.	183.	221.	247.	263.
269.	268.	261.	246.	230.	211.	187.	160.	135.	115.
99.	86.	74.	66.	57.	50.	43.	37.	32.	28.
24.	21.	18.	16.	14.	12.	10.	9.	8.	7.
6.	5.	4.	4.	3.	3.	3.	2.	2.	2.
1.	1.	1.	1.	1.	0.	0.			

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HYDROGRAPH AT STATION SREU21

TOTAL RAINFALL = 1.36, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.37

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 23.98-HR

19.	12.20	(CFS)	3.	1.	1.	1.
		(INCHES)	0.241	0.364	0.364	0.364
		(AC-FT)	1.	2.	2.	2.

CUMULATIVE AREA = 0.11 SQ MI

\*\*\* \*\*

\*\*\*\*\*  
 \* \*  
 32 KK \* Silv08 \*  
 \* \*  
 \*\*\*\*\*

Silverado Ranch Estates Detention Basin at Intersection of 7th and Britannia  
 Data from Summit Engineering Report for Silverado Ranch Estate Unit 2 Phase 1

HYDROGRAPH ROUTING DATA

35 RS	STORAGE ROUTING								
	NSTPS	1	NUMBER OF SUBREACHES						
	ITYP		STOR TYPE OF INITIAL CONDITION						
	RSVVIC	-1.00	INITIAL CONDITION						
	X	0.00	WORKING R AND D COEFFICIENT						
36 SV	STORAGE	0.0	0.3	0.6	1.3	2.0	2.9	3.9	4.9
37 SQ	DISCHARGE	0.	0.	2.	5.	6.	7.	8.	9.
38 SE	ELEVATION	4970.00	4971.00	4972.00	4973.00	4974.00	4975.00	4976.00	4977.00

\*\*\* \*\*

HYDROGRAPH AT STATION Silv08

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	23.98-HR
3.	13.03	(CFS)	2.	1.	1.	1.
		(INCHES)	0.218	0.338	0.338	0.338
		(AC-FT)	1.	2.	2.	2.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	23.98-HR
1.	12.97		1.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	23.98-HR
4972.34	13.03		4972.10	4971.39	4971.39	4971.39

CUMULATIVE AREA = 0.11 SQ MI

\*\*\* \*\*

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 \* \* \*  
 39 KK \* RipRap \* Watershed Contributing to Riprap Ditch from Silverado Estates U2 P1  
 \* \* \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

40 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.08 SUBBASIN AREA

PRECIPITATION DATA

41 PH DEPTHS FOR 20-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.18	0.28	0.40	0.52	0.60	0.78	1.02	1.42	0.00	0.00	0.00	0.00

STORM AREA = 0.08

42 LS SCS LOSS RATE

STRTL	0.35	INITIAL ABSTRACTION
CRVNBR	85.00	CURVE NUMBER
RTIMP	0.00	PERCENT IMPERVIOUS AREA

43 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	0.15	LAG
------	------	-----

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VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH  
 47 END-OF-PERIOD ORDINATES

9.	28.	54.	89.	135.	184.	223.	248.	258.	258.
248.	230.	209.	183.	152.	123.	103.	86.	73.	65.
53.	45.	37.	32.	26.	22.	19.	16.	13.	11.
9.	8.	7.	6.	5.	4.	3.	3.	3.	2.
2.	2.	1.	1.	1.	0.	0.			

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HYDROGRAPH AT STATION § RipRap

TOTAL RAINFALL = 1.36, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.37

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
17.	12.17	(CFS) 2.	1.	1.	1.
		(INCHES) 0.241	0.364	0.364	0.364
		(AC-FT) 1.	2.	2.	2.

CUMULATIVE AREA = 0.08 SQ MI

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*****
*           *
44 KX      *   DB&RR *   Combine Hydrographs From Riprap Swale and Detention basin
*           *
*****

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45 HC      HYDROGRAPH COMBINATION
          ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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***
***
***
***
HYDROGRAPH AT STATION DB&RR
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)
19.            12.17
(CFS)          6-HR      24-HR      72-HR      23.98-HR
                5.        2.         2.         2.
(INCHES)       0.226     0.350     0.350     0.350
(AC-FT)        2.         4.         4.         4.
CUMULATIVE AREA = 0.19 SQ MI

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*****
*           *
46 KK      *   RT C2 *   Route the outlet from D. Basin and RR Swale to outlet of Coit 2
*           *
*****

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HYDROGRAPH ROUTING DATA

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48 RM      MUSKINGUM ROUTING
          NSTPS      1 NUMBER OF SUBREACHES
          AMSKK      0.11 MUSKINGUM K
          X          0.35 MUSKINGUM X

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***** WARNING ***** POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RT C2.
REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

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***
***
***
***
HYDROGRAPH AT STATION RT C2
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)
17.            12.27
(CFS)          6-HR      24-HR      72-HR      23.98-HR
                5.        2.         2.         2.
(INCHES)       0.226     0.348     0.348     0.348
(AC-FT)        2.         4.         4.         4.
CUMULATIVE AREA = 0.19 SQ MI

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\* \*  
\* \*  
\* \*  
\*\*\*\*\*

49 KK \* Coit 2 \* Watershed of Coit Heights Unit 2 and Area 15 from Silverado U2 P1

SUBBASIN RUNOFF DATA

50 BA SUBBASIN CHARACTERISTICS  
TAREA 0.04 SUBBASIN AREA

PRECIPITATION DATA

51 PH DEPTHS FOR 20-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.18	0.28	0.40	0.52	0.60	0.78	1.02	1.42	0.00	0.00	0.00	0.00

STORM AREA = 0.04

52 LS SCS LOSS RATE  
STRTL 0.30 INITIAL ABSTRACTION  
CRVNER 97.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVICUS AREA

53 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.25 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH  
77 END-OF-PERIOD ORDINATES

2.	4.	8.	12.	17.	23.	31.	39.	49.	58.
65.	71.	75.	78.	79.	79.	78.	75.	72.	68.
64.	60.	55.	49.	43.	38.	34.	30.	27.	25.
22.	20.	18.	16.	15.	13.	12.	11.	10.	9.
8.	7.	6.	6.	5.	5.	4.	4.	3.	3.
3.	2.	2.	2.	2.	2.	1.	1.	1.	1.
1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.		

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HYDROGRAPH AT STATION Coit 2

TOTAL RAINFALL = 1.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 0.44

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
8.	12.27	(CFS) 1.	0.	0.	0.
		(INCHES) 0.291	0.437	0.437	0.437
		(AC-FT) 1.	1.	1.	1.



CUMULATIVE AREA = 0.04 SQ MI

\*\*\*\*\*

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*****
*                               *
54 KK *   Comb   *   Combine Routed Detention basin and Riprap swale with Coit Heights 2
*                               *
*****

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55 HC   HYDROGRAPH COMBINATION
        ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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\*\*\*

HYDROGRAPH AT STATION Comb

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
25.	12.27	(CFS) 6.	2.	2.	2.
		(INCHES) 0.237	0.364	0.364	0.364
		(AC-FT) 3.	5.	5.	5.

CUMULATIVE AREA = 0.23 SQ MI

\*\*\*\*\*

```

*****
*                               *
56 KK *   RTCOIT *   Route the outlet from O. Basin and RR Swale to the Coit O. Basin
*                               *
*****

```

HYDROGRAPH ROUTING DATA

```

58 RM   MUSKINGUM ROUTING
        NSTPS      1 NUMBER OF SUBREACHES
        AMSKK     0.11 MUSKINGUM K
        X         0.35 MUSKINGUM X

```

\*\*\*

\*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RTCOIT.  
 REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

\*\*\*

HYDROGRAPH AT STATION RTCOIT

PEAK FLOW      TIME                      MAXIMUM AVERAGE FLOW

(CFS)	(HR)		6-HR	24-HR	72-HR	23.98-HR
23.	12.37	(CFS)	6.	2.	2.	2.
		(INCHES)	0.237	0.362	0.362	0.362
		(AC-FT)	3.	5.	5.	5.

CUMULATIVE AREA = 0.23 SQ MI

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\*\*\*\*\*  
 \* \*  
 59 KK \* Coit 1 \* Watershed of Coit Heights Unit 1, Sierra Highlands and Future Dev.  
 \* \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

60 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.05 SUBBASIN AREA

PRECIPITATION DATA

61 PH DEPTHS FOR 20-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	.....	.....	TP-40	.....	.....	TP-49	.....	.....	.....	.....
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.18	0.28	0.40	0.52	0.60	0.78	1.02	1.42	0.00	0.30	0.30	0.30

STORM AREA = 0.05

62 LS SCS LOSS RATE  
 STRTL 0.30 INITIAL ABSTRACTION  
 CRVNBR 87.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

63 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.17 LAG

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 ; 0.01667 24.00000

UNIT HYDROGRAPH  
 53 END-OF-PERIOD ORDINATES

4.	12.	23.	37.	56.	78.	100.	116.	127.	133.
133.	130.	123.	114.	104.	91.	77.	64.	54.	46.
40.	35.	30.	26.	22.	19.	16.	14.	12.	10.
9.	7.	6.	6.	5.	4.	4.	3.	3.	2.
2.	2.	1.	1.	1.	1.	1.	1.	1.	0.
0.	0.	0.							

\*\*\*                      \*\*\*                      \*\*\*                      \*\*\*                      \*\*\*

HYDROGRAPH AT STATION Coit 1

TOTAL RAINFALL = 1.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 0.44

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
12.	12.18	(CFS) 2.	1.	1.	1.
		(INCHES) 0.291	0.438	0.438	0.438
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.05 SQ MI

\*\*\*\*\*

```

*****
*                               *
64 KK *   RTCOIT *   Route the outlet from D. Basin and RR Swale to the Coit D. Basin
*                               *
*****

```

HYDROGRAPH ROUTING DATA

```

66 RM      MUSKINGUM ROUTING
          NSTPS      1 NUMBER OF SUBREACHES
          AMSKK     0.11 MUSKINGUM K
          X         0.35 MUSKINGUM X

```

\*\*\*

\*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RTCOIT.  
REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION RTCOIT

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
11.	12.28	(CFS) 2.	1.	1.	1.
		(INCHES) 0.291	0.436	0.436	0.436
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.05 SQ MI

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*****
*                               *
67 KK *   Bullys *   Watershed Concentrating at Bullys Sports bar
*                               *
*****

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SUBBASIN RUNOFF DATA

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68 3A      SUBBASIN CHARACTERISTICS
          TAREA     J.02 SUBBASIN AREA

```

PRECIPITATION DATA

69 PH

DEPTHS FOR 20-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.18	0.28	0.40	0.52	0.60	0.78	1.02	1.42	0.00	0.00	0.00	0.00

STORM AREA = 0.02

70 LS

SCS LOSS RATE

STRTL 0.30 INITIAL ABSTRACTION  
 CRVNB 87.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

71 UD

SCS DIMENSIONLESS UNITGRAPH

TLAG 0.17 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH

53 END-OF-PERIOD ORDINATES

2.	5.	10.	16.	24.	33.	42.	50.	54.	56.
57.	55.	52.	48.	44.	39.	33.	27.	23.	20.
17.	15.	13.	11.	9.	8.	7.	6.	5.	4.
4.	3.	3.	2.	2.	2.	2.	1.	1.	1.
1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
0.	0.	0.							

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HYDROGRAPH AT STATION Bullys

TOTAL RAINFALL = 1.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 0.44

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
5.	12.18	(CFS) 1.	0.	0.	0.
		(INCHES) 0.291	0.438	0.438	0.438
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.02 SQ MI

1  
3

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\*\*\*\*\*

72 KK

\* RTCOIT \* Route the outlet from D. Basin and RR Swale to the Coit D. Basin  
 \* \*  
 \*\*\*\*\*

HYDROGRAPH ROUTING DATA

74 RM

MUSKINGUM ROUTING

NSTPS 1 NUMBER OF SUBREACHES

AMSKX 0.11 MUSKINGUM X  
X 0.35 MUSKINGUM X

\*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RTCOIT.  
REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

HYDROGRAPH AT STATION RTCOIT

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
4.	12.28	(CFS) 1.	0.	0.	0.
		(INCHES) 0.291	0.436	0.436	0.436
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.02 SQ MI

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\* \* \* \* \*  
75 KK \* CoitPl \* Watershed of Coit Plaza  
\* \* \* \* \*  
\*\*\*\*\*

SUBBASIN RUNOFF DATA

76 BA SUBBASIN CHARACTERISTICS  
TAREA 0.04 SUBBASIN AREA

PRECIPITATION DATA

77 PH DEPTHS FOR 20-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.18	0.28	0.40	0.52	0.60	0.78	1.02	1.42	0.00	0.00	0.00	0.00

STORM AREA = 0.04

78 LS SCS LOSS RATE  
STRTL 0.30 INITIAL ABSTRACTION  
CRVNBR 87.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

79 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.17 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH

53 END-OF-PERIOD ORDINATES

3. 11. 20. 33. 50. 70. 89. 104. 113. 118.

119.	116.	109.	101.	92.	81.	68.	57.	48.	41.
36.	31.	27.	23.	20.	17.	15.	12.	11.	9.
8.	7.	6.	5.	4.	4.	3.	3.	2.	2.
2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
0.	0.	0.							

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION CoitPl

TOTAL RAINFALL = 1.36, TOTAL LOSS = 0.92, TOTAL EXCESS = 0.44

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
10.	12.18	(CFS) 1.	1.	1.	1.
		(INCHES) 0.291	0.438	0.438	0.438
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = 0.04 SQ MI

\*\*\*\*\*

30 KK

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\*                    \*  
\*                    \*  
\*                    \*  
\*                    \*  
\*\*\*\*\*

Combine outlet of Routed Silverado Detention Basin with Coit DB

81 HC

HYDROGRAPH COMBINATION

ICOMP                    4 NUMBER OF HYDROGRAPHS TO COMBINE

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\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION Comb

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
42.	12.30	(CFS) 9.	4.	4.	4.
		(INCHES) 0.253	0.387	0.387	0.387
		(AC-FT) 5.	7.	7.	7.

CUMULATIVE AREA = 0.35 SQ MI

\*\*\*\*\*

32 KK

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\*                    \*  
\*                    \*  
\*                    \*  
\*                    \*  
\*\*\*\*\*

Mccarn

Reservoir routing at McCarran Blvd.  
With 54 inch storm drain in place through Canyon Center

HYDROGRAPH ROUTING DATA

85 RS	STORAGE ROUTING										
	NSTPS	1 NUMBER OF SUBREACHES									
	ITYP	STOR TYPE OF INITIAL CONDITION									
	RSVVIC	-1.00 INITIAL CONDITION									
	X	0.00 WORKING R AND D COEFFICIENT									
86 SV	STORAGE	0.0	0.0	0.3	0.6	0.9	1.3	1.7	2.2	2.7	3.2
		3.8	4.4	5.1	5.8	6.6	7.4	8.3			
88 SQ	DISCHARGE	0.	5.	18.	38.	61.	79.	94.	107.	118.	128.
		138.	147.	155.	163.	171.	178.	185.			
90 SE	ELEVATION	48.40	49.40	50.40	51.40	52.40	53.40	54.40	55.40	56.40	57.40
		58.40	59.40	60.40	61.40	62.40	63.40	64.40			

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HYDROGRAPH AT STATION McCarrn

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	23.98-HR
31.	12.47	(CFS) 9.	4.	4.	4.
		(INCHES) 0.253	0.385	0.385	0.385
		(AC-FT) 5.	7.	7.	7.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	23.98-HR
0.	12.45	0.	0.	0.	0.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	23.98-HR
51.06	12.47	49.71	48.97	48.97	48.97

CUMULATIVE AREA = 0.35 SQ MI

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	SREU21	19.	12.20	3.	1.	1.	0.11		
ROUTED TO	SilvOB	3.	13.03	2.	1.	1.	0.11	4972.34	13.03
HYDROGRAPH AT	RipRap	17.	12.17	2.	1.	1.	0.08		
2 COMBINED AT	DB&RR	19.	12.17	5.	2.	2.	0.19		
ROUTED TO	RT C2	17.	12.27	5.	2.	2.	0.19		
HYDROGRAPH AT	Coit 2 C	8.	12.27	1.	0.	0.	0.04		
2 COMBINED AT	Comb (R. 2)	25.	12.27	6.	2.	2.	0.23		
ROUTED TO	RTCOIT	23.	12.37	6.	2.	2.	0.23		
HYDROGRAPH AT	Coit 1 (R. 2) 213)	12.	12.18	2.	1.	1.	0.05		
ROUTED TO	RTCOIT	11.	12.28	2.	1.	1.	0.05		
HYDROGRAPH AT	Bullys (R. 2)	5.	12.18	1.	0.	0.	0.02		
ROUTED TO	RTCOIT	4.	12.28	1.	0.	0.	0.02		
HYDROGRAPH AT	Coit PL	10.	12.18	1.	1.	1.	0.04		
4 COMBINED AT	Comb	42.	12.30	9.	4.	4.	0.35		
ROUTED TO	Mccarn	31.	12.47	9.	4.	4.	0.35	51.06	12.47

\*\*\* NORMAL END OF HEC-1 \*\*\*



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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
* Lahey F77L-EM/32 version 5.01
* Dodson & Associates, Inc.
* RUN DATE 02/14/97 TIME 10:28:47
*
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
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X X X X X
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X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTICR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

100 YR

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

*DIAGRAM
1         ID *****
2         ID      Jeff Codega Planning/Design
3         ID      433 West Plumb Lane
4         ID      Reno NV 89509
5         ID      (702) 322-5100 Fax (702) 322-1551
6         ID
7         ID
8         ID      Coit Center
9         ID
10        ID
11        ID      JCPD JOB 1317.07
12        ID
13        ID
14        ID
15        ID
16        ID      RAIN FALL DATA FROM NOAA ATLAS 2, VOLUME VII
17        ID      LAG TIME COMPUTED WITH THE UPLAND METHOD AND THE PROCEDURES DESCRIBED IN TR
18        ID      CURVE NUMBER FROM TR-55 AND NEH-4
19        ID      ROUTING PREFORMED WITH MODIFIDE PULS
20        ID
21        ID      ===== 100 YEAR, 24 HOUR EVENT =====
22        ID
23        ID
24        ID      =====
25        IT      1          1440
26        IO      3          0

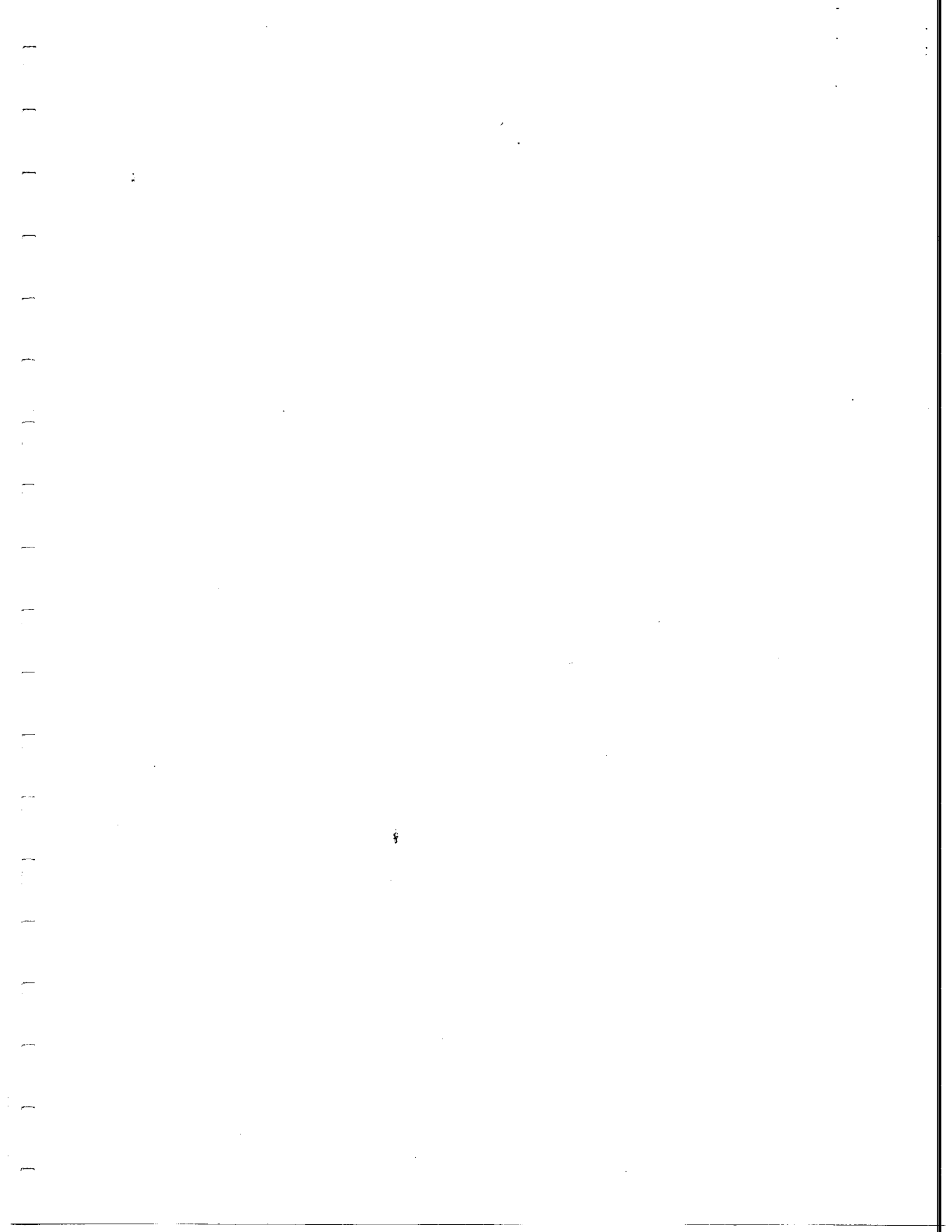
27        KK SREU21 Silverado Ranch Estates Unit 2 Phase 1 Detention Basin Calculation
28        BA 0.1065
29        PH      1          .48      .73      1.08      1.2      1.32      1.62      2.16      2.88
30        LS      85
31        UD      .1823

32        KK Silv08
33        KM Silverado Ranch Estates Detention Basin at Intersection of 7th and Brittania
34        KM Data from Summit Engineering Report for Silverado Ranch Estate Unit 2 Phase 1
35        RS      1      STOR      -1
36        SV      0      .2982      .5784      1.2810      2.0177      2.9420      3.8663      4.8843
37        SQ      0      0      2.3      4.5      6.0      7.0      8.0      9.0
38        SE      4970      4971      4972      4973      4974      4975      4976      4977

39        KK RipRap Watershed Contributing to Riprap Ditch from Silverado Estates U2 P1
40        BA .0848
41        PH      1          .48      .73      1.08      1.2      1.32      1.62      2.16      2.88
42        LS      85
43        UD      .15

44        KK OB&RR Combine Hydrographs From Riprap Swale and Detention basin
45        HC      2
    
```

LINE	ID	1	2	3	4	5	6	7	8	9	10
46	KK RT C2	Route the outlet from D. Basin and RR Swale to outlet of Coit 2									
47	RK	2500	0.025	.014		CIRC	30	0	YES		
48	RM	1	.11	.35							
49	KK Coit 2	Watershed of Coit Heights Unit 2 and Area 15 from Silverado U2 P1									
50	BA	.04214									
51	PH	1		.48	.73	1.08	1.2	1.32	1.62	2.16	2.88
52	LS		87								
53	UD	.25									
54	KK Comb	Combine Routed Detention basin and Riprap swale with Coit Heights 2									
55	HC	2									
56	KK RTCOIT	Route the outlet from D. Basin and RR Swale to the Coit D. Basin									
57	RK	1000	0.04	.014		CIRC	48	0	YES		
58	RM	1	.11	.35							
59	KK Coit 1	Watershed of Coit Heights Unit 1, Sierra Highlands and Future Dev.									
60	BA	.04923									
61	PH	1		.48	.73	1.08	1.2	1.32	1.62	2.16	2.88
62	LS		87								
63	UD	.17									
64	KK RTCOIT	Route the outlet from D. Basin and RR Swale to the Coit D. Basin									
65	RK	1000	0.025	.014		CIRC	36	0	YES		
66	RM	1	.11	.35							
67	KK Bullys	Watershed Concentrating at Bullys Sports bar									
68	BA	.02094									
69	PH	1		.48	.73	1.08	1.2	1.32	1.62	2.16	2.88
70	LS		87								
71	UD	.17									
72	KK RTCOIT	Route the outlet from D. Basin and RR Swale to the Coit D. Basin									
73	RK	1000	0.025	.014		CIRC	36	0	YES		
74	RM	1	.11	.35							
75	KK CoitPl	Watershed of Coit Plaza									
76	BA	.04386									
77	PH	1		.48	.73	1.08	1.2	1.32	1.62	2.16	2.88
78	LS		87								
79	UD	.17									
80	KK Comb	Combine outlet of Routed Silverado Detention Basin with Coit DB									
81	HC	4									
82	KK McCarrn										
83	KM	Reservoir routing at McCarran Blvd.									
84	KM	With 54 inch storm drain in place through Canyon Center									
85	RS	;	STOR	-;							
86	SV	0	.038	.272	.589	.939	1.324	1.745	2.204	2.702	3.240
87	SV	3.819	4.442	5.110	5.826	6.592	7.410	8.281			
88	SQ	0	5.1	18.3	37.8	61	79.3	94	106.6	118.1	128.4
89	SQ	137.9	146.9	155.3	163.3	170.9	178.2	185.2			



1 NETWORK

ERSION OR PUMP FLOW

IRN OF DIVERTED OR PUMPED FLOW

.....3.....9.....10

4. 55.4 56.4 57.4

4.

f  
CoitPl  
:  
:  
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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   MAY 1991
*   VERSION 4.0.1E
*   Lahey F77L-EM/32 version 5.01
*   : Dodson & Associates, Inc.
* RUN DATE 02/14/97 TIME 10:28:47
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*****

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\*\*\*\*\*

Jeff Codega Planning/Design  
433 West Plumb Lane  
Reno NV 89509  
(702) 322-5100 Fax (702) 322-1551

Coit Center

JCPD JOB 1317.07

RAIN FALL DATA FROM NOAA ATLAS 2, VOLUME VII  
LAG TIME COMPUTED WITH THE UPLAND METHOD AND THE PROCEDURES DESCRIBED IN TR  
CURVE NUMBER FROM TR-55 AND NEH-4  
ROUTING PREFORMED WITH MODIFIDE PULS

===== 100 YEAR, 24 HOUR EVENT=====

=====

26 IO

OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE

IT

HYDROGRAPH TIME DATA

NMIN 1 MINUTES IN COMPUTATION INTERVAL  
IDATE 1 0 STARTING DATE  
ITIME 0000 STARTING TIME  
NO 1440 NUMBER OF HYDROGRAPH ORDINATES  
NDDATE 1 0 ENDING DATE  
NDTIME 2359 ENDING TIME  
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.02 HOURS  
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
PRECIPITATION DEPTH INCHES

LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FeET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

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 \* \*  
 \* \*  
 \* \*  
 \*\*\*\*\*

27 KK \* SREU21 \* Silverado Ranch Estates Unit 2 Phase 1 Detention Basin Calculation

SUBBASIN RUNOFF DATA

28 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.11 SUBBASIN AREA

PRECIPITATION DATA

29 PH DEPTHS FOR 1-PERCENT HYPOTHETICAL STORM  
 ..... HYDRO-35 ..... TP-40 ..... TP-49 .....  
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY  
 0.48 0.73 1.08 1.20 1.32 1.62 2.16 2.88 0.00 0.00 0.00 0.00

STORM AREA = 0.11

30 LS SCS LOSS RATE  
 STRTL 0.35 INITIAL ABSTRACTION  
 CRVNBR 85.00 CURVE NUMBER  
 RTIMP 0.30 PERCENT IMPERVIOUS AREA

31 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.18 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH											
57 END-OF-PERIOD ORDINATES											
7.	22.	42.	67.	100.	139.	183.	221.	247.	263.		
269.	268.	261.	246.	230.	211.	187.	160.	135.	115.		
99.	86.	74.	66.	57.	50.	43.	37.	32.	28.		
24.	21.	18.	16.	14.	12.	10.	9.	8.	7.		
6.	5.	4.	4.	3.	3.	3.	2.	2.	2.		
1.	1.	1.	1.	1.	0.	0.					

\*\*\* \*\*

HYDROGRAPH AT STATION SREU21

TOTAL RAINFALL = 2.88, TOTAL LOSS = 1.39, TOTAL EXCESS = 1.49

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 (CFS) (HR) 6-HR 24-HR 72-HR 23.98-HR

111.	12.18	(CFS)	12.	4.	4.	4.
		(INCHES)	1.333	1.477	1.477	1.477
		(AC-FT)	6.	8.	8.	8.

CUMULATIVE AREA = 0.11 SQ MI

\*\*\* \*\*

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*****
*      *
32 KK *  silv08 *
*      *
*****

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Silverado Ranch Estates Detention Basin at Intersection of 7th and Britannia  
Data from Summit Engineering Report for Silverado Ranch Estate Unit 2 Phase 1

HYDROGRAPH ROUTING DATA

35 RS	STORAGE ROUTING								
	NSTPS	1	NUMBER OF SUBREACHES						
	ITYP		STOR TYPE OF INITIAL CONDITION						
	RSVRC	-1.00	INITIAL CONDITION						
	X	0.00	WORKING R AND D COEFFICIENT						
36 SV	STORAGE	0.0	0.3	0.6	1.3	2.0	2.9	3.9	4.9
37 SQ	DISCHARGE	0.	0.	2.	5.	6.	7.	8.	9.
38 SE	ELEVATION	4970.00	4971.00	4972.00	4973.00	4974.00	4975.00	4976.00	4977.00

\*\*\* \*\*

HYDROGRAPH AT STATION silv08

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	23.98-HR
8.	12.85	(CFS)	7.	4.	4.	4.
		(INCHES)	0.651	1.258	1.258	1.258
		(AC-FT)	4.	7.	7.	7.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	23.98-HR
4.	12.85		3.	2.	2.	2.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	23.98-HR
4975.95	12.88		4975.45	4972.99	4972.99	4972.99

CUMULATIVE AREA = 0.11 SQ MI

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 \* \* \*  
 39 KK \* RipRap \* Watershed Contributing to Riprap Ditch from Silverado Estates U2 P1  
 \* \* \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

40 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.08 SUBBASIN AREA

PRECIPITATION DATA

41 PH DEPTHS FOR 1-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.48	0.73	1.08	1.20	1.32	1.62	2.16	2.38	0.00	0.00	0.00	0.00

STORM AREA = 0.08

42 LS SCS LOSS RATE

STRTL	0.35	INITIAL ABSTRACTION
CRVNBR	85.00	CURVE NUMBER
RTIMP	0.00	PERCENT IMPERVIOUS AREA

43 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	0.15	LAG
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VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH  
 47 END-OF-PERIOD ORDINATES

9.	28.	54.	89.	135.	184.	223.	248.	258.	258.
248.	230.	209.	183.	152.	123.	103.	86.	73.	63.
53.	45.	37.	32.	26.	22.	19.	16.	13.	11.
9.	8.	7.	6.	5.	4.	3.	3.	3.	2.
2.	2.	1.	1.	1.	0.	0.			

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HYDROGRAPH AT STATION RipRap

TOTAL RAINFALL = 2.88, TOTAL LOSS = 1.39, TOTAL EXCESS = 1.49

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
100.	12.15	(CFS) 9.	3.	3.	3.
		(INCHES) 1.033	1.479	1.479	1.479
		(AC-FT) 5.	7.	7.	7.

CUMULATIVE AREA = 0.08 SQ MI

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\*\*\*\*\*  
 \* \*  
 44 XK \* DB&RR \* Combine Hydrographs From Riprap Swale and Detention basin  
 \* \*  
 \*\*\*\*\*

45 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*  
 \*\*\*  
 \*\*\*  
 \*\*\*  
 \*\*\*

HYDROGRAPH AT STATION DB&RR

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
105.	12.15	(CFS) 17.	7.	7.	7.
		(INCHES) 0.805	1.356	1.356	1.356
		(AC-FT) 8.	14.	14.	14.

CUMULATIVE AREA = 0.19 SQ MI

\*\*\*\*\*

\*\*\*\*\*  
 \* \*  
 46 XK \* RT C2 \* Route the outlet from D. Basin and RR Swale to outlet of Coit 2  
 \* \*  
 \*\*\*\*\*

HYDROGRAPH ROUTING DATA

48 RM MUSKINGUM ROUTING  
 NSTPS 1 NUMBER OF SUBREACHES  
 AMSKK 0.11 MUSKINGUM K  
 X 0.35 MUSKINGUM X

\*\*\*\*\*  
 \*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RT C2.  
 REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).  
 \*\*\*\*\*

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HYDROGRAPH AT STATION RT C2

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
94.	12.25	(CFS) 17.	7.	7.	7.
		(INCHES) 0.805	1.349	1.349	1.349
		(AC-FT) 8.	14.	14.	14.

CUMULATIVE AREA = 0.19 SQ MI

\*\*\*\*\*

\*\*\*\*\*  
 \* \*  
 49 KK \* Coit 2 \* Watershed of Coit Heights Unit 2 and Area 15 from Silverado U2 P1  
 \* \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

50 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.04 SUBBASIN AREA

PRECIPITATION DATA

51 PH DEPTHS FOR 1-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.48	0.73	1.08	1.20	1.32	1.62	2.16	2.88	0.00	0.00	0.00	0.00

STORM AREA = 0.04

52 LS SCS LOSS RATE

STRTL	0.30	INITIAL ABSTRACTION
CRVNBR	87.00	CURVE NUMBER
RTIMP	0.00	PERCENT IMPERVIOUS AREA

53 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	0.25	LAG
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VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH  
 77 END-OF-PERIOD ORDINATES

2.	4.	8.	12.	17.	23.	31.	39.	49.	58.
65.	71.	75.	78.	79.	79.	78.	75.	72.	68.
64.	60.	55.	49.	43.	38.	34.	30.	27.	25.
22.	20.	18.	16.	15.	13.	12.	11.	10.	9.
8.	7.	6.	6.	5.	5.	4.	4.	3.	3.
3.	2.	2.	2.	2.	2.	1.	1.	1.	1.
1.	1.	1.	1.	1.	1.	1.	1.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

HYDROGRAPH AT STATION Coit 2

TOTAL RAINFALL = 2.88, TOTAL LOSS = 1.25, TOTAL EXCESS = 1.63

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
40.	12.25	(CFS) 5.	2.	2.	2.
		(INCHES) 1.122	1.620	1.620	1.620
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = 0.04 SQ MI

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*****
*      *
54 KK * Comb *      Combine Routed Detention basin and Riprap swale with Coit Heights 2
*      *
*****

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55 HC      HYDROGRAPH COMBINATION
          ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION Comb

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
134.	12.25	(CFS) 22.	9.	9.	9.
		(INCHES) 0.861	1.398	1.398	1.398
		(AC-FT) 11.	17.	17.	17.

CUMULATIVE AREA = 0.23 SQ MI

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*****
*      *
56 KK * RTCOIT *      Route the outlet from D. Basin and RR Swale to the Coit D. Basin
*      *
*****

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HYDROGRAPH ROUTING DATA

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58 RM      MUSKINGUM ROUTING
          NSTPS      1 NUMBER OF SUBREACHES
          AMSKK      0.11 MUSKINGUM K
          X          0.35 MUSKINGUM X

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\*\*\*

\*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RTCOIT.  
 REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

\*\*\* \*\*

HYDROGRAPH AT STATION RTCOIT

PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW

(CFS)	(HR)		6-HR	24-HR	72-HR	23.98-HR
123.	12.35	(CFS)	22.	9.	9.	9.
		(INCHES)	0.860	1.392	1.392	1.392
		(AC-FT)	11.	17.	17.	17.

CUMULATIVE AREA = 0.23 SQ MI

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*****
*
59 KK * Coit 1 * Watershed of Coit Heights Unit 1, Sierra Highlands and Future Dev.
*
*****

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SUBBASIN RUNOFF DATA

60 BA SUBBASIN CHARACTERISTICS  
TAREA 0.05 SUBBASIN AREA

PRECIPITATION DATA

61 PH DEPTHS FOR 1-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	.....	.....	TP-40	.....	.....	TP-49	.....			
5-MIN	15-MIN	30-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.48	0.73	1.08	1.20	1.32	1.62	2.16	2.88	0.00	0.00	0.00	0.00

STORM AREA = 0.05

62 LS SCS LOSS RATE  
STRTL 0.30 INITIAL ABSTRACTION  
CRVNBR 37.00 CURVE NUMBER  
RTIMP 0.00 PERCENT IMPERVIOUS AREA

63 UD SCS DIMENSIONLESS UNITGRAPH  
TLAG 0.17 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH  
53 END-OF-PERIOD ORDINATES

4.	12.	23.	37.	56.	78.	100.	116.	127.	133.
133.	130.	123.	114.	104.	91.	77.	64.	54.	46.
40.	35.	30.	26.	22.	19.	16.	14.	12.	10.
9.	7.	6.	6.	5.	4.	4.	3.	3.	2.
2.	2.	1.	1.	1.	1.	1.	1.	1.	0.
0.	0.	0.							

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HYDROGRAPH AT STATION Coit 1

TOTAL RAINFALL = 2.38, TOTAL LOSS = 1.25, TOTAL EXCESS = 1.63

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
59.	12.17	(CFS) 6.	2.	2.	2.
		(INCHES) 1.123	1.624	1.624	1.624
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = 0.05 SQ MI

\*\*\*\*\*

```

*****
*                               *
64 KK *   RTCOIT *   Route the outlet from D. Basin and RR Swale to the Coit D. Basin
*                               *
*****

```

HYDROGRAPH ROUTING DATA

66 RM MUSKINGUM ROUTING

NSTPS	1 NUMBER OF SUBREACHES
AMSKK	0.11 MUSKINGUM K
X	0.35 MUSKINGUM X

\*\*\*

\*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RTCOIT.  
REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

\*\*\*

HYDROGRAPH AT STATION RTCOIT

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
54.	12.27	(CFS) 6.	2.	2.	2.
		(INCHES) 1.123	1.619	1.619	1.619
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = 0.05 SQ MI

fj

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*****
*                               *
67 KK *   Bullys *   Watershed Concentrating at Bullys Sports bar
*                               *
*****

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SUBBASIN RUNOFF DATA

68 8A SUBBASIN CHARACTERISTICS

TAREA	0.02 SUBBASIN AREA
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PRECIPITATION DATA

69 PH

DEPTHS FOR 1-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.48	0.73	1.08	1.20	1.32	1.52	2.16	2.88	0.00	0.00	0.00	0.00

STORM AREA = 0.02

70 LS

SCS LOSS RATE

STRTL 0.30 INITIAL ABSTRACTION  
 CRVNR 87.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

71 UD

SCS DIMENSIONLESS UNITGRAPH

TLAG 0.17 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.00000

UNIT HYDROGRAPH

53 END-OF-PERIOD ORDINATES

2.	5.	10.	16.	24.	33.	42.	50.	54.	56.
57.	55.	52.	48.	44.	39.	33.	27.	23.	20.
17.	15.	13.	11.	9.	8.	7.	6.	5.	4.
4.	3.	3.	2.	2.	2.	2.	1.	1.	1.
1.	1.	1.	1.	0.	0.	0.	0.	0.	0.
0.	0.	0.							

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HYDROGRAPH AT STATION Sullys

TOTAL RAINFALL = 2.88, TOTAL LOSS = 1.25, TOTAL EXCESS = 1.63

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
25.	12.17	(CFS) 3.	1.	1.	1.
		(INCHES) 1.123	1.624	1.624	1.624
		(AC-FT) 1.	2.	2.	2.

CUMULATIVE AREA = 0.02 SQ MI

\*\*\*\*\*

72 KK

\*\*\*\*\*  
 \* \*  
 \* RTCOIT \*  
 \* \*  
 \*\*\*\*\*

Route the outlet from D. Basin and RR Swale to the Coit D. Basin

HYDROGRAPH ROUTING DATA

74 RM

MUSKINGUM ROUTING

NSTPS 1 NUMBER OF SUBREACHES

AMSKK 0.11 MUSKINGUM X  
 X 0.35 MUSKINGUM X

\*\*\*\*\* WARNING \*\*\*\*\* POSSIBLE INSTABILITIES IN THE MUSKINGUM ROUTING FOR REACH RTCOIT.  
 REDUCE NSTPS OR DECREASE YOUR COMPUTATION INTERVAL (FIRST FIELD OF THE IT RECORD).

\*\*\* \*\*

HYDROGRAPH AT STATION RTCOIT

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
23.	12.27	(CFS) 3.	1.	1.	1.
		(INCHES) 1.123	1.620	1.620	1.620
		(AC-FT) 1.	2.	2.	2.

CUMULATIVE AREA = 0.02 SQ MI

\*\*\*\*\*

\*\*\*\*\*  
 \* \*  
 75 KK \* CoitPl \* Watershed of Coit Plaza  
 \* \*  
 \*\*\*\*\*

SUBBASIN RUNOFF DATA

76 BA SUBBASIN CHARACTERISTICS  
 TAREA 0.04 SUBBASIN AREA

PRECIPITATION DATA

77 PH DEPTHS FOR 1-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
0.48	0.73	1.08	1.20	1.32	1.62	2.16	2.88	0.00	0.00	0.00	0.00

§ STORM AREA = 0.34

78 LS SCS LOSS RATE  
 STRTL 0.30 INITIAL ABSTRACTION  
 CRVNR 87.00 CURVE NUMBER  
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

79 UD SCS DIMENSIONLESS UNITGRAPH  
 TLAG 0.17 LAG

\*\*\*

VALUE EXCEEDS TABLE IN LOGLOG 0.01667 0.01667 24.30000

UNIT HYDROGRAPH  
 53 END-OF-PERIOD ORDINATES

3. 11. 20. 33. 50. 70. 89. 104. 113. 118.



119.	116.	109.	101.	92.	81.	68.	57.	48.	41.
36.	31.	27.	23.	20.	17.	15.	12.	11.	9.
8.	7.	6.	5.	4.	4.	3.	3.	2.	2.
2.	1.	1.	1.	1.	1.	1.	1.	0.	0.
0.	0.	0.							

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HYDROGRAPH AT STATION CoitPl

TOTAL RAINFALL = 2.88, TOTAL LOSS = 1.25, TOTAL EXCESS = 1.63

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
53.	12.17	(CFS) 5.	2.	2.	2.
		(INCHES) 1.123	1.624	1.624	1.624
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = 0.04 SQ MI

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*****
*           *
80 KK *   Combo   *   Combine outlet of Routed Silverado Detention Basin with Coit 08
*           *
*****

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81 HC            HYDROGRAPH COMBINATION  
                  ICOMP            4    NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\*                    \*\*\*                    \*\*\*                    \*\*\*                    \*\*\*

HYDROGRAPH AT STATION Comb

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
223.	12.30	(CFS) 35.	14.	14.	14.
		(INCHES) 0.944	1.467	1.467	1.467
		(AC-FT) 17.	27.	27.	27.

CUMULATIVE AREA = 0.35 SQ MI

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*****
*           *
92 KK *   Mccarn  *
*           *
*****

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Reservoir routing at McCarran Blvd.  
 With 54 inch storm drain in place through Canyon Center

HYDROGRAPH ROUTING DATA

85 RS	STORAGE ROUTING										
	NSTPS	1 NUMBER OF SUBREACHES									
	ITYP	STOR TYPE OF INITIAL CONDITION									
	RSVRIC	-1.00 INITIAL CONDITION									
	X	0.00 WORKING R AND D COEFFICIENT									
86 SV	STORAGE	0.0	0.0	0.3	0.6	0.9	1.3	1.7	2.2	2.7	3.2
		3.3	4.4	5.1	5.8	6.5	7.4	8.3			
88 SQ	DISCHARGE	0.	5.	18.	38.	61.	79.	94.	107.	118.	128.
		138.	147.	155.	163.	171.	178.	185.			
90 SE	ELEVATION	48.40	49.40	50.40	51.40	52.40	53.40	54.40	55.40	56.40	57.40
		58.40	59.40	60.40	61.40	62.40	63.40	64.40			

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HYDROGRAPH AT STATION McCarrn

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	23.98-HR
129.	12.52	35.	14.	14.	14.
		(INCHES) 0.940	1.459	1.459	1.459
		(AC-FT) 17.	27.	27.	27.
PEAK STORAGE (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	23.98-HR
3.	12.52	1.	0.	0.	0.
PEAK STAGE (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	23.98-HR
57.51	12.52	51.35	49.77	49.77	49.77

CUMULATIVE AREA = 0.35 SQ MI

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	SREU21	111.	12.18	12.	4.	4.	0.11		
ROUTED TO	Silv08	8.	12.85	7.	4.	4.	0.11	4975.95	12.38
HYDROGRAPH AT	RipRap	100.	12.15	9.	3.	3.	0.08		
2 COMBINED AT	DB&RR	105.	12.15	17.	7.	7.	0.19		
ROUTED TO	RT C2	94.	12.25	17.	7.	7.	0.19		
HYDROGRAPH AT	Coit 2	40.	12.25	5.	2.	2.	0.04		
2 COMBINED AT	Comb (Pipe 1)	134.	12.25	22.	9.	9.	0.23		
ROUTED TO	RTCOIT	123.	12.35	22.	9.	9.	0.23		
HYDROGRAPH AT	Coit (Pipe 273)	59.	12.17	6.	2.	2.	0.05		
ROUTED TO	RTCOIT	54.	12.27	6.	2.	2.	0.05		
HYDROGRAPH AT	Bullys (Pipe 4)	25.	12.17	3.	1.	1.	0.02		
ROUTED TO	RTCOIT	23.	12.27	3.	1.	1.	0.02		
HYDROGRAPH AT	CoitPl	53.	12.17	5.	2.	2.	0.04		
4 COMBINED AT	Comb	223.	12.30	35.	14.	14.	0.35		
ROUTED TO	Mccarn	129.	12.52	35.	14.	14.	0.35	57.51	12.52

\*\*\* NORMAL END OF HEC-1 \*\*\*

**ON-SITE CALCULATIONS  
FLOW MASTER**

System A  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	12.00 in
Discharge	2.26 cfs

---

---

Results		
Channel Slope	0.004024	ft/ft
Depth	12.0	in
Flow Area	0.79	ft <sup>2</sup>
Wetted Perimeter	3.14	ft
Top Width	0.00	ft
Critical Depth	0.64	ft
Percent Full	100.00	
Critical Slope	0.007253	ft/ft
Velocity	2.88	ft/s
Velocity Head	0.13	ft
Specific Energy	FULL	ft
Froude Number	FULL	
Maximum Discharge	2.43	cfs
Full Flow Capacity	2.26	cfs
Full Flow Slope	0.004024	ft/ft

---

System A  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	36.00 in
Discharge	91.60 cfs

---

---

Results		
Channel Slope	0.018863	ft/ft
Depth	36.0	in
Flow Area	7.07	ft <sup>2</sup>
Wetted Perimeter	9.42	ft
Top Width	0.00	ft
Critical Depth	2.86	ft
Percent Full	100.00	
Critical Slope	0.016351	ft/ft
Velocity	12.96	ft/s
Velocity Head	2.61	ft
Specific Energy	FULL	ft
Froude Number	FULL	
Maximum Discharge	98.53	cfs
Full Flow Capacity	91.60	cfs
Full Flow Slope	0.018863	ft/ft

---

System A  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	48.00 in
Discharge	151.60 cfs

---

---

Results	
Channel Slope	0.011140 ft/ft
Depth	48.0 in
Flow Area	12.57 ft <sup>2</sup>
Wetted Perimeter	12.57 ft
Top Width	0.00 ft
Critical Depth	3.61 ft
Percent Full	100.00
Critical Slope	0.009789 ft/ft
Velocity	12.06 ft/s
Velocity Head	2.26 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	163.08 cfs
Full Flow Capacity	151.60 cfs
Full Flow Slope	0.011140 ft/ft

---

System B  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	30.00 in
Discharge	60.00 cfs

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---

Results	
Channel Slope	0.021400 ft/ft
Depth	30.0 in
Flow Area	4.91 ft <sup>2</sup>
Wetted Perimeter	7.85 ft
Top Width	0.00 ft
Critical Depth	2.39 ft
Percent Full	100.00
Critical Slope	0.018607 ft/ft
Velocity	12.22 ft/s
Velocity Head	2.32 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	64.54 cfs
Full Flow Capacity	60.00 cfs
Full Flow Slope	0.021400 ft/ft

---



System B  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	36.00 in
Discharge	60.00 cfs

---

---

Results	
Channel Slope	0.008093 ft/ft
Depth	36.0 in
Flow Area	7.07 ft <sup>2</sup>
Wetted Perimeter	9.42 ft
Top Width	0.00 ft
Critical Depth	2.50 ft
Percent Full	100.00
Critical Slope	0.007855 ft/ft
Velocity	8.49 ft/s
Velocity Head	1.12 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	64.54 cfs
Full Flow Capacity	60.00 cfs
Full Flow Slope	0.008093 ft/ft

---

System C  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	24.00 in
Discharge	25.00 cfs

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---

Results		
Channel Slope	0.012214	ft/ft
Depth	24.0	in
Flow Area	3.14	ft <sup>2</sup>
Wetted Perimeter	6.28	ft
Top Width	0.00	ft
Critical Depth	1.76	ft
Percent Full	100.00	
Critical Slope	0.010977	ft/ft
Velocity	7.96	ft/s
Velocity Head	0.98	ft
Specific Energy	FULL	ft
Froude Number	FULL	
Maximum Discharge	26.89	cfs
Full Flow Capacity	25.00	cfs
Full Flow Slope	0.012214	ft/ft

---

System D  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	18.00 in
Discharge	10.30 cfs

---

---

Results	
Channel Slope	0.009616 ft/ft
Depth	18.0 in
Flow Area	1.77 ft <sup>2</sup>
Wetted Perimeter	4.71 ft
Top Width	0.00 ft
Critical Depth	1.24 ft
Percent Full	100.00
Critical Slope	0.009538 ft/ft
Velocity	5.83 ft/s
Velocity Head	0.53 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	11.08 cfs
Full Flow Capacity	10.30 cfs
Full Flow Slope	0.009616 ft/ft

---

System D  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	24.00 in
Discharge	13.40 cfs

---

---

Results	
Channel Slope	0.003509 ft/ft
Depth	24.0 in
Flow Area	3.14 ft <sup>2</sup>
Wetted Perimeter	6.28 ft
Top Width	0.00 ft
Critical Depth	1.32 ft
Percent Full	100.00
Critical Slope	0.005901 ft/ft
Velocity	4.27 ft/s
Velocity Head	0.28 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	14.41 cfs
Full Flow Capacity	13.40 cfs
Full Flow Slope	0.003509 ft/ft

---

System E  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	18.00 in
Discharge	8.70 cfs

---

---

Results	
Channel Slope	0.006860 ft/ft
Depth	18.0 in
Flow Area	1.77 ft <sup>2</sup>
Wetted Perimeter	4.71 ft
Top Width	0.00 ft
Critical Depth	1.14 ft
Percent Full	100.00
Critical Slope	0.007972 ft/ft
Velocity	4.92 ft/s
Velocity Head	0.38 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	9.36 cfs
Full Flow Capacity	8.70 cfs
Full Flow Slope	0.006860 ft/ft

---

System E  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	18.00 in
Discharge	10.63 cfs

---

---

Results		
Channel Slope	0.010242	ft/ft
Depth	18.0	in
Flow Area	1.77	ft <sup>2</sup>
Wetted Perimeter	4.71	ft
Top Width	0.00	ft
Critical Depth	1.25	ft
Percent Full	100.00	
Critical Slope	0.009925	ft/ft
Velocity	6.02	ft/s
Velocity Head	0.56	ft
Specific Energy	FULL	ft
Froude Number	FULL	
Maximum Discharge	11.43	cfs
Full Flow Capacity	10.63	cfs
Full Flow Slope	0.010242	ft/ft

---

System E  
Worksheet for Circular Channel

---

Project Description	
Project File	c:\haestad\fmw\coit-pla.fm2
Worksheet	SYSTEM A
Flow Element	Circular Channel
Method	Manning's Formula
Solve For	Full Flow Slope

---

---

Input Data	
Mannings Coefficient	0.013
Diameter	12.00 in
Discharge	2.00 cfs

---

---

Results	
Channel Slope	0.003152 ft/ft
Depth	12.0 in
Flow Area	0.79 ft <sup>2</sup>
Wetted Perimeter	3.14 ft
Top Width	0.00 ft
Critical Depth	0.60 ft
Percent Full	100.00
Critical Slope	0.006859 ft/ft
Velocity	2.55 ft/s
Velocity Head	0.10 ft
Specific Energy	FULL ft
Froude Number	FULL
Maximum Discharge	2.15 cfs
Full Flow Capacity	2.00 cfs
Full Flow Slope	0.003152 ft/ft

---

**ON-SITE DETENTION CALCULATIONS  
POND PACK**



Type.... Executive Summary (Nodes)  
 Name.... Watershed  
 File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAY.PPW  
 Storm... TypeII 24hr Tag: Pre..5

Page 2.01  
 Event: 5 yr

NETWORK SUMMARY -- NODES  
 (Trun.= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left & Rt)

DEFAULT Design Storm File, ID = COIT.RNQ coit plaza

Storm Tag Name = Pre..5

-----  
 Data Type, File, ID = Synthetic Storm SCSTYPES.RNF TypeII 24hr  
 Storm Frequency = 5 yr  
 Total Rainfall Depth= 1.4200 in  
 Duration Multiplier = 1  
 Resulting Duration = 24.0000 hrs  
 Resulting Start Time= .0000 hrs Step= .1000 hrs End= 24.0000 hrs

Node ID	Type	HYG Vol ac-ft	Qpeak Trun. hrs	Qpeak cfs	Max WSEL ft
-----	-----	-----	-----	-----	-----
Outfall OUTFALL	JCT	.692	12.0300	10.12	
PRE-DEVELOPED	AREA	.692	12.0300	10.12	

Type.... Executive Summary (Nodes)  
 Name.... Watershed  
 File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAY.PPW  
 Storm... TypeII 24hr Tag: Pre100

Page 2.05  
 Event: 100 yr

NETWORK SUMMARY -- NODES  
 (Trun.= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left & Rt)

DEFAULT Design Storm File, ID = COIT.RNQ coit plaza

Storm Tag Name = Pre100

-----  
 Data Type, File, ID = Synthetic Storm SCSTYPES.RNF TypeII 24hr  
 Storm Frequency = 100 yr  
 Total Rainfall Depth= 2.8800 in  
 Duration Multiplier = 1  
 Resulting Duration = 24.0000 hrs  
 Resulting Start Time= .0000 hrs Step= .1000 hrs End= 24.0000 hrs

Node ID	Type	HYG Vol ac-ft	Trun.	Qpeak hrs	Qpeak cfs	Max WSEL ft
Outfall	OUTFALL	3.008		12.0000	49.32	
	PRE-DEVELOPED	3.008		12.0000	49.32	

Type.... Executive Summary (Nodes)  
 Name.... Watershed  
 File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAYPOST.PPW  
 Storm... TypeII 24hr Tag: Dev..5

Page 2.01  
 Event: 5 yr

NETWORK SUMMARY -- NODES  
 (Trun.= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left & Rt)

DEFAULT Design Storm File, ID = COIT.RNQ coit plaza

Storm Tag Name = Dev..5

-----  
 Data Type, File, ID = Synthetic Storm SCSTYPES.RNF TypeII 24hr  
 Storm Frequency = 5 yr  
 Total Rainfall Depth= 1.4200 in  
 Duration Multiplier = 1  
 Resulting Duration = 24.0000 hrs  
 Resulting Start Time= .0000 hrs Step= .1000 hrs End= 24.0000 hrs

Node ID	Type	HYG Vol ac-ft	Trun.	Qpeak hrs	Qpeak cfs	Max WSEL ft
DEVELOPED	AREA	2.932		11.9800	44.40	
Outfall OUTLET	JCT	2.932		11.9800	44.40	
POND	IN POND	2.932		11.9800	44.40	
POND	OUT POND	2.932		11.9800	44.40	

Type.... Executive Summary (Nodes)  
 Name.... Watershed  
 File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAYPOST.PPW  
 Storm... TypeII 24hr Tag: Dev100

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 Event: 100 yr

NETWORK SUMMARY -- NODES  
 (Trun.= HYG Truncation: Blank=None; L=Left; R=Rt; LR=Left & Rt)

DEFAULT Design Storm File, ID = COIT.RNQ coit plaza

Storm Tag Name = Dev100

-----  
 Data Type, File, ID = Synthetic Storm SCSTYPES.RNF TypeII 24hr  
 Storm Frequency = 100 yr  
 Total Rainfall Depth= 2.8800 in  
 Duration Multiplier = 1  
 Resulting Duration = 24.0000 hrs  
 Resulting Start Time= .0000 hrs Step= .1000 hrs End= 24.0000 hrs

Node ID	Type	HYG Vol ac-ft	Trun.	Qpeak hrs	Qpeak cfs	Max WSEL ft
DEVELOPED	AREA	6.411		11.9800	93.12	
Outfall OUTLET	JCT	6.411		11.9800	93.12	
POND	IN POND	6.411		11.9800	93.12	
POND	OUT POND	6.411		11.9800	93.12	

Type.... Target Outflow Volume Estimates  
Name.... EST.VOL.PK. 10

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File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAYPOST.PPW

DETENTION STORAGE ESTIMATES -- Target Peak Outflow Rate

Return Events	Peak In (cfs)	Target (cfs)	Lower (ac-ft)	Linear (ac-ft)	Curvlinr (ac-ft)	Upper (ac-ft)	Total (ac-ft)
	44.399	10.120	.759	.887	1.221	1.850	2.932

CALCULATION TIME RANGES

Return Events	Lower		Linear		Curvilinear		Upper		Total	
	From (hrs)	To (hrs)	From (hrs)	To (hrs)	From (hrs)	To (hrs)	From (hrs)	To (hrs)	From (hrs)	To (hrs)
	11.68	12.23	11.51	12.23	2.40	12.23	2.40	12.23	2.40	24.46

File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAYPOST.PPW

DETENTION STORAGE ESTIMATES -- Target Peak Outflow Rate

Return Events	Peak In (cfs)	Target (cfs)	Lower (ac-ft)	Linear (ac-ft)	Curvlinr (ac-ft)	Upper (ac-ft)	Total (ac-ft)
	93.117	43.800	.802	1.197	2.018	3.939	6.411

CALCULATION TIME RANGES

Return Events	Lower		Linear		Curvilinear		Upper		Total	
	From (hrs)	To (hrs)	From (hrs)	To (hrs)	From (hrs)	To (hrs)	From (hrs)	To (hrs)	From (hrs)	To (hrs)
	11.80	12.13	11.56	12.13	1.26	12.13	1.26	12.13	1.26	24.49

Type.... Vol: Elev-Area  
Name.... POND

File.... C:\HAESTAD\PPKW\SAMPLE\COIT-MAYPOST.PPW

Elevation : (ft)	Planimeter (sq.in)	Area (acres)	A1+A2+sq(A1*A2) (acres)	Volume (ac-ft)	Volume Sum (ac-ft)
854.00	-----	.0973	.0000	.000	.000
865.00	-----	.5420	.8689	3.186	3.186

POND VOLUME EQUATIONS

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2} - \text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1} * \text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
Area1, Area2 = Areas computed for EL1, EL2, respectively  
Volume = Incremental volume between EL1 and EL2

Elev. vs. Volume  
POND

